

```

C**** Definition of some constant values
S1=A1/NREF**2
S2=B1
S5=E1
S6=F1*NREF
S7=G1*NREF**2
S8=H1*NREF**3

C**** Initial guess for speed (X1) and flowrate (X2)
C**** the initial speed is taken to be the speed where
C**** HEADpump=HEADsystem at zero flowrate
NINIT=NREF*(S3/A1)**.5
IF(NINIT.GE.NMAX)THEN
  FAIL=4
ENDIF
C**** the initial flowrate is taken to be the flowrate
C**** at maximum permitted speed where HEADpump=HEADsystem
QINIT=((S3-S1*NMAX**2)/(S2-S4))**.5
X(1)=NINIT
X(2)=QINIT

C**** The following part evaluates the torque required to
C**** provide flow.
C**** Evaluation of Q and H at shutoff condition
C**** QOFF is choosen to be very small, i.e. QNOM per second
C**** divided by 100
QOFF=QNOM/3.6E5
HOFF=A1-B1*QOFF**2
C**** Computation of torque at shutoff condition at reference
C**** speed
IF(POFF.LT.0)THEN
  ETAOFF=E1+F1*QOFF+G1*QOFF**2+H1*QOFF**3
  TOFF=CONST*QOFF*HOFF/ETAOFF/NREF
ELSE
  TOFF=POFF/(2.*PI*NREF)
ENDIF

TREQ=TOFF*(NINIT/NREF)**2
FAIL=0

C-----
ELSE
C**** First and following calls in timestep
FAIL=0
C**** Set inputs
TL=XIN(1)

X(1)=S(ISTORE)
X(2)=S(ISTORE+1)

C**** to avoid division by zero, i.e. if torque=0

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IF(TL.GT.TREQ)THEN
  LOOP=0

C*****
50  CONTINUE
  COUNTER=1
C**** Iterative process to find the solution of the system of
C**** nonlinear equations, using Newton's method
100  CONTINUE
C**** set up the objective functions
  CALL SYSTEM(F,X,TL)
C**** set up of the Jacobian matrix
  CALL JACOBIAN(J,X,TL)

C**** To inverse the matrix a direct method via the adjuncate is used
C**** Evaluation of the determinant of the Jacobian
  DET=J(1,1)*J(2,2)-J(2,1)*J(1,2)

C**** Evaluation of the inverse of the Jacobian
  JINV(1,1)=J(2,2)/DET
  JINV(1,2)=-J(1,2)/DET
  JINV(2,1)=-J(2,1)/DET
  JINV(2,2)=J(1,1)/DET

C**** Basic algorithm
  XNEW(1)=X(1)-(JINV(1,1)*F(1)+JINV(1,2)*F(2))
  XNEW(2)=X(2)-(JINV(2,1)*F(1)+JINV(2,2)*F(2))

C**** Check on the infinity norm of the solution vector
C**** i.e. the maximum value of xnew-xold (=max. error)
C**** about convergence
  DELTA1=ABS(XNEW(1)-X(1))
  DELTA2=ABS(XNEW(2)-X(2))
  IF (MAX(DELTA1,DELTA2).GT.EPS) THEN
    IF (COUNTER.LT.MAXIT) THEN
      COUNTER=COUNTER+1
      X(1)=XNEW(1)
      X(2)=XNEW(2)
      GOTO 100
    ELSE
C**** Convergence was not attained after maxit iterations
      FAIL=3
    ENDIF
  ENDIF

C*****
  X(1)=XNEW(1)
  X(2)=XNEW(2)
  N=XNEW(1)
  Q=XNEW(2)
C**** Check if Q is in the negative range, i.e. the wrong solution

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C**** is found
      IF ((Q.LT.0.).OR.(N.LT.0)) THEN
C**** to protect an endless loop situation the following
C**** control function is introduced
      IF (LOOP.EQ.0) THEN
        X(1)=NMAX
        X(2)=5.*QINIT
        LOOP=1
        GOTO 50
      ELSEIF (LOOP.EQ.1) THEN
C**** try again with higher limits
        X(1)=2.*NMAX
        X(2)=2.*QNOM
        LOOP=2
        GOTO 50
      ELSE
C**** Newton could not find proper solution
C**** go ahead
        FAIL=2
      ENDIF
    ENDIF

C**** Evaluation of total head and efficiency
      H=S3+S4*Q**2
      ETA=CONST*Q*H/TL/N
C**** Check if speed exceeds maximum speed
      IF (N.GT.NMAX) THEN
C**** Flowrate is taken to be the flowrate at maximum
C**** permitted speed
        Q=QINIT
        FAIL=1
C**** Evaluation of total head
        H=S3+S4*Q**2
C**** Efficiency is evaluated at NMAX and QINIT
        ETA=S5+S6*Q/NMAX+S7*Q**2/NMAX**2+S8*Q**3/NMAX**3
C**** Correction of initial guess
        X(1)=NMAX
        X(2)=QINIT
      ENDIF
    ELSE
C**** In this case the affinity laws are valid. The torque
C**** or the speed follows a parabolic function
      N=NREF*(TL/TOFF)**.5
      Q=0.
      H=HOF*(N/NREF)**2
      ETA=0.
    ENDIF
  ENDIF
C-----

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IF((X(1).GT.0).AND.(X(2).GT.0))THEN
  S(ISTORE)=X(1)
  S(ISTORE+1)=X(2)
ENDIF

PHYD=RHO*Q*H
PMECH=2*PI*TL*N

C**** Set outputs
OUT(1)=N
OUT(2)=TL
OUT(3)=Q
OUT(4)=H
OUT(5)=H/A
OUT(6)=PHYD
OUT(7)=PMECH
OUT(8)=FAIL

END

C*****
SUBROUTINE SYSTEM(FX,TL)
C**** Subroutine provides the objective function of the system
C   of nonlinear equations
C   TL,X1,X2 in
C   F out

REAL F(2),X(2)
REAL TL,S1,S2,S3,S4,S5,S6,S7,S8,CONST

COMMON /COEF/ S1,S2,S3,S4,S5,S6,S7,S8,CONST

F(1)=S1*X(1)**2+S2*X(2)**2-S3-S4*X(2)**2
F(2)=CONST/TL*(S1*X(1)**4*X(2)+S2*X(1)**2*X(2)**3)
& -S5*X(1)**3-S6*X(1)**2*X(2)-S7*X(1)*X(2)**2-S8*
& X(2)**3
END

C*****
SUBROUTINE JACOBIAN(JX,TL)
C**** Subroutine provides all the derivatives for the Jacobian matrix
C   X1,X2,TL in
C   J out

REAL J(2,2),X(2)
REAL TL,S1,S2,S3,S4,S5,S6,S7,S8,CONST

COMMON /COEF/ S1,S2,S3,S4,S5,S6,S7,S8,CONST

J(1,1)=2.*S1*X(1)

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      J(1,2)=2.*S2*X(2)-2.*S4*X(2)
      J(2,1)=CONST/TL*(4.*S1*X(1)**3*X(2)+2.*S2*X(1)*X(2)**3)
&      -3.*S5*X(1)**2-2.*S6*X(1)*X(2)-S7*X(2)**2
      J(2,2)=CONST/TL*(S1*X(1)**4+3.*S2*X(1)**2*X(2)**2)-
&      S6*X(1)**2-2.*S7*X(1)*X(2)-3.*S8*X(2)**2
      END

C*****
      SUBROUTINE HEADPOLYNOMIAL(A1,B1)

C**** Program fits a polynomial through a given number of data
C**** points using least squares method
C**** the polynomial has the form  $y=a+bx^2$ 

C**** HEAD -- head of the pump [m]
C**** CAP -- Capacity (volumetric flowrate) [m^3/sec]
C**** A1,B1 -- Coefficients of the constructed polynomial
C**** MEAN -- Average over the head values
C**** RSQUARES -- R^2 measure of curve fit
C**** SUM1-SUM6 -- Summation terms occurring in the normal equations
C**** Y -- Array containing the fitted values

      REAL SUM1,SUM2,SUM3,SUM4,SUM5,SUM6,A1,B1
      REAL MEAN,RSQUARE
      REAL HEAD(50),CAP(50),Y(50)
      INTEGER M

C**** Input file contains the data
      OPEN (12,FILE='HEAD.DAT',STATUS='OLD')
      REWIND(12)

C**** Read in number of data pairs
      READ(12,*) M

C**** Read in the data pairs
      DO 100 I=1,M
        READ(12,*) CAP(I),HEAD(I)
      100 CONTINUE

C**** Evaluation of the sum terms in the normal equations
      SUM1=0.
      SUM2=0.
      SUM3=0.
      SUM4=0.
      DO 200 J=1,M
        SUM1=SUM1+CAP(J)**2
        SUM2=SUM2+HEAD(J)
        SUM3=SUM3+CAP(J)**4
        SUM4=SUM4+HEAD(J)*CAP(J)**2
      200 CONTINUE

```



```

C**** Evaluation of the coefficients of the polynomial
      B1=(M*SUM4-SUM2*SUM1)/(M*SUM3-SUM1**2)
      A1=(SUM2 B1+SUM1)/M

      DO 300 L=1,M
        Y(L)=A1+B1*CAP(L)**2
300  CONTINUE

C**** Estimation of the curve fit precision
      MEAN=SUM2/M
      SUM5=0.
      SUM6=0.
      DO 400 LL=1,M
        SUM5=SUM5+(Y(LL)-MEAN)**2
        SUM6=SUM6+(HEAD(LL)-MEAN)**2
400  CONTINUE
C**** R^2 measures the proportion of total variation about the mean
C**** explained by the regression
      RSQUARE=SUM5/SUM6
      END

C*****
      SUBROUTINE EFFPOLYNOMIAL(E1,F1,G1,H1)

C**** Subroutine fits a polynomial through a given number of data
C**** points using least squares method
C**** the polynomial has the form  $y=a+bx+cx^2+dx^3$ 

C**** ETA -- pump efficiency
C**** CAP -- Capacity (volumetric flowrate)
C**** ESUM1-ESUM12 -- Summation terms occurring in the normal equations
C**** E1,F1,G1,H1 -- Coefficients of the constructed polynomial
C**** MEAN -- Average over the efficiency values
C**** RSQUARES -- R^2 measure of curve fit
C**** Y -- Array of dimension NN containing the fitted values
C**** A -- Array of dimension NN*NN containing the coefficients
C**** of the normal equations
C**** B -- Array of dimension NN (B-vector)
C**** SOL -- Array containing the solution, i.e. the coefficients
C**** E1,F1,G1,H1
C**** LINDEK -- index vector (Gaussian elimination)
C**** S -- scale vector (Gaussian elimination)

      INTEGER M,MM,NN
      PARAMETER (NN=4)
      REAL ESUM1,ESUM2,ESUM3,ESUM4,ESUM5,ESUM6,ESUM7,ESUM8
      REAL ESUM9,SUM10,ESUM11,ESUM12,E1,F1,G1,H1
      REAL MEAN,RSQUARE
      REAL ETA(50),CAP(50),Y(50),A(NN,NN),B(NN),SOL(NN)
      REAL LINDEK(NN),S(NN)

```

```

C**** Input file contains the data
      OPEN (14,FILE='EFF.DAT',STATUS='OLD')
      REWIND(14)

C**** Read in number of data pairs
      READ(14,*) M
      MM=M+4
C**** Read in the data pairs
      DO 100 I=1,M
        READ(14,*) CAP(I),ETA(I)
100  CONTINUE

C**** To force the fitted curve through the origin a couple
C**** of data pairs are set equal 0
      DO 120 II=M+1,MM
        CAP(II)=0.
        ETA(II)=0.
120  CONTINUE

C**** Evaluation of the sum terms in the normal equations
      ESUM1=0.
      ESUM2=0.
      ESUM3=0.
      ESUM4=0.
      ESUM5=0.
      ESUM6=0.
      ESUM7=0.
      ESUM8=0.
      ESUM9=0.
      ESUM10=0.
      DO 200 J=1,M
        ESUM1=ESUM1+CAP(J)
        ESUM2=ESUM2+CAP(J)**2
        ESUM3=ESUM3+CAP(J)**3
        ESUM4=ESUM4+CAP(J)**4
        ESUM5=ESUM5+CAP(J)**5
        ESUM6=ESUM6+CAP(J)**6
        ESUM7=ESUM7+ETA(J)
        ESUM8=ESUM8+ETA(J)*CAP(J)
        ESUM9=ESUM9+ETA(J)*CAP(J)**2
        ESUM10=ESUM10+ETA(J)*CAP(J)**3
200  CONTINUE

C**** Set up the matrix containing the normal equations A(n,n)
C**** In this case it is a (4*4) matrix
      A(1,1)=REAL(MM)
      A(2,1)=ESUM1
      A(2,2)=ESUM2
      A(3,1)=ESUM2
      A(3,2)=ESUM3

```

```

A(3,3)=ESUM4
A(4,1)=ESUM3
A(4,2)=ESUM4
A(4,3)=ESUM5
A(4,4)=ESUM6

C**** because of the symmetry of the matrix,it can be
C**** filled up by

DO 250 I=1,4
  DO 250 J=1,4
    IF(I.NE.J)THEN
      A(I,J)=A(J,I)
    ENDIF
  250 CONTINUE

C**** Set up B vector (dimension=4)
B(1)=ESUM7
B(2)=ESUM8
B(3)=ESUM9
B(4)=ESUM10

C**** The linear system of equations (normal equations) is solved
C**** using Gaussian elimination with partial pivoting
C**** LINDEX & S must occur in the calling sequence because they
C**** have a variable dimension. They are not used as output
      CALL GAUSS(A,B,SOL,LINDEX,S,NN)

C***** Output
E1=SOL(1)
F1=SOL(2)
G1=SOL(3)
H1=SOL(4)

DO 300 L=1,MM
  Y(L)=E1+F1*CAP(L)+G1*CAP(L)**2+H1*CAP(L)**3
300 CONTINUE

C**** Estimation of the curve fit precession
MEAN=ESUM7/REAL(MM)

ESUM11=0.
ESUM12=0.
DO 400 LL=1,MM
  ESUM11=ESUM11+(Y(LL)-MEAN)**2
  ESUM12=ESUM12+(Y(LL)-MEAN)**2
400 CONTINUE

C**** R^2 measures the proportion of total variation about the mean
C**** explained by the regression
RSQUARE=ESUM11/ESUM12

```



```

END

C*****
C**** Subroutine Gauss with partial pivoting
SUBROUTINE GAUSS(A,B,X,L,S,NN)

REAL A(NN,NN),B(NN),L(NN),S(NN),X(NN)

C**** Scale factors(s) and pivot(l)
DO 30 I=1,NN
  L(I)=1
  SMAX=0.
  DO 20 J=1,NN
    SMAX=AMAX1(SMAX,ABS(A(I,J)))
  20 CONTINUE
  S(I)=SMAX
30 CONTINUE

C**** Look for largest ratio to select pivot row
DO 70 K=1,NN-1
  RMAX=0.
  DO 40 I=K,NN
    R=ABS(A(L(I),K))/S(L(I))
    IF (R.GT.RMAX) THEN
      J=I
      RMAX=R
    ENDIF
  40 CONTINUE

C**** Update pivot vector
  XK=L(J)
  L(J)=L(K)
  L(K)=XK

C**** Forward elimination
  DO 60 I=K+1,NN
    XMULT=A(L(I),K)/A(L(K),K)
    DO 50 J=K+1,NN
      A(L(I),J)=A(L(I),J)-XMULT*A(L(K),J)
    50 CONTINUE
    A(L(I),K)=XMULT
  60 CONTINUE
70 CONTINUE

C**** Backward substitution
DO 100 K=1,NN-1
  DO 100 I=K+1,NN
    B(L(I))=B(L(I))-A(L(I),K)*B(L(K))
  100 CONTINUE

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```

X(NN)=B(L(NN))/A(L(NN),NN)
DO 150 I=NN-1,1,-1
  SUM=B(L(I))
  DO 140 J=I+1,NN
    SUM=SUM-A(L(I),J)*X(J)
140  CONTINUE
  X(I)=SUM/A(L(I),I)
150  CONTINUE

END

```

Resistance

```

C*****
C SUBROUTINE TYPE59(TIME,XIN,OUT,T,DTDT,PAR,INFO)
C   Version from: 12/14/89
C-----
C   This subroutine represents a model of an ohmic resistance.
C   The value of the resistance has to be provided as a
C   parameter by the user. This component is designed to operate
C   in a photovoltaic powered energy system. It can operate on
C   two different modes: voltage or current mode. If the MODE
C   signal is set to be one, the current is significant input and
C   voltage will be evaluated. Otherwise voltage is significant
C   input and current will be evaluated corresponding to the
C   ohmic law.
C*****
C**** Definition of the variables:
C**** TRNSYS specific variables:
C   XIN == input array
C   OUT == output array
C   PAR == parameters
C   TIME == simulation time
C   T,DTDT == not used in this component
C   INFO == array to use TRNSYS internal information

C**** component specific variables:
C   I == current [amps]
C   V == voltage [volts]
C   P == power [watts]
C   R == resistance [ohms]
C   MODE == signal determining operating mode
C     MODE=1: current is significant input
C     MODE=2: voltage is significant input
C*****
C**** declaration of variables:
C   INTEGER INFO
C   REAL R,V,I,TIME,XIN,OUT,T,DTDT,PAR,MODE

```

```

      DIMENSION XIN(3), OUT(3), PAR(1), INFO(10)
C*****
      INFO(6)=3
      INFO(9)=0
C-----
C**** initial call of component
      IF(INFO(7).LT.0)THEN
          CALL TYPECK(1,INFO,3,1,0)
C**** set parameters
          R=PAR(1)
      ENDIF
C-----
C**** set inputs
      I=XIN(1)
      V=XIN(2)
      MODE=XIN(3)

      IF (MODE.EQ.1.)THEN
C**** current guess
          V=I*R+B
      ELSE
C**** voltage guess
          I=(V-B)/R
      ENDIF
      P=I*V

C**** set outputs
      OUT(1)=I
      OUT(2)=V
      OUT(3)=P

      END

```

Battery

```

C*****
      SUBROUTINE TYPE70 (T,XIN,OUT,Q,DQDT,PAR,INFO)
C   version from 12/22/89
C*****
C   THIS COMPONENT SIMULATES THE PERFORMANCE OF A LEAD-ACID
C   STORAGE BATTERY. IT IS DESIGNED TO OPERATE IN CONJUNCTION
C   WITH A SOLAR CELL ARRAY AND A REGULATOR.

C   Q = STATE OF CHARGE [AH]
C   QM = RATED CAPACITY OF CELL [AH]
C   QC,QD = CAPACITY PARAMETERS ON CHARGE, DISCHARGE
C   F = FRACTIONAL STATE OF CHARGE = Q/QM (1.0 IS FULL CHARGE)
C   CP,CS = NUMBER OF CELLS IN PARALLEL, SERIES

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C P = POWER [WATTS]
C IQ = CURRENT [AMPS]
C IQMAX,IQMIN = MAXIMUM CURRENT (CHARGE), MINIMUM CURREN
C (DISCHARGE)
C V = VOLTAGE [VOLTS]
C VC,IC = CUTOFF VOLTAGE ON CHARGE, CURRENT CORRESPONDING
C TO VC
C ICTOL = PARAMETER FOR ITERATIVE CALCULATIONS
C VD = CUTOFF VOLTAGE ON DISCHARGE
C ED,RD = DATA USED TO CALCULATE VD WHEN VCONTR .LT. 0.
C VCONTR = SPECIFICATION OF VOLTAGE CONTROL ON DISCHARGE.
C POSITIVE MEANS  $VD = VCONTR$ . NEGATIVE MEANS  $VD = ED - ABS(IQ) * RD$ .
C VDI = DIODE VOLTAGE FROM Z-P MODEL
C VOC = OPEN CIRCUIT VOLTAGE AT FULL CHARGE
C ESC,ESD = EXTRAPOLATED OPEN CIRCUIT VOLTAGES
C GC,GD = COEFFICIENTS OF  $(1-F)IN V$  FORMULAS
C RSC,RSD = INTERNAL RESISTANCES AT FULL CHARGE
C MC,MD = CELL TYPE PARAMETERS WHICH DETERMINE THE SHAPES OF THE
C I-V-Q CHARACTERISTICS
C KCOUNT=COUNTS THE NUMBER OF ITERATIONS INVOLVED IN OBTAINING IC
C
C THE BATTERY MODEL IS THE MODEL RECOMMENDED IN THE BEST
C REPORT (THE HYMAN MODEL). IT IS THE SHEPHERD MODEL MODIFIED BY
C THE ADDITION OF A ZIMMERMAN-PETERSEN DIODE IN BOTH THE CHARGE AND
C DISCHARGE EQUIVALENT CIRCUITS.
C*****
  DIMENSION
  + DQDT(1), INFO(9), OUT(9), PAR(21),
  + Q(1), XIN(1)
  REAL
  + IL, IC, IC1, ICTOL,
  + IDF, IQ, IQMAX, IQMIN,
  + K1, MC, MD
C*****
  IF(INFO(7).GE.0)THEN
C**** set inputs
    IQ=XIN(1)
C**** current for one cell
    IQ=IQ/CP
  ENDIF

  IF(INFO(7).EQ.0)THEN
C**** computation of state of charge of battery from
C**** the previous time step
    F=OUT(2)
    H=1.-F
  ENDIF
C-----
C**** Initialization--first call of component
  IF (INFO(7).LT.0) THEN

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INFO(9)=1
INFO(6)=9
CALL TYPECK (1,INFO,1.21,1)
NDER=INFO(5)
IF (NDER.NE.1) THEN
  CALL TYPECK (5,INFO,0,0,0)
  RETURN
ENDIF
C**** Set parameters
QM=PAR(1)
CP=PAR(2)
CS=PAR(3)
EPF=PAR(4)
VC=PAR(5)
VCONTR=PAR(6)
IF (VCONTR.GT.0) THEN
  VD=VCONTR
C**** Check on minimum discharge voltage
  IF (VD.GT.2.5.OR.VD.LT.1.5) CALL TYPECK (-4,INFO,0,0,0)
ENDIF
ICTOL=PAR(7)
ESC=PAR(8)
ESD=PAR(9)
GC=PAR(10)
GD=PAR(11)
MC=PAR(12)
MD=PAR(13)
ED=PAR(14)
RD=PAR(15)
I1=PAR(16)
K1=PAR(17)
QC=PAR(18)
QD=PAR(19)
RSC=PAR(20)
RSD=PAR(21)

C**** Check on maximum charge voltage
  IF (VC.GT.2.8.OR.VC.LT.1.8) CALL TYPECK (-4,INFO,0,0,0)
C-----
C**** first and following calls in time step
  ELSE

C**** Modified Shepherd Model
  VOC=(ESC+ESD)/2.
  IF (IQ.GE.0.) THEN
C**** Charging
    VDI=1./K1*ALOG(IQ/I1+1.)
    V=VOC+VDI-GC*H+IQ*RSC*(1.+MC*H/(QC/QM-H))

    ICOUNT=0

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      IC=50.
C**** Iterative search for current
30  CONTINUE
      IC1=IC
      VDI=1./K1*ALOG(ABS(IC1)/I1+1.)
      IC=(VC-VOC-VDI+GC*H)/RSC/(1.+MC*H/(QC/QM-H))
      ICOUNT=ICOUNT+1

C**** 100 iterations are permitted to find IC
      IF(ICOUNT.GT.100)THEN
        GOTO 50
      ELSE
        IF (ABS(IC1-IC).GT.ICTOL) GO TO 30
      ENDIF
50  CONTINUE

      DQDT(1)=IQ*EFF

      ELSE
C**** Discharging
      VDI=1./K1*ALOG(-IQ/I1+1.)
      V=VOC-VDI-GD*H+IQ*RSD*(1.+MD*H/(QD/QM-H))
      DQDT(1)=IQ
    ENDIF
  ENDIF

C-----
      P=IQ*V

C**** Output
      OUT(1)=Q(1)
      OUT(2)=Q(1)/QM
      OUT(3)=P*CP*CS
      OUT(4)=0.
      IF (P.GT.0.) OUT(4)=(1.-EFF)*P*CP*CS
      OUT(5)=IQ*CP
      OUT(6)=V*CS
      IF (VCONTR.LT.0.) VD=ED-ABS(IQ)*RD
      OUT(7)=VD*CS
      OUT(8)=VC*CS
      OUT(9)=IC*CP
      RETURN
      END

```

Series Type Charge Controller

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C*****
SUBROUTINE TYPE73(TIME,XIN,OUT,T,DTDT1,PAR,INFO)
C  version from: 12/22/89
C*****

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C**** Subroutine represents a charge controller for a system including
C**** PV array, load and battery storage.
C**** The controller represents a series type controller.
C**** A blocking diode is included in the model. It prevents that the
C**** battery is being discharged through the cell. It is assumed that
C**** voltage drop at the diode is constant throughout the simulation
C**** and just depends on the diode material used in the system.
C**** The user has to provide this information as a parameter
C*****
C   Variables:
C   VB -- battery voltage [volts]
C   VD -- low limit on voltage, when battery discharging
C   VC -- high limit on voltage, when battery charging: cutoff voltage
C   VDA -- limit on voltage, above battery can again begin to discharge
C         after being charged
C   VCA -- limit on voltage, above battery can again begin to charge
C         after being discharged
C   VDIODE -- voltage of diode
C   VCELL -- voltage send to cell
C   VLOAD -- voltage send to load
C   F -- fractional state of charge
C   FD -- discharge limit on F
C   FC -- charge limit on F
C   FDA -- limit on F above battery can be discharged again after
C         being charged
C   FCA -- limit on F below battery can be charged again after
C         being discharged
C   IBMIN,IBMAX -- min. and max. battery current permitted
C   IB -- battery current
C*****

      IMPLICIT NONE
      INTEGER INFO
      INTEGER ISTORE,NSTORE,IAV
      REAL TIME,XIN,OUT,T,DTDT,PAR,S
      REAL VB,VC,VD,V,VDA,VCA,VDIODE,IB
      REAL F,FD,FC,FDA,FCA,IBMIN,IBMAX,FAIL
      REAL VCELL,VLOAD,DUMMY
      DIMENSION XIN(5),OUT(3),PAR(9),INFO(10)

      COMMON /STORE/NSTORE,IAV,S(5000)
C**** store is used to store values from previous timestep
C*****
      INFO(6)=3
      INFO(9)=0

C-----
C**** Initial call of component
      IF(INFO(7).LT.0)THEN

```

```

C**** storage allocation
      INFO(10)=1
      CALL TYPECK(1,INFO,5,9,0)
      ISTORE=INFO(10)
C**** Initialization of auxiliary variables used in secant
C**** method
      S(ISTORE)=0.
C**** SET PARAMETERS
      FD=PAR(1)
      FC=PAR(2)
      FDA=PAR(3)
      FCA=PAR(4)
      VDA=PAR(5)
      VCA=PAR(6)
      IBMAX=PAR(7)
      IBMIN=PAR(8)
      VDIODE=PAR(9)

      DUMMY=0.
C-----
C**** first and following calls in time step
      ELSE
        DUMMY=S(ISTORE)
C**** Set inputs
        VB=XIN(1)
        IB=XIN(2)
        F=XIN(3)
        VC=XIN(4)
        VD=XIN(5)

C**** check on discharge rate
        IF(IB.LT.0.)THEN
          IF(IB.LT.IBMIN)THEN
            FAIL=1
          ENDIF
        ELSE
          IF(IB.GT.IBMAX)THEN
            FAIL=2
          ENDIF
        ENDIF

C**** initially no restrictions are made, battery can either
C**** be charged or discharged
        IF(DUMMY.EQ.0.)THEN

C**** check on low limit of F and V
        IF((F.LT.FD).OR.(VB.LT.VD))THEN
C**** load will be disconnected from battery and from cell,
C**** but cell can still charge battery

```

```

        VLOAD=0.
        VCELL=VDIODE+VB
        DUMMY=1.
C****    check on high limit of voltage
        ELSEIF((F.GT.FC).OR.(VB.GT.VC))THEN
C****    cell will be disconnected from battery and load,
C****    battery will be discharged
        VCELL=-333.
C****    this is just a characteristic value that the cell
C****    recognizes that it is being disconnected
        VLOAD=VB
        DUMMY=2.
        ELSE
C****    no restrictions
        VCELL=VDIODE+VB
        VLOAD=VB
        ENDIF

        ELSEIF(DUMMY.EQ.1.)THEN
C****    battery can only begin to discharge again, when VB is
C****    greater than VDA and F is greater than FDA
        IF((F.LT.FDA).OR.(VB.LT.VDA))THEN
            VLOAD=0.
            VCELL=VDIODE+VB
        ELSE
C****    no restrictions
            VCELL=VDIODE+VB
            VLOAD=VB
            DUMMY=0.
        ENDIF

        ELSEIF(DUMMY.EQ.2.)THEN
C****    battery can only begin to charge again, when VB is
C****    less than VCA and F is less than FCA
        IF((F.GT.FCA).OR.(VB.GT.VCA))THEN
            VCELL=-333.
            VLOAD=VB
            DUMMY=2.
        ELSE
C****    no restrictions
            VCELL=VDIODE+VB
            VLOAD=VB
            DUMMY=0.
        ENDIF
        ENDIF
    ENDIF

    S(ISTORE)=DUMMY

C**** SET OUTPUTS

```

```

OUT(1)=VCELL
OUT(2)=VLOAD
OUT(3)=FAIL

```

```

END

```

Shunt Type Charge Controller: Part A

```

C*****
SUBROUTINE TYPE74(TIME,XIN,OUT,T,DT,PAR,INFO)
C   version from: 12/22/89
C***** Subroutine
represents a charge controller for a system including
C**** PV-array, load and battery storage.
C**** The controller represents a shunt type controller. A multi step
C**** control scheme is implemented. That means if the battery voltage
C**** exceeds the gassing voltage specified by the user, the current
C**** into the battery will be limited to the current corresponding
C**** to the gassing voltage. Excess energy is shunted through a
C**** dissipater.
C**** A blocking diode is included in the model to prevent that the
C**** battery is being discharged through the cell. It is assumed that
C**** voltage drop at the diode is constant throughout the simulation
C**** and just depends on the diode material used in the system.
C**** The user has to provide this information as a parameter.
C**** Another diode is included in the undervoltage protection
C**** device. This way the battery can be disconnected from the load,
C**** i.e. the battery won't be discharged, while the array can still
C**** charge the battery.
C*****
C**** variables:
C   F -- fractional State of Charge
C   FD -- discharge limit on F
C   FC -- charge limit on F
C   FDA -- F after which battery can be discharged again,
C         after being charged
C   FCA -- F after which battery can be charged again,
C         after being discharged
C   GUARD -- signal from undervoltage regulator
C   IB -- battery current [amps]
C   SIGNAL -- signals that undervoltage limit is exceeded
C   SUV -- signal to undervoltage regulator
C   VB -- battery voltage [volts]
C   VCA -- limit on voltage, above battery can again begin to charge
C         after being discharged
C   VCELL -- voltage send to cell
C   VC -- high limit on voltage, when battery charging-cutoff voltage
C   VDA -- limit on voltage, above battery can again begin to discharge

```


C after being charged
 C VDIODE -- voltage of diode
 C VD -- low limit on voltage, when battery discharging
 C VLOAD -- voltage send to load

```

IMPLICIT NONE
INTEGER INFO
INTEGER ISTORE,NSTORE,IAV
REAL TIME,XIN,OUT,T,DTDT,PAR,S
REAL VB,VD,VC,VDA,VCA,VDIODE
REAL VCELL,VLOAD,DUMMY
REAL SIGNAL,SUV,GUARD
REAL TB,F,FD,FC,FDA,FCA
DIMENSION XIN(7), OUT(5), PAR(6), INFO(10)

```

```

COMMON /STORE/ NSTORE,IAV,S(5000)

```

C**** store is used to store values from previous timestep

```

INFO(5)=5
INFO(9)=1

```

```

DUMMY=S(ISTORE)

```

C-----

C**** Initial call of component

```

IF(INFO(7).LT.0)THEN

```

C**** storage allocation

```

INFO(10)=1
CALL TYPECK(1,INFO,7,6,0)
ISTORE=INFO(10)

```

C**** Initialization of auxiliary variables used in secant

C**** method
 S(ISTORE)=0.

C**** SET PARAMETERS

```

VDA=PAR(1)
FD=PAR(2)
FC=PAR(3)
FDA=PAR(4)
FCA=PAR(5)
VDIODE=PAR(6)

```

```

DUMMY=0.

```

C-----

C**** first and following calls in time step

```

ELSE

```

C**** Following calls in time step

C**** Set inputs

```

VB=XIN(1)
VLOAD=XIN(2)
GUARD=XIN(3)

```

```

IB=XIN(4)
F=XIN(5)
VC=XIN(6)
VD=XIN(7)

IF(INFO(7).EQ.0)THEN
  IF(DUMMY.EQ.1)THEN
    DUMMY=11.
  ELSEIF(DUMMY.EQ.22)THEN
    DUMMY=0.
  ENDIF
ENDIF

C**** initially no restrictions are made, battery can either
C**** be charged or discharged
IF(DUMMY.EQ.0)THEN

C**** F checks
IF((F.GT.FC).AND.(IB.GT.0.))THEN
C**** very little current into battery
C**** current is shunted through a dissipative device
VCELL=VDIODE+VB
VLOAD=VB
SIGNAL=0.
SUV=2.
DUMMY=2.

  ELSEIF((F.LT.FD).AND.(IB.LT.0.))THEN
C**** no current out of battery
C**** direct coupled mode: array direct connected to load
VCELL=VDIODE+VLOAD
SIGNAL=1.
SUV=0.
DUMMY=1.

  ELSE

C**** check voltage
IF(VB.LT.VD)THEN
C**** satisfying the load is prior to charging the battery

  VCELL=VDIODE+VLOAD
SIGNAL=1.
SUV=0.
DUMMY=1.

  ELSEIF(VB.GT.VC)THEN
C**** current is shunted through a dissipative device
C**** to reduce the battery voltage: trickle charge

```

```

VCELL=VDIODE+VB
VLOAD=VB
SIGNAL=0.
SUV=3.
DUMMY=22.

ELSE
C****    no restrictions
VCELL=VDIODE+VB
VLOAD=VB
SIGNAL=0.
SUV=0.
ENDIF
ENDIF

ELSEIF(DUMMY.EQ.1.)THEN
C****    direct coupled mode; array direct connected to load
VCELL=VDIODE+VLOAD
SIGNAL=1.
SUV=0.

ELSEIF(DUMMY.EQ.11.)THEN
C****    try to run the system with battery
C****    battery is disconnected from load
VCELL=VDIODE+VDIODE+VB
VLOAD=VDIODE+VB
SIGNAL=0.
SUV=1.
DUMMY=12.

ELSEIF(DUMMY.EQ.12.)THEN
C****    try to run the system with battery
IF((F.LT.FDA).OR.(VB.LT.VDA))THEN
C****    battery is still disconnected from load

IF(GUARD.EQ.1.)THEN
C****    battery would be discharged; switch to
C****    direct coupled mode
VCELL=VDIODE+VLOAD
SIGNAL=1.
SUV=0.
DUMMY=1.
ELSE
C****    dummy=11 mode is continued
VCELL=VDIODE+VDIODE+VB
VLOAD=VDIODE+VB
SIGNAL=0.
SUV=1.
ENDIF
ELSE

```

```

C****    no restrictions
VCELL=VDIODE+VB
VLOAD=VB
SIGNAL=0.
SUV=0.
DUMMY=0.
ENDIF

ELSEIF(DUMMY.EQ.2.)THEN
C****    battery can only begin to charge again, when F is
C****    less than FCA
IF(B.GT.0)THEN
C****    battery is still on charge

IF(F.GT.FCA)THEN
C****    very little current into battery
C****    current is shunted through a dissipative device
VCELL=VDIODE+VB
VLOAD=VB
SIGNAL=0.
SUV=2.
DUMMY=2.

ELSE
IF(VB.GT.VC)THEN
C****    current is shunted through a dissipative device
C****    to reduce the battery voltage: trickle charge
VCELL=VDIODE+VB
VLOAD=VB
SIGNAL=0.
SUV=3.
DUMMY=22.

ELSE
C****    no restrictions
VCELL=VDIODE+VB
VLOAD=VB
SIGNAL=0.
SUV=0.
DUMMY=0.
ENDIF
ENDIF

ELSE
C****    no restrictions
VCELL=VDIODE+VB
VLOAD=VB
SIGNAL=0.
SUV=0.

```

```

        DUMMY=0.
    ENDIF

    ELSEIF(DUMMY.EQ.22.)THEN
C****    current is shunted through a dissipative device
C****    to reduce the battery voltage: trickle charge
        VCELL=VDIODE+VB
        VLOAD=VB
        SIGNAL=0.
        SUV=3.
        DUMMY=22.
    ENDIF
ENDIF
C-----
S(ISTORE)=DUMMY
C**** set outputs
    OUT(1)=VCELL.
    OUT(2)=VLOAD
    OUT(3)=SIGNAL.
    OUT(4)=SUV
    OUT(5)=DUMMY
END

Shunt Type Controller: Part B
C*****
SUBROUTINE TYPE75(TIME,XIN,OUT,T,DTDT,PAR,INFO)
C    version from: 12/22/89
C*****
C**** Subroutine represents a charge controller for a system including
C**** PV-array, load and battery storage.
C**** The controller represents a part of a shunt type controller:
C**** the undervoltage and overvoltage protection
C*****
C**** Variables:
C    IB -- battery current [amps]
C    SUV -- control signal: incoming
C    GUARD -- control signal: outgoing
C    IBMAX -- maximum battery current permitted
C    IBMIN -- minimum battery current permitted
C    FAIL -- message: =1 IBMIN is exceed
C             -2 IBMAX is exceed
C    IC -- current corresponding to VC [amps]
C    VC -- gassing voltage of the battery [volts]
C    VB -- battery voltage [volts]
C    IDISS -- dissipated current [amps]
C    VDISS -- voltage drop at dissipater [volts]
C    PDISS -- dissipated power [watts]
C*****

```



```

IMPLICIT NONE

INTEGER INFO
REAL TIME,XIN,OUT,T,DTDT,PAR
REAL IB,SUV,GUARD,IBMAX,IBMIN,FAIL
REAL IC,VC,VB,IDISS,VDISS,PDISS

DIMENSION XIN(5),PAR(2),OUT(4),INFO(10)

C*****

INFO(6)=4
INFO(9)=0

C**** PARAMETERS
IBMAX=PAR(1)
IBMIN=PAR(2)

FAIL=0.
C**** Set inputs
IB=XIN(1)
VB=XIN(2)
IC=XIN(3)
VC=XIN(4)
SUV=XIN(5)

IF(SUV.EQ.1.)THEN
C**** undervoltage protection
C**** check on IB
IF(IB.LT.0.)THEN
GUARD=1.
IB=0.
ELSE
GUARD=0.
ENDIF
ELSEIF(SUV.EQ.2.)THEN
C**** that is when battery SOC (upper limit) is exceeded
C**** current gets shunted through dissipater
IDISS=IB-0.1
VDISS=VB
IF(IDISS.LT.0.)THEN
IDISS=0.
VDISS=0.
ELSE
IB=0.1
ENDIF
ELSEIF(SUV.EQ.3.)THEN
C**** trickle charge at constant charge rate IC
IDISS=IB-IC
VDISS=VC

```

```

IF(IDISS.LT.0.)THEN
  IDISS=0.
  VDISS=0.
ELSE
  IB=IC
ENDIF

ELSEIF(SUV.EQ.0.)THEN
  GUARD=0.
ENDIF

C**** check on discharge rate
IF(IB.LT.IBMIN)THEN
  FAIL=1.
ELSEIF(IB.GT.IBMAX)THEN
  FAIL=2.
ENDIF

PDISS=IDISS*VDISS
C**** set outputs
OUT(1)=IB
OUT(2)=GUARD
OUT(3)=PDISS
OUT(4)=FAIL

END

```

Appendix B

TRNSYS DECKS

Direct-Coupled Systems

```

*****
*   PV-cell connected to a separately excited DC motor and a
*   centrifugal pump
*****
* Simulation starts at TIME 1 and will run 24 hours with a
* time step of 1
SIMULATION 1 24 1
*
WIDTH 80
* use relative tolerances
TOLERANCES .001 .001
*
LIMITS 60 10
*
EQUATIONS 3
SUN=[2,6]/3.6
SUNA=[2,6]/3.6*83.692
QHOUR=[6,3]*3600
*****
UNIT 1 TYPE 9 DATA READER (FORMATED)
PARAMETERS 13
*ND ELTATd HOURS IH TA LUNIT FORMATED
3 1 -1 1 0 -2 1 0 3 .1 273 1 1
(4X,F3.0,7X,F4.0,2X,F3.0)
*****
UNIT 2 TYPE 16 SOLAR RADIATION PROCESSOR
PARAMETERS 7
*RADMODE TRACKMOD N LAT SC SHFT IE
1 1 152 43.1 4871 0 -1
INPUTS 6
*I id1 id2 rhog beta gamma
1,2 1,19 1,20 0,0 0,0 0,0
0 0 0 0.2 40 0
*****

```

```

UNIT 3 TYPE 62 PV-CELL
PARAMETERS 9
*ISCR VOCCR TCR SUNRISE VMR IMR MISC MVOC NCS
2.9 20. 301. 1000. 16.5 2.67 1.325E-3 -77.5E-3 36
PARAMETERS 9
*NS NP TCNOCT TANOCCT SUNNOCT AREA TAU ALEG RS
14 10 319 293 800 0.427 .9 1.12 -1
INPUTS 4
*SUN TA V MODE
2.6 1.3 4.2 0.0
0 0 0 1
*****
LOOP 2 REPEAT 30
4 6
*****
UNIT 4 TYPE 66 DC-MOTOR
PARAMETERS 8
*TYPE NMAX IRAT IMAX KF CSTAT CVISC RA
1 70 20 25 .59 0.5 0.02 1.44 0.7
INPUTS 5
*I V N TM MODE
3.2 3.1 6.1 6.2 0.0
0 0 0 0 1
*****
UNIT 6 TYPE 68 PUMP
PARAMETERS 6
*K1 K2 NREF NMAX POFF QNOM
30.48 4.2104E5 50. 58.3 -1 15
INPUTS 1
*TI.
4.4
0
*****
UNIT 7 TYPE 25 PRINTER 1
PARAMETERS 4
*PRINT EVERY HOUR
1 1 24 7
INPUTS 6
3.1 3.2 3.3 3.4 3.5 SUN
V I P PMAX UTIL SUN
*****
UNIT 8 TYPE 25 PRINTER 2
PARAMETERS 4
1 1 24 9
INPUTS 5
6.2 6.1 QHOUR 6.4 6.5
TM N Q H ETA
*****
UNIT 9 TYPE 25 PRINTER 3
PARAMETERS 4

```

```

1 1 24 10
INPUTS 2
6,8 4,8
FAILP FAILM
*****
UNIT 10 TYPE 25 PRINTER 4
PARAMETERS 4
1 1 24 11
INPUTS 6
3,3 4,5 4,6 6,6 6,7 SUNA
PCELL PEL PMECHM PHYD PMECHM SUNA
*****
END

*****
* PV-array connected to a series DC motor and a
* centrifugal pump
*****
* Simulation starts at TIME 1 and will run 24 hours with a
* time step of 1
SIMULATION 1 24 1
*
WIDTH 80
* use relative tolerances
TOLERANCES .001 .001
*
LIMITS 60 10
*
EQUATIONS 3
SUN=[2,6]/3.6
SUNA=[2,6]/3.6*83.692
QHOUR=[6,3]*3600
*****
UNIT 1 TYPE 9 DATA READER (FORMATED)
PARAMETERS 13
*NDELTATdHOURS IH TA IUNIT FORMATED
3 1 -1 1 0 -2 1 0 3.1 273 1 1
(4X,F3.0,7X,F4.0,2X,F3.0)
*****
UNIT 2 TYPE 16 SOLAR RADIATION PROCESSOR
PARAMETERS 7
*RADMODE TRACKMOD N LAT SC SHIFT IE
1 1 152 43.1 4871 0 -1
INPUTS 6
*I id1 id2 rhog beta gamma
1,2 1,19 1,20 0,0 0,0 0,0
0 0 0 0.2 40 0
*****

```



```

UNIT 3 TYPE 62 PV-CELL
PARAMETERS 9
*ISCR VOCR TCR SUNREF VMR IMR MISC MVOC NCS
2.9 20. 301.1000. 16.5 2.67 1.325E-3 -77.5E-3 36
PARAMETERS 9
*NS NP TCNOCT TANOCCT SUNNOCT AREA TAU ALPH RS
14 10 319 293 800 0.427 9 1.12 -1
INPUTS 4
*SUNTA V MODE
2,6 1,3 4,2 0,0
0 0 0 1
*****
LOOP 2 REPEAT 30
4 5
*****
UNIT 4 TYPE 66 DC-MOTOR
PARAMETERS 9
*TYPENMAX IRAT IMAX KF CSTAT CVISC RA RF
2 70 20 25 .0275 0.5 0.02 1.44 0.7
INPUTS 5
*I V N TM MODE
3,2 3,1 6,1 6,2 0,0
0 0 0 0 1
*****
UNIT 6 TYPE 68 PUMP
PARAMETERS 6
*K1 K2 NREF NMAX POFF QNOM
30.48 4.2104E5 50. 58.3 -1 15
INPUTS 1
*TL
4,4
0
*****
UNIT 7 TYPE 25 PRINTER 1
PARAMETERS 4
*PRINT EVERY HOUR
1 1 24 7
INPUTS 6
3,1 3,2 3,3 3,4 3,5 SUN
V I P PMAX UTIL SUN
*****
UNIT 8 TYPE 25 PRINTER 2
PARAMETERS 4
1 1 24 9
INPUTS 5
6,2 6,1 QHOUR 6,4 6,5
TM N Q II ETA
*****
UNIT 9 TYPE 25 PRINTER 3
PARAMETERS 4

```

```

1 1 24 10
INPUTS 2
6,8 4,8
FAILP FAILM
*****
UNIT 10 TYPE 25 PRINTER 4
PARAMETERS 4
1 1 24 11
INPUTS 6
3,3 4,5 4,6 6,6 6,7 SUNA
PCELL PEL PMECHM PHYD PMECHM SUNA
*****
END

```

Systems with Battery Storage

```

*****
*   PV-cell connected with a DC motor, a centrifugal pump,
*   a battery and a series type charge controller
*****
* Simulation starts at 1st of June and will run 48 hours with a
* time step of one
SIMULATION 1 48 1
*
WIDTH 80
* use absolute tolerances
TOLERANCES .001 .001
*
LIMITS 100 10
*
EQUATIONS 7
NS=14
NP=20
AREA=0.427
IBAT=[3,2]-[4,1]
SUN=[2,6]/3.6
QHOUR=[6,3]*3600
SUNA=[2,6]/3.6*NS*NP*AREA
*****
UNIT 1 TYPE 9 DATA READER (FORMATED)
PARAMETERS 13
*NDELTATdHOURS IH TA LUNIT FORMATED
3 1 -1 1 0 2 1 0 3 1 273 1 1
(4X,F3.0,7X,F4.0,2X,F3.0)
*****
UNIT 2 TYPE 16 SOLAR RADIATION PROCESSOR
PARAMETERS 7
*RADMODE TRACKMOD N LAT SC SHFT IE
1 1 152 43.1 4871 0 -1

```

```

INPUTS 6
*I id1 id2 rhog beta gamma
1.2 1.19 1.20 0.0 0.0 0.0
0 0 0 0.2 40 0
*****

UNIT 5 TYPE 70 BATTERY (250 AH lead acid)
PARAMETERS 7
*QM CP CS EFF VC VD ICTOL
250 2 102 0.95 2.3 -1 0.01
PARAMETERS 7
*ESC ESD GC GD MC MD ED
2.25 2.10 0.08 0.08 0.864 1. 1.8
PARAMETERS 7
*RD IDI KDI QC QD RSC RSD
2.4E-3 2.5 29.3 -8.75 294.12 0.012 0.002
INPUTS 1
*IBAT
IBAT
15.0
DERIVATIVES 1
250.
*****

UNIT 14 TYPE 73 SERIES CHARGE CONTROLLER
PARAMETERS 9
*FD FC FDA FCA VDA VCA IBMAX IBMIN VDIODE
0.7 1 0.72 0.98 223 215 40 40 0.7
INPUTS 5
*VB IB F VC VD
5.6 5.5 5.2 5.8 5.7
0 0 0 0 0
*****

UNIT 3 TYPE 62 PV-CELL
PARAMETERS 9
*ISCR VOCR TCR SUNREF VMR IMR MISC MVOC NCS
2.9 20. 301. 1000. 16.5 2.67 1.325E-3 -77.5E-3 36
PARAMETERS 9
*NS NP TCNOCT TANOCT SUNNOCT AREA TAUALEG RS
NS NP 319 293 800 0.427 .9 1.12 -1
INPUTS 4
*SUN TA V MODE
2.6 1.3 14.1 0.0
0 0 0 0
*****

LOOP 2 REPEAT 50
4 6
*****

UNIT 4 TYPE 66 DC-MOTOR
PARAMETERS 8
*TYPE NMAX IRAT IMAX KP CSTAT CVISC RA

```

```

1  70  20  30  .59 0.5  0.02  1.44
INPUTS 5
*I V N TM MODE
0,0  14,2  6,1  6,2  0,0
0  0  0  0  0
*****
UNIT 6 TYPE 68 PUMP
PARAMETERS 6
*K1 K2 NREF NMAX POFF QNOM
30.48 4.2104E5 50. 65 -1 15
INPUTS 1
*TL
4,4
0
*****
UNIT 8 TYPE 25 PRINTER 1
PARAMETERS 4
*PRINT EVERY HOUR
1 1 48 7
INPUTS 6
3,1 3,2 3,3 3,4 3,5 SUN
V I P PMAX UTIL SUN
*****
UNIT 9 TYPE 25 PRINTER 2
PARAMETERS 4
*PRINT EVERY HOUR
1 1 48 8
INPUTS 5
3,1 4,2 5,6 5,1 5,2
VCELL VLOAD VBAT SOC F
*****
UNIT 11 TYPE 25 PRINTER 3
PARAMETERS 4
1 1 48 11
INPUTS 5
6,2 6,1 QHOUR 6,4 6,5
TM N Q H ETA
*****
*UNIT 13 TYPE 25 PRINTER 4
*PARAMETERS 4
*1 1 48 13
*INPUTS 6
*3,3 4,5 4,6 6,6 6,7 SUNA
*PCELL PEL PMECHM PHYD PMECHM SUNA
*****
UNIT 13 TYPE 25 PRINTER 4
PARAMETERS 4
1 1 48 13
INPUTS 4
3,5 SUN QHOUR 5,2

```

UTILSUNQHOUR I'

END

* PV-cell connected with a DC motor, a centrifugal pump,
* a battery and a shunt type charge controller

* Simulation starts at 1st of June and will run 48 hours with a

* time step of one

SIMULATION 1 48 1

*

WIDTH 80

* use absolute tolerances

TOLERANCES .001 .001

*

LIMITS 100 10

*

EQUATIONS 7

NS=14

NP=20

AREA=0.427

IBAT=[3,2]-[4,1]

SUN=[2,6]/3.6

QHOUR=[6,3]*3600

SUNA=[2,6]/3.6*NS*NP*AREA

UNIT 1 TYPE 9 DATA READER (FORMATED)

PARAMETERS 13

*NDELTATd HOURS IH TA LUNIT FORMATED

3 1 -1 1 0 -2 1 0 3.1 273 1 1

(4X,F3.0,7X,F4.0,2X,F3.0)

UNIT 2 TYPE 16 SOLAR RADIATION PROCESSOR

PARAMETERS 7

*RADMODE TRACKMOD N LAT SC SHFT IE

1 1 152 43.1 4871 0 -1

INPUTS 6

*I id1 id2 rhog beta gamma

1,2 1,19 1,20 0,0 0,0 0,0

0 0 0 0.2 40 0

UNIT 5 TYPE 70 BATTERY (250 AH lead acid)

PARAMETERS 7

*QM CP CS EFF VC VD ICTOL

250 2 102 0.95 2.3 -1 0.01

PARAMETERS 7

*ESC ESD GC GD MC MD ED


```

2.25 2.10 0.08 0.08 0.864 1. 1.8
PARAMETERS 7
*RD IDI KDI QC QD RSC RSD
2.4E-3 2.5 29.3 -8.75 294.12 0.012 0.002
INPUTS 1
*IBAT
18.1
15.0
DERIVATIVES 1
250.
*****
UNIT 16 TYPE 74 SHUNT CHARGE CONTROLLER PART A
PARAMETERS 6
*VDA FD FC FDA FCA VDIODE
223 0.7 0.99 0.72 0.98 0.7
INPUTS 7
*VH VLOAD GUARD IH F VC VD
5.6 4.2 18.2 5.5 5.2 5.8 5.7
0 0 0 0 0 0 0
*****
UNIT 3 TYPE 62 PV-CELL
PARAMETERS 9
*ISCR VOCR TCR SUNREF VMR IMR MISC MVOC NCS
2.9 20. 301. 1000. 16.5 2.67 1.325E-3 -77.5E-3 36
PARAMETERS 9
*NS NP TCNOCT TANOC T SUNNOCT AREA TAUALEG RS
NS NP 319 293 800 0.427 .9 1.12 -1
INPUTS 4
*SUNTA V MODE
2.6 1.3 16.1 16.3
0 0 0 0
*****
LOOP 2 REPEAT 50
4 6
*****
UNIT 4 TYPE 66 DC-MOTOR
PARAMETERS 8
*TYPE NMAX IRAT I MAX KP CSTAT CVISC RA
1 70 20 30 .59 0.5 0.02 1.44
INPUTS 5
*I V N TM MODE
3.2 16.2 6.1 6.2 16.3
0 0 0 0 0
*****
UNIT 6 TYPE 68 PUMP
PARAMETERS 6
*K1 K2 NRIEF NMAX POFF QNOM
30.48 4.2104E5 50. 65 -1 15
INPUTS 1
*TL

```

```

4,4
0
*****
UNIT 18 TYPE 75 SHUNT CHARGE CONTROLLER PART B
PARAMETERS 2
*IBMAX IBMIN
40 -40
INPUTS 5
*IB VB IC VC SUV
IBAT 5,6 5,9 5,8 16,4
0 0 0 0 0
*****
UNIT 8 TYPE 25 PRINTER 1
PARAMETERS 4
*PRINT EVERY HOUR
1 1 48 7
INPUTS 6
3,1 3,2 3,3 3,4 3,5 SUN
V I P PMAX UTIL SUN
*****
UNIT 9 TYPE 25 PRINTER 2
PARAMETERS 4
*PRINT EVERY HOUR
1 1 48 8
INPUTS 5
3,1 4,2 5,6 5,1 5,2
VCELL VLOAD VBAT SOC F
*****
UNIT 11 TYPE 25 PRINTER 3
PARAMETERS 4
1 1 48 11
INPUTS 5
6,2 6,1 QHOUR 6,4 6,5
TM N Q H ETA
*****
*UNIT 13 TYPE 25 PRINTER 4
*PARAMETERS 4
*1 1 48 13
*INPUTS 6
*3,3 4,5 4,6 6,6 6,7 SUNA
*PCELL PEL PMECHM PHYD PMECHM SUNA
*****
UNIT 13 TYPE 25 PRINTER 4
PARAMETERS 4
1 1 48 13
INPUTS 4
3,5 SUN QHOUR 5,2
UTIL SUN QHOUR F
*****
END

```

System with Battery Storage and Maximum Power Tracking

```

*****
*      PV-cell connected with a max. power point tracker, a DC motor, a centrifugal
*      pump, a battery and a series type charge controller
*****
* Simulation starts at 1st of June and will run 24 hours with a
* time step of one
SIMULATION 1 24 1
*
WIDTH 80
* use absolute tolerances
TOLERANCES .001 .001
*
LIMITS 100 10
*
EQUATIONS 7
NS=14
NP=20
AREA=0.427
IBAT=[3,2]-[4,1]
SUN=[2,6]/3.6
QHOUR=[6,3]*3600
SUNA=[2,6]/3.6*NS*NP*AREA
*****
UNIT 1 TYPE 9 DATA READER (FORMATED)
PARAMETERS 13
*NDELTATd HOURS IH TA LUNIT FORMATED
3 1 -1 10 -2 10 3.1273 1 1
(4X,F3.0,7X,F4.0,2X,F3.0)
*****
UNIT 2 TYPE 16 SOLAR RADIATION PROCESSOR
PARAMETERS 7
*RADMODE TRACKMOD N LAT SC SHIFT IE
1 1 152 43.14871 0 -1
INPUTS 6
*I td1 td2 rhog beta gamma
1,2 1,19 1,20 0,0 0,0 0,0
0 0 0 0.2 40 0
*****
UNIT 3 TYPE 70 BATTERY (250 AH lead acid)
PARAMETERS 7
*QM CP CS BFF VC VD ICTOL
250 3 102 0.95 2.3 -1 0.01
PARAMETERS 7
*ESC ESD GC GD MC MD ED
2.25 2.10 0.08 0.08 0.864 1, 1.8

```

```

PARAMETERS 7
*RD IDI KDI QC QD RSC RSD
2.4E-3 2.5 29.3 -8.75 294.12 0.012 0.002
INPUTS 1
*IBAT
IBAT
15.0
DERIVATIVES 1
200.
*****
UNIT 14 TYPE 73 SERIES CHARGE CONTROLLER
PARAMETERS 9
*FD FC FDA FCA VDA VCA IBMAX IBMIN VDIODE
0.6 1 0.63 0.98 223 215 40 -40 0.7
INPUTS 5
*VB IB F VC VD
5,5 5,5 5,2 5,8 5,7
0 0 0 0 0
*****
UNIT 3 TYPE 62 PV-CELL
PARAMETERS 9
*ISCR VOCT TCR SUNREF VMR IMR MISC MVOC NCS
2.9 20. 301. 1000. 16.5 2.67 1.325E-3 -77.5E-3 36
PARAMETERS 9
*NS NP TCNOCT TANOCCT SUNNOCT AREA TAUALEG RS
NS NP 319 293 800 0.427 .9 1.12 -1
INPUTS 4
*SUNTA V MODE
2.6 1.3 0.0 0.0
0 0 0 0
*****
UNIT 15 TYPE 65 MAXIMUM POWER TRACKER
PARAMETERS 1
*EPF
0.98
INPUTS 4
*IMAX VMAX VB MODE
3.7 3.6 14.1 0.0
0 0 0 0
*****
LOOP 2 REPEAT 50
4 6
*****
UNIT 4 TYPE 66 DC-MOTOR
PARAMETERS 8
*TYPE NMAX IRAT IMAX KF CSTAT CVISC RA
1 70 20 30 .59 0.5 0.02 1.44
INPUTS 5
*I V N TM MODE
0.0 14.2 6.1 6.2 0.0

```

```

0 0 0 0 0
*****
UNIT 6 TYPE 68 PUMP
PARAMETERS 6
*K1 K2 NREF NMAX POFF QNOM
30.48 4.2104E5 50. 65 -1 15
INPUTS 1
*TL
4,4
0
*****
UNIT 8 TYPE 25 PRINTER 1
PARAMETERS 4
*PRINT EVERY HOUR
1 1 96 7
INPUTS 6
3,1 3,2 3,3 3,4 3,5 SUN
V I P PMAX UTIL SUN
*****
UNIT 9 TYPE 25 PRINTER 2
PARAMETERS 4
*PRINT EVERY HOUR
1 1 96 8
INPUTS 5
3,1 4,2 5,6 5,1 5,2
VCELL VLOAD VBAT SOC F
*****
UNIT 11 TYPE 25 PRINTER 3
PARAMETERS 4
1 1 96 11
INPUTS 5
6,2 6,1 QHOUR 6,4 6,5
TM N Q II ITA
*****
*UNIT 13 TYPE 25 PRINTER 4
*PARAMETERS 4
*1 1 96 13
*INPUTS 6
*3,3 4,5 4,6 6,6 6,7 SUNA
*PCELL PEL PMECHM PHYD PMECHM SUNA
*****
UNIT 13 TYPE 25 PRINTER 4
PARAMETERS 4
1 1 96 13
INPUTS 4
3,5 SUN QHOUR 5,2
UTIL SUN QHOUR F
*****
END

```

Appendix C

SIMULATION DATA

This Appendix contains the data used for the simulations performed in Chapters 2, 3, 4, and 5.

Motor - Centrifugal Fan Data

	Series	Sep. excited
RA [ohms]	1.5	1.5
RF [ohms]	0.7	n/a
$k\phi$ [Vs]	n/a	0.621
MAF [henry]	0.0675	n/a
n-rated [1/s]	25	25

The coefficients for the fan torque-speed relation according to equation (3.3.15) are:

$$a = 0.3 \quad b = 0.00039 \quad c = 1.8$$

The static and viscous friction components of the motor are:

$$c_{\text{stat}} = 0.2 \text{ Nm} \quad c_{\text{visc}} = 0.015 \text{ Nm*s}$$

Motor - Centrifugal Pump Data

	Series	Sep. excited
RA [ohms]	1.44	1.44
RF [ohms]	0.7	n/a
$k\phi$ [Vs]	n/a	0.59
MAF [henry]	0.0275	n/a
n-rated [1/s]	38.4	38.4

The static and viscous friction components of the motor are:

$$c_{\text{stat}} = 0.5 \text{ Nm} \quad c_{\text{visc}} = 0.02 \text{ Nm*s}$$

The Pump data are read from Figure 3.14. The two following tables contain the head-flowrate and the efficiency-flowrate profiles at a reference speed of 3000 Rpm.

Q [m ³ /s]	Head [m]
0	37.795
0.00063	37.49
0.00126	36.881
0.00189	36.271
0.00252	35.357
0.00315	34.138
0.00378	32.309
0.00441	29.566
0.00504	26.822
0.00567	22.86

Q [m ³ /s]	efficiency
0.002019	0.45
0.002587	0.5
0.003218	0.55
0.004354	0.58
0.005363	0.55
0.005742	0.5

PV Array Data for a Single Module

	Solarex MSX-30	Kyocera
ISCRBF	1.82	2.9
VOCREF	21.3	20
TCREF	298	301
Φ_{REF}	1000	1000
VMPREF	17.8	16.5
IMPREF	1.68	2.67
μ_{ISC}	0.0015	0.001325
μ_{VOC}	-0.073	-0.0775
TCNOCT	318	319
Φ_{NOCT}	1000	800
TANNOCT	293	293
ϵ_G	1.12	1.12
Area-module	0.259	0.427

The parameters for a lead-acid battery are taken from *TRNSYS* [2].

E_{SC}	= 2.25 V	M_D	= 1.0
E_{SD}	= 2.10 V	E_D	= 1.8 V
G_C	= 0.08	R_D	= 2.4E-3 ohms
G_D	= 0.08	I_{DI}	= 2.5 amps
M_C	= 0.864	K_{DI}	= 29.3

The following parameters depend on the size of the battery and can be obtained using the proposed relations [2]:

$$\begin{aligned}
 Q_C &= -0.035 Q_M & Q_D &= \frac{Q_M}{0.85} \\
 R_{SC} &= \frac{3.0}{Q_M} & R_{SD} &= \frac{0.5}{Q_M}
 \end{aligned}$$

For all simulations, the rated capacity, Q_M , was taken to be 250 ampere-hours and the charging efficiency was assumed to be 0.95.

Appendix D

COMPARISON DATA

This Appendix contains the data for the comparison between the simulations and the experiments conducted at the Florida Solar Energy Center.

Pump-Motor Data

The motor parameters were obtained from measured I-V motor-pump curves and the rated motor data. Simulations were run for two different sets of motor parameters (indicated as estimated - 1 and estimated - 2; see also Chapter 6). The pump performance data were given in a combined form together with the motor data. The head-flowrate profiles were given as a function of voltage and electric power. To run simulations, the pump data are required in an explicit form (as head-flowrate and efficiency-flowrate profiles for a reference speed). The motor-pump relations derived in Chapter 3 were used to make the data compatible to the requirements of the simulations. Therefore, two different sets of pump performance data are given corresponding to the two different sets of motor parameters.

rated permanent magnet motor data: 36 V-DC, 1500 Rpm, 1/2 Hp

motor parameters

estimated - 1: $RA = 0.43$ $k\phi = 0.188$

estimated - 2: $RA = 0.59$ $k\phi = 0.173$

The motor loss coefficients were assumed to be: $c_{\text{stat}} = 0.25 \text{ Nm}$ $c_{\text{visc}} = 0.011 \text{ Nms}$

Pump performance data for estimated - 1:

Q [m ³ /s]	Head [m]	efficiency
0.000208	18.5	0.24
0.00049	17.5	0.37
0.000764	15	0.43
0.000903	14	0.42
0.00118	10	0.32
0.0014	7	0.22

Pump performance data for estimated - 2:

Q [m ³ /s]	Head [m]	efficiency
0.00025	17.5	0.33
0.00044	17	0.41
0.000628	16	0.44
0.000903	14	0.34
0.001183	8.5	0.27
0.001389	4	0.15

The pump performance data are provided at the reference speed of 1500 Rpm.

PV Array

Single module ratings:

$$T_{\text{CREF}} = 50^{\circ}\text{C}$$

$$V_{\text{MPREF}} = 13.56 \text{ V}$$

$$\Phi_{\text{REF}} = 1000 \text{ W/m}^2$$

$$I_{\text{SCREF}} = 4.87 \text{ amps}$$

$$V_{\text{OCREF}} = 18.0 \text{ V}$$

$$I_{\text{MPREF}} = 4.32 \text{ amps}$$

the following parameters were assumed

$$T_{\text{CNOCT}} = 319^{\circ}\text{K}$$

$$\mu_{\text{ISC}} = 3.e-3 \text{ A/K}$$

$$T_{\text{ANOCT}} = 293^{\circ}\text{K}$$

$$\mu_{\text{VOC}} = -75.5e-3 \text{ V/K}$$

$$\Phi_{\text{NOCT}} = 800 \text{ W/m}^2$$

$$\text{NCS} = 36$$

$$\text{AREA} = 0.720 \text{ m}^2$$

$$\tau\alpha_{\text{AVE}} = 0.9$$

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