

**AUTOMATED GENERATION OF  
HOURLY DESIGN SEQUENCES**

by

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## Abstract

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The influence of climatic conditions on building structures can be significant. For example, outdoor air dry bulb temperature influences transmission gains and losses through the building envelope, ventilation sensible loads, and performance of air cooled heat pumping systems. The magnitude and variation of outdoor air humidity has an influence on moisture migration through building envelopes and ventilation latent loads. The character of wind (speed and direction) can significantly influence building envelope infiltration rates. Extreme sequences of solar radiation are important due to its influence on building envelope heat gains and solar gains through building fenestration systems.

To evaluate a specific design, a sequence of intervals on the order of the system's time constant is needed. Extreme hourly weather data, are readily available but are only appropriate when thermal capacitance effects are negligible. In addition, "binned" data are of limited usefulness since the temporal nature of the weather data is lost. Examination of long term hourly data could be computationally difficult because the set may be 30 or more years. If a suitable reporting location is not available, interpolation between stations may be required, introducing additional uncertainty into the energy calculations.

To alleviate these difficulties a methodology and a computer program are developed to synthesize extreme weather sequences of dry bulb temperature, humidity ratio, wind speed and total horizontal radiation for a given time of the year, location and sequence duration from one to seven days using readily available data as inputs.

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## Nomenclature<sup>\*</sup>

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$A$	Daily amplitude or $(T_{\text{high}} - T_{\text{low}})_{\text{day}}$
$a_t$	White noise process
$H$	Total daily radiation
$H_o$	Total daily extraterrestrial radiation
$I$	Total hourly radiation
$k_T$	Hourly clearness index
$K_T$	Daily clearness index
$\bar{K}_T$	Average monthly clearness index
$long$	Longitude
$R^2$	Coefficient of determination
$Range$	$(\bar{T}_{\max, \text{mon}} - \bar{T}_{\min, \text{mon}})$
$r_t$	Ratio of total radiation in an hour to total in a day
$s$	Standard deviation of the residuals
Skew Index	$\frac{(\bar{T}_{\text{mon}} - \bar{T}_{\text{yr}})}{Range}$
$\bar{T}_{\max, \text{day}}$	Daily average dry bulb temperature for an extreme hot day
$\bar{T}_{\max, \text{mon}}$	Highest monthly average dry bulb temperature for the year
$\bar{T}_{\min, \text{day}}$	Daily average dry bulb temperature for an extreme cold day

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\* This list contains most, but not all, of the nomenclature used within this thesis. Some additional symbols are defined locally.

$\bar{T}_{\min,mon}$	Lowest monthly average dry bulb temperature for the year
$\bar{T}_{mon}$	Monthly average dry bulb temperature
$T_{sa,max}$	Dry bulb temperature coincident with maximum stand alone humidity ratio
$\bar{T}_{yr}$	Average annual dry bulb temperature
xxxxy	Location and month i.e. alb01 is Albuquerque, NM for the month of January
$z$	Elevation
$f$	Latitude, AR(1) coefficient
$s_{yr}$	Standard deviation of $\bar{T}_{mon}$
$w$	Hour angle
$w_s$	Sunset hour angle
$v_{mon}$	Average monthly humidity ratio
$w_{coin,max}$	Humidity ratio (*1000) coincident with maximum dry-bulb temperature
$w_{sa,max}$	Maximum average stand-alone humidity ratio (*1000)
$w_t$	humidity ratio at time $t$

## Chapter 1

### Introduction

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#### 1.1 Motivation

The objective of this research project is to develop algorithms to synthesize hourly extreme or design weather sequences, such as a series of unusually hot, humid days. These design sequences are important in the context of designing energy efficient buildings and properly sizing HVAC equipment to serve those buildings. When used in conjunction with an energy simulation package such as TRNSYS [1996], DOE-2 [1997] or BLAST [1990] extreme weather sequences will allow architects and engineers to better determine optimal sizing and operation of HVAC equipment.

The influence of climatic conditions on building structures can be significant. For example, outdoor air dry bulb temperature influences transmission gains and losses through the building envelope, ventilation sensible loads, and performance of air cooled heat pumping systems. The magnitude and variation of outdoor air humidity has an influence on moisture migration through building envelopes and ventilation latent loads. The character of wind (speed and direction) can significantly influence building envelope infiltration rates. Extreme sequences of solar radiation are important due to its influence on building envelope heat gains and solar gains through building fenestration systems.

If the extreme sequences can be confidently estimated for a given location the increased costs associated with under-sizing or over-sizing equipment may be avoided. A methodology and a computer program are developed to synthesize extreme weather

sequences of dry bulb temperature, humidity ratio, wind speed and total horizontal radiation for a given time of the year, location and sequence duration from one to seven days.

## 1.2 Weather Data Sources

Long-term weather hourly data are available for many locations from numerous sources, among them are:

- National Renewable Energy Laboratory - (NREL)
- Canadian Weather Energy and Engineering Data Set - (CWEEDS)
- National Climatic Data Center - (NCDC).

The Solar and Meteorological Surface Observation Network (SAMSON) CD produced jointly by the National Climatic Data Center (NCDC) and the National Renewable Energy Laboratory (NREL) contains thirty years of hourly (or every 3 hours) data from 1961 through 1990. This CD contains meteorological elements from 237 stations in the United States, Guam and Puerto Rico. The data used in this project are from the SAMSON database.

The CWEEDS (Canadian Weather Energy and Engineering Data Sets) database contains 143 Canadian locations.

NCDC (National Climatic Data Center) issues monthly and annual summaries observed of extreme dry-bulb temperatures, and average dew-point and wet-bulb temperatures as well as other parameters.

### 1.2.1 Weather Data Sets

Weather data sets used as inputs to the various energy simulation programs normally include a full year of data and at least the following parameters:

- dry-bulb temperature
- humidity
- solar radiation

- wind speed
- station pressure.

In the past, hourly data sets that may be appropriate for design evaluation were not readily available. Normally, only extreme hourly weather data, such as that found in the ASHRAE Handbook of Fundamentals [1993], for a limited number of locations were readily available. Monthly extreme values and annual summaries are available from NOAA. In addition, “binned” data are compiled in Engineering Weather Data [1978]. Since the temporal nature of the weather data is lost in averaged or “binned” data, the value of these of data are limited and only appropriate when thermal capacitance effects are negligible (very light structures). If a suitable reporting location is not available, interpolation between stations may be required, introducing additional uncertainty into the energy calculations.

If the designer requires an extreme weather sequence to evaluate a particular building, HVAC component or system where thermal capacitance are significant a minimum of two steps are required. First, the designer would determine what constitutes an extreme sequence for the particular loads involved. Second, the available weather data is examined for the appropriate geographical location. Examination of the data could be computationally difficult because the set may be 30 or more years of hourly data. Obviously, this is a labor-intensive operation and due to this, a number of techniques have evolved. Among these, is the development of various weather data sets for use with energy simulation programs. These data sets are normally a year long since annual energy cost is a common metric output by energy simulation programs. Typically these data sets represent either average years, **Test Reference Year**, (TRY) [NCDC, 1976] or a year composed of average months, **Typical Meteorological Year**, (TMY/TMY2) [NCDC, 1981, NREL 1995] using long term data.

Other formats are available for specialized applications such as **California Thermal Zones** (CTZ) [CEC 1992, 1994] developed for Title 24 energy regulations. The latest format, **Weather Year for Energy Calculations (WYEC/WYEC2)** [ASHRAE 1985, Perez 1992] attempts to incorporate typical weather patterns rather than straight long-term averages.

None of the previously mentioned formats specifically contains extreme sequences. Crawley et al. [1997] compared the use of these artificial data to actual weather data. Crawley et al. extracted actual years from the SAMSOM data base that represented the maximum, average, median and minimum data for temperature, heating and cooling degree-days and solar radiation along with 99% (winter) and 2.5% (summer) design temperature values for 6 locations representing a variety of climates. The comparison found that the energy consumption due to actual weather variation was as much as +7.0%/-11.0% compared to the long-term average data. They also found that no data format consistently outperformed the others, as far as approaching the long-term average conditions. In addition, the WYEC2 format more closely matched the design temperatures and degree-days while the TMY format provided a closer match for the solar radiation. Finally, they recommend that future data formats create three separate years of data. An average year, a cold/cloudy year and a hot/sunny year. This approach would allow the designer to assess influences of weather variability on their designs. This does not, of course, guarantee that the hot or cold year will contain an extreme sequence for a given load.

### **1.3 Extreme Sequences – Prior Work**

The above data formats consist of one year of hourly data. To evaluate a specific design, a sequence of intervals on the order of the system's time constant is needed. Since most buildings and their HVAC systems have time constants of less than a few days, this

would normally be less than a 7-day extreme sequence. ASHRAE recognized the need for extreme weather sequences and initiated a research project to abstract such sequences from long-term hourly data sets (RP-828). As part of RP-828, Colliver et al. [1996] abstracted extreme sequences from actual long-term data for 239 US locations (SAMSON) and 143 Canadian locations (CWEEDS). Colliver et al. identified hourly 1, 3, 5 and 7 day sequence lengths for high and low dry-bulb temperature, high enthalpy, high dew-point temperature and low wet-bulb depression. Sequences were found for the extreme and the 0.4, 1.0 and 2.0% annual frequency of occurrence. Extreme wind and solar radiation sequences were not identified in this study. These sequences were then extracted and stored on a CD-ROM database. The extreme sequence database is accessed through a graphical user interface (GUI) front-end.

## 1.4 Data Used for Extreme Sequence Generation

For the purposes of the current research project, the following 30 year hourly data was retrieved from the SAMSON data base for 7 development and 7 test locations (Table 1) for the months of January, March, July and October:

- dry-bulb temperature
- dew point temperature
- relative humidity
- station pressure
- total horizontal radiation.

The seven development locations were chosen to represent a range of typical continental US climate types such as the coastal and mid-continental regions and will be used to formulate regression equations. The seven independent test locations attempt to provide the same climate diversity as the

development locations and are used as a means of independently testing the regressions developed.

The months selected attempt to capture, both the maximum and minimum values of temperature, humidity, wind and solar radiation as well as the maximum variation in those parameters over a one to seven day sequence.

To make the extreme sequence weather generator practical, the data required by the program must be readily available for any location. This requirement severely limits the number of parameters that are available to estimate the extreme sequence. The variables selected, based on the above criteria, are:

- latitude
- longitude
- elevation
- average monthly dry-bulb temperature
- average monthly total horizontal solar radiation (monthly clearness index)
- average humidity ratio
- windspeed.

<b>Development Locations</b>	<b>Test Locations</b>
Albuquerque, NM	Charleston, SC
Atlanta, GA	Chicago, IL
Baltimore, MD	Kansas, MS
Houston, TX	Los Angeles, CA
Madison, WI	New York, NY
Miami, FL	San Francisco, CA
Seattle, WA	West Palm Beach, FL

**Table 1.1 – Development and Test Locations**

## 1.5 Report Organization

A number of possible methods for evaluating and determining an extreme sequence for particular weather parameters are explored. Then the extreme dry-bulb temperature

sequences are identified and characterized followed by humidity ratio, solar radiation and windspeed.

## Chapter2

### Extreme Sequences

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In order to find the extreme sequence for each weather parameter, first the sequence or data window must be defined and then a method must be specified to evaluate each sequence for ranking. The parameters utilized are dry-bulb temperature, humidity ratio, total global solar radiation and wind speed. Three methods, called data filters, are examined to rank each possible data window for a given data set. The effect of the particular data filter and the series ranking are explored. Once the series are ranked, a decision as to what comprises an extreme series must be made.

#### 2.1 Extreme Sequences Parameters

##### 2.1.1 Data Windows

Consider the following ordered series of observations or time series:

$$\dots Y_{t-3}, Y_{t-2}, Y_{t-1}, Y_t, Y_{t+1}, Y_{t+2}, Y_{t+3} \dots$$

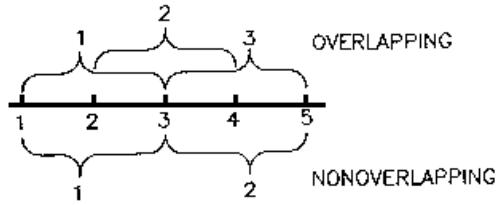
where:

$Y$  = any weather parameter

$t$  = time index, hour from the beginning of the series

Any contiguous sequence of this parameter is defined as a data window. Two types of data windows are possible:

- consecutive, non-overlapping window [NO]
- consecutive, overlapping or sliding window [O].



**Figure 2.1 – Data Window Types**

The data in each non-overlapping window cannot be used in another window, while overlapping or sliding windows share data as illustrated in Figure 2.1. A further consideration concerning the overlapping data window is whether the same data should be used in windows greater than 24 hours. If a particular hour of data is limited to one occurrence within a ranked series such a series is called an exclusive, overlapping data window.

### 2.1.2 Data Filters

Three data filters were investigated by Colliver et al.[1996] to determine which filter produced the greatest extreme for a given set of data. The following filters were examined:

- mean of hourly values [M]
- root mean squared deviation [RMS]
- mean non-steady state heat flow (transfer function method) [C].

#### 2.1.2.1 Mean Value Filter

The mean value filter is simply the average value of the parameter over the sequence length as shown in equation 2.1.

$$NO \text{ or } O = \frac{\sum_{i=1}^{i=24*days} Y_i}{24 * days} \quad (2.1)$$

### 2.1.2.2 Root Mean Squared (RMS) Filter

The mean average weights each observation equally while the RMS filter gives a higher weight parameters that are farther away from the setpoint as illustrated in equation 2.2.

$$NO \text{ or } O = \sqrt{\frac{\sum_{i=1}^{i=24*\text{days}} (Y_i - \text{setpoint})^2}{24 * \text{days}}} \quad (2.2)$$

### 2.1.2.3 Transfer Function Filter

The transfer function model is based on the analytical solution to the 1-D transient conduction problem for heat conduction in walls. This method is outlined in the ASHRAE handbook of Fundamentals [1993]. The method is computationally complex, depends on the type wall and may use data outside of the current window. The filter for this method is defined in equation 2.3.

$$NO \text{ or } O = \frac{\sum_{m=i-d}^{m=i} q_m}{\text{days}} \quad (2.3)$$

where:  $q_m$  = energy flow over time,  $i$

$m$  = summation index

Colliver et al. assumed the inside air temperature remained constant and used the outside dry-bulb temperature rather than the sol-air temperature normally used.

### 2.1.3 Data Window and Filter Selection

Colliver et al. applied these filters to both exclusive, overlapping and non-overlapping data windows. The study came to the following conclusions:

- exclusive, overlapping data windows produced the most extreme results

- data window rankings are highly dependent on the filter type
- window starting time did not make a significant difference.

The mean value filter was ultimately selected to evaluate each data window for ranking. This filter type is computationally simple and it is independent of the system being analyzed. The RMS and the transfer function filters are dependent on the setpoint and wall type respectively and are generally appropriate for temperature only. The RMS and transfer function filters are also more suited to temperature than for other weather parameters.

## 2.2 Extreme Sequence Calculations

### 2.2.1 Data Windows

This project examined window lengths of 24, 48, 72, 96, 120, 144 and 168 hours. Non-exclusive overlapping data windows were used for all four of the weather parameters. Exclusive overlapping data windows were not used, primarily because for the purposes of this project we are only interested in only the extreme sequence for each data window and not necessarily in ranking the data windows.

As extracted from the SAMSON database the file for each location and month contains 30 years of hourly data. In some instances, data are reported every three hours. In any case, the data window was reset when the end of the month was reached for each year. In other words, data windows for each month were evaluated separately for each year of data. Ignoring any missing data, the number of non-exclusive overlapping data windows available for 30 years of data for a 31-day month is:

$$n = 30 \times (d - wl + 1)$$

where:  $n$  = number of windows

$wl$  = window length in days

$d$  = number of days in the month

Table 2.1 summarizes the number of windows available using 30 years of data for each

Data Window Length [Days]	Number of Data Windows
1	930
2	900
3	870
4	840
5	810
6	780
7	750

**Table 2.1 – Data Windows**

window length for a 31 day month or 22,320 hours.

### 2.2.2 Filter Selection

The mean value filter (equation 2.1) was used for all weather parameters examined except for the solar radiation. The solar radiation is unique in that it is not continuous over the data window. The metric used to rank the solar radiation data windows is the integrated hourly solar radiation over the data window divided by the number of days in the data window. The filters used are summarized in Table 2.2.

Parameter	Filter Type
Dry-bulb Temperature	Mean Value
Humidity Ratio	Mean Value
Total Horizontal Solar Radiation	Mean Value over the number of days in the window
Windspeed	Mean Value

**Table 2.2 – Parameters and Filter Types**

### 2.2.3 Extreme Sequence Summary

Appendix B contains summary listings of extreme high and low sequences for 1 to 7 days for a number of weather parameters and associated coincident parameters. The data contained in the summary listings are shown in Table 2.3. The programs used to evaluate and extract the sequences are listed in Appendix E.

Extreme Parameter	Coincident Parameter
Dry-bulb Temperature [ $^{\circ}$ F]	Humidity Ratio [ $lb_w/lb_a$ ]
Humidity Ratio [ $lb_w/lb_a$ ]	Dry-bulb Temperature [ $^{\circ}$ F]
Total Horizontal Radiation [btu/ $ft^2$ ]	Dry-bulb Temperature [ $^{\circ}$ F]
Dry-bulb Temperature [ $^{\circ}$ F]	Total Horizontal Radiation [btu/ $ft^2$ ]
Wet-bulb Temperature [ $^{\circ}$ F]	Dry-bulb Temperature [ $^{\circ}$ F]
Windspeed [mph]	N/A

**Table 2.3 – Parameter Summary**

## Chapter 3

### Temperature Sequences

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The goal of this phase of the project is to develop a methodology that allows accurate generation of extreme dry bulb temperature sequences using readily available information e.g. monthly average dry bulb temperature, elevation, latitude etc. Accomplishing this objective requires developing techniques to characterize the distributions of hourly dry bulb temperatures, independent of the distribution shape. Information from a probability distribution of hourly dry bulb temperatures can then be abstracted to allow generation of hourly extreme time-series dry bulb temperature sequences.

Developing sequences of extreme dry bulb temperatures proceeded in two phases: distribution analysis and time-series analysis. The distribution analysis focused on investigating the nature of dry bulb temperature probability density functions for four separate months during the year (Table 3.1). These months were chosen to capture both the extremes of a given weather parameter (in this case dry bulb temperature) as well as the maximum variation of those parameters over a given design sequence.

Month	Type
January	Winter
March	Shoulder
July	Summer
October	Shoulder

**Table 3.1 – Month Types**

The probability density function can provide a significant amount of information on the behavior of dry bulb temperature for a given time and location, such as highest observation, highest percentile observation, etc. However, the probability density function does not

contain any information concerning the time-order of the observations. The time dimension or sequence order is essential for generating sequences of extremes.

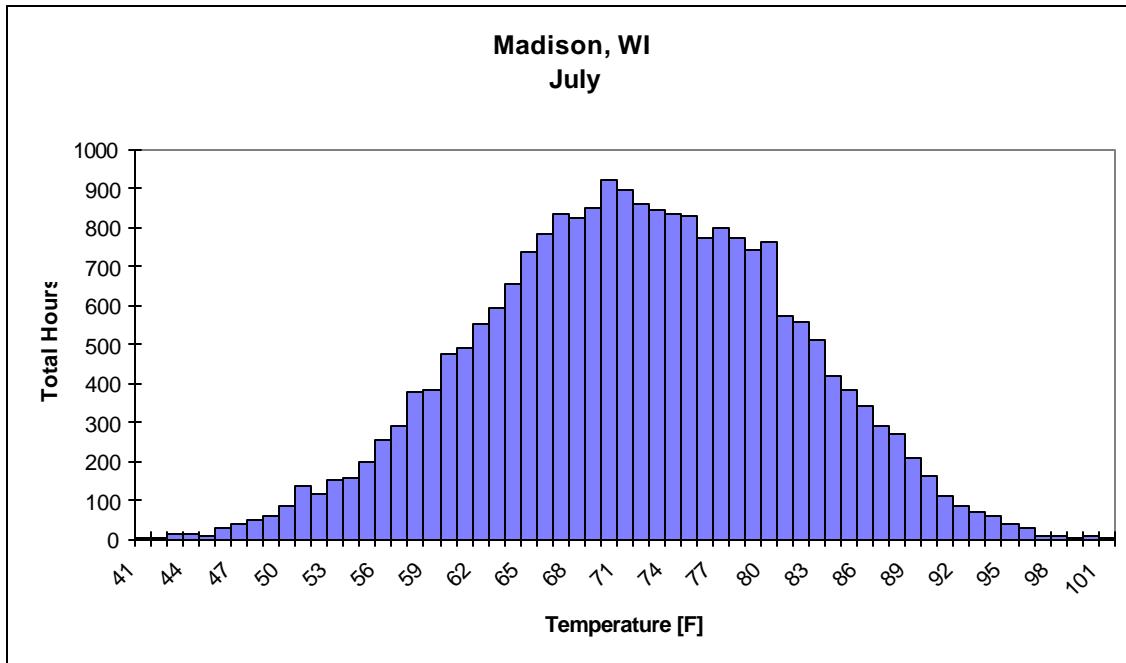
Finally, the time-series nature of dry bulb temperature is discussed and techniques are proposed to map dry bulb temperature probability density functions to sequences of temperature extremes ranging from 24 to 168 hours in length. A method is presented to obtain the average temperature for each day in a multi-day sequence. Three approaches to ordering days in multiple day sequences are presented.

### **3.1 Distribution Analysis**

If the hourly dry bulb temperatures for a specific month are normally distributed then the PDF (probability density function) can be completely defined by the mean and the standard deviation. If these two parameters were readily available, a designer could easily develop a probable distribution of hourly temperatures and infer any desired design condition (e.g. 99% design values for winter or 2.5% design values for summer). Unfortunately, the distribution of hourly dry bulb temperatures for a given month and location are seldom normally distributed. Many of the dry bulb temperature distributions investigated during the course of this research project were significantly skewed. In this case, alternative techniques had to be developed to account for the skewed nature of the distributions.

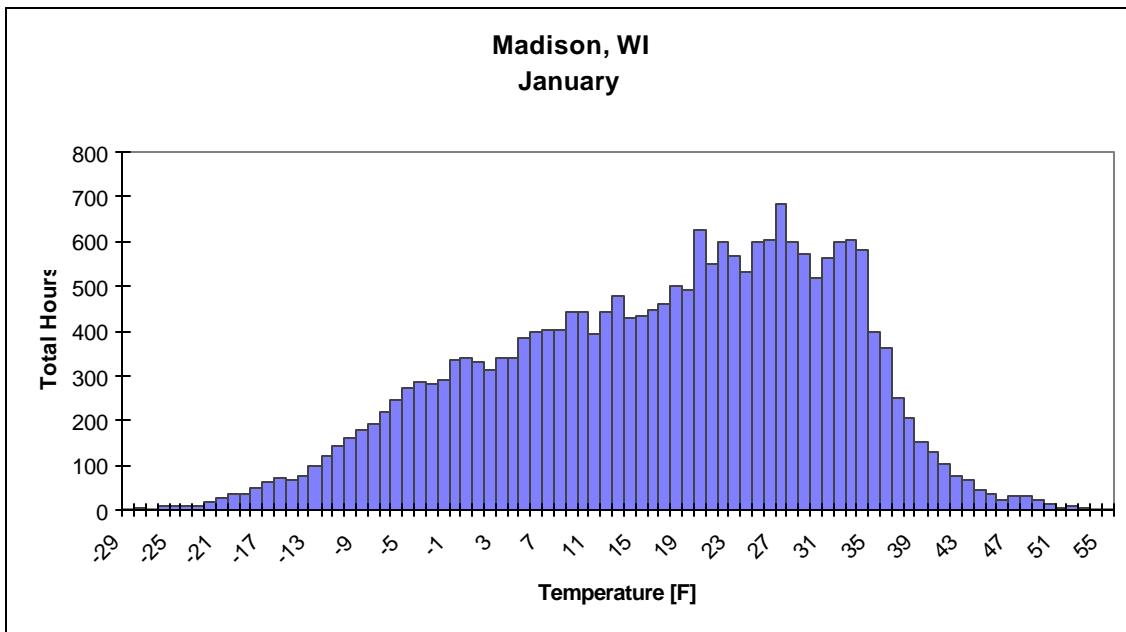
Three methods are explored to cope with the irregularity of the dry bulb temperature distributions: transformations, two-step distributions, and regressions. These techniques, in addition to the filtering methods previously described, form the basis to determine the information necessary to generate hourly values that makeup single day extreme dry bulb temperature sequences.

A common trend observed in the hourly temperature distributions developed with 30 years of hourly data is a skewing (e.g. the difference between the median and the mean) of the distribution due to the season and/or the location. This trend is illustrated by the following histograms showing the temperature distributions for the months of July and January in Madison, WI. The July temperature distribution for Madison, WI (Figure 3.1)



**Figure 3.1 – Madison July Hourly Temperature Frequency Distribution**

appears relatively normal. Both the median and the mean are about 72 °F. However, the January distribution (Figure 3.2) is noticeably skewed. The median is 19 °F the while the mean is 17 °F. The skewness is a concern since it affects the nature of the tails of the distributions, which represent the extreme temperatures. The skewness also precludes the use of a normal distribution to represent the temperature frequency distribution.



**Figure 3.2– Madison January Hourly Temperature Frequency Distribution**

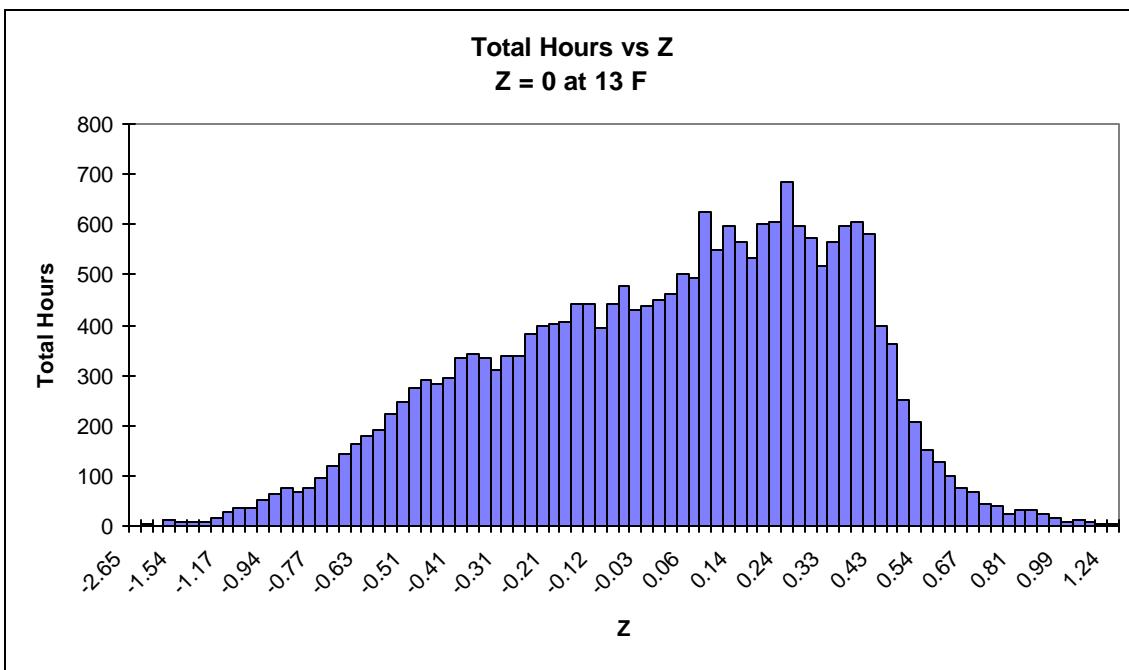
### 3.1.1 Transformation Approach

One possible technique to eliminate distribution skewness is to identify a suitable transformation to map or transform the data to a normal distribution. A transformation that has been used with some success for daily radiation data [Klein, 1976] is the hyperbolic tangent function applied to the dry-bulb temperature as follows. The dimensionless temperature, R, is defined such that:

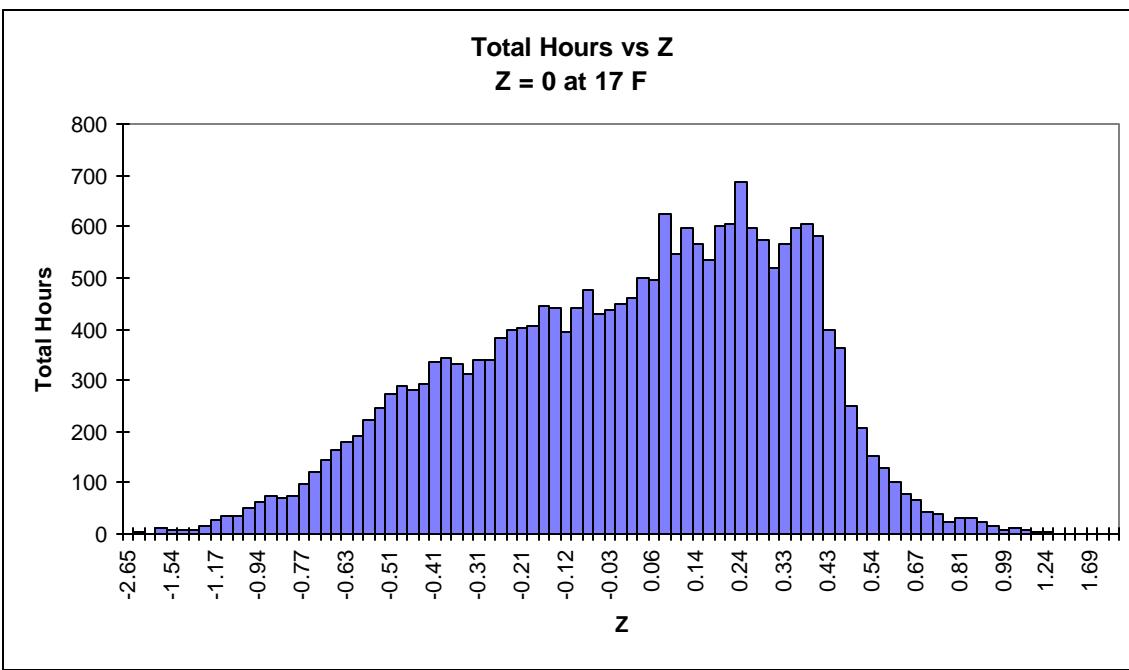
$$R = \frac{2(T - T_{\min})}{T_{\max} - T_{\min}} - 1 \quad (3.1)$$

where R ranges from -1 to +1. However, a normal distribution ranges from  $-\infty$  to  $+\infty$ . The hyperbolic tangent function can be applied to change R from a bounded to an unbounded function as follows:

$$R = \tanh(Z) \quad (3.2).$$



**Figure 3.3 – Madison January Transformed Hourly Temperature Frequency Distribution**



**Figure 3.4 – Madison January Transformed Hourly Temperature Frequency Distribution**

Here Z is the transformed dimensionless temperature. A plot of the distribution for January in Madison, WI is shown in Figure 3.3. The hyperbolic transformation provides some improvement but skewness in the transformed distribution is still evident. This is because, unlike normalized radiation data, the temperature distribution is unbounded. Even if  $T_{\max}$  is adjusted to force Z to zero at 17 °F, the mean temperature for Madison, WI in January, some skewness is still evident. Clearly, an alternative approach would be desirable.

### 3.2.1 Two Step Distribution Approach

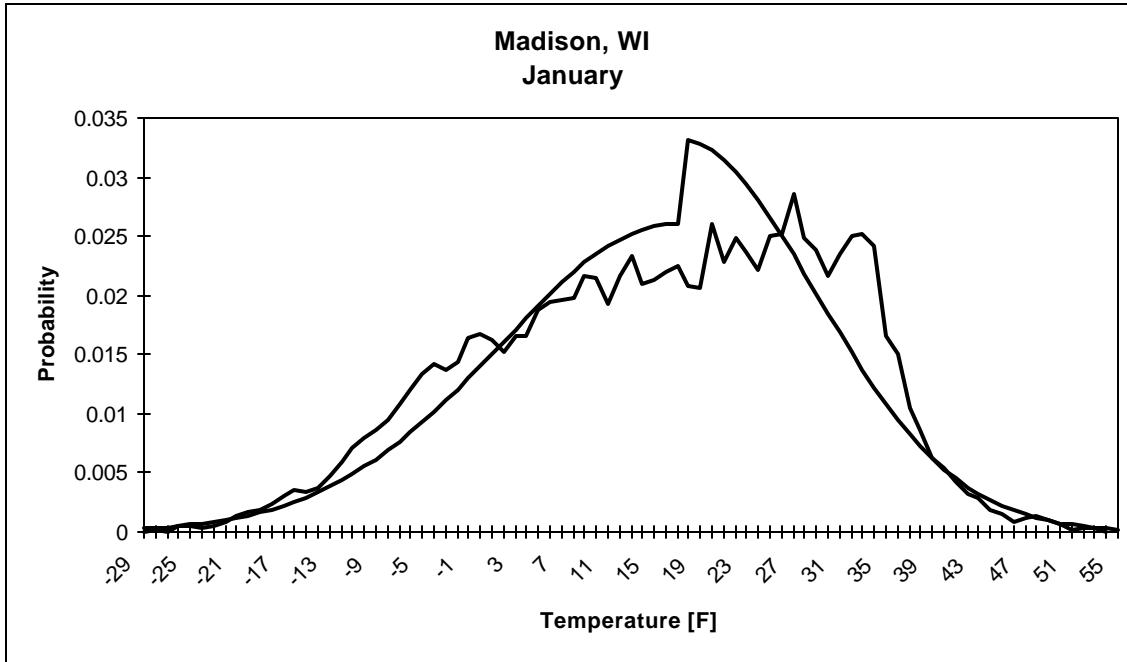
An alternative method to constructing a distribution which is reflective of the actual data (skewed or normal), involves building a distribution in two steps. The first step constructs the portion of the distribution above the mean while the second step constructs the distribution below the mean. The data required to perform the two step construction include high, low, and mean hourly temperature values. Using this information and the fact that three standard deviations is approximately 99% of the area under the normal curve we may estimate the standard deviation for either the left or right-side of the distribution in the following manner:

$$\hat{s}_{high} \approx \frac{|T_{avg} - T_{high,hourly,extreme}|}{3} \quad (3.3)$$

$$\hat{s}_{low} \approx \frac{|T_{avg} - T_{low,hourly,extreme}|}{3} \quad (3.4)$$

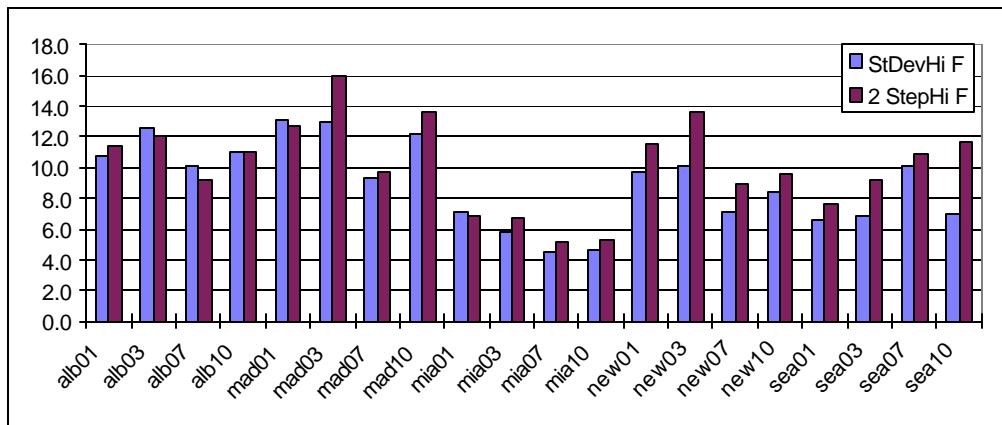
Here two different standard deviations are used, one for temperatures above the mean ( $\hat{s}_{high}$ ), and the other for temperatures below the mean ( $\hat{s}_{low}$ ) in order to accurately represent the skewness evident in the distribution data. In general, two parameters (the mean and the standard deviation) completely characterize a normal distribution. Applying the two step

procedure for a composite temperature distribution for the January Madison data can be constructed as illustrated in Figure 3.5. The composite distribution is a normal

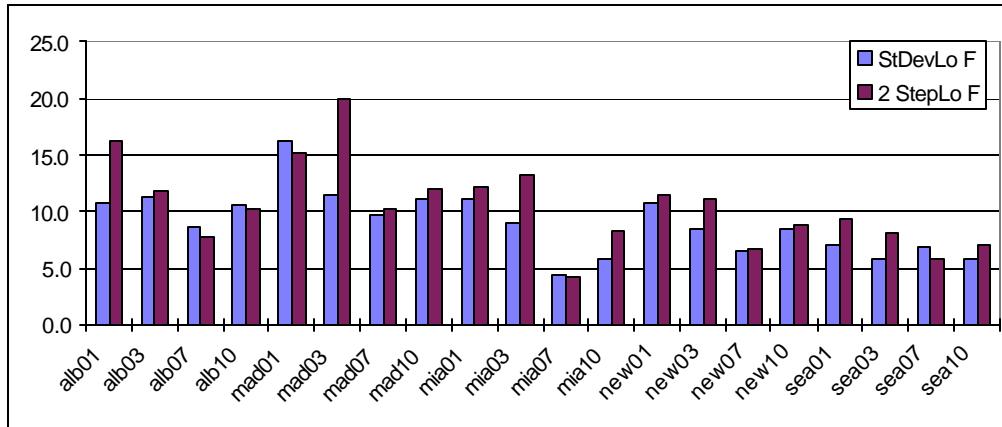


**Figure 3.5 – Madison January Two-Step Hourly Temperature Distribution**

distribution with differing standard deviations above and below the mean. The area enclosed by the normal distribution is 0.5 on each side of the mean. The total area under the curve is 1.0. The long-term mean in this instance is 17 °F. The normal curve closely matches the actual data in the most important regions of the actual distribution, at the upper and lower tails of the distribution. This approach allows the designer to construct the hourly temperature distribution needing only three pieces of information: the average and the observed extreme hourly high and low temperatures. To test the accuracy of this approach the standard deviation, calculated in the conventional manner, is compared to the standard deviation estimated using equations 3.3 and 3.4. The results are illustrated in Figures 3.6 and



**Figure 3.6 – Two-Step vs. Actual Standard Deviations above the Mean**



**Figure 3.7– Two-Step vs. Actual Standard Deviations below the Mean**

3.7. While all of the observations are incorporated into the conventional standard deviation compared to only two pieces of information in the two step approach it is evident that this method is strongly influenced by outliers. The unusual observation may be the result of error or it may be actual data. Attempts to formulate regression equations relating the actual standard deviation to the estimate proved inadequate. The resulting  $R^2$ 's (coefficient of determination) ranged from 61% to 76%. A more accurate method to estimate the hourly extremes is needed.

### 3.1.3 Regression Equation Approach

The lowest and highest hourly observed temperature over a 24-hour period is not usually available. If a probability distribution is used to determine the coldest or hottest temperature, the hour in which the observation occurred is not known. The distribution also does not contain any information concerning the order of the observations. A way to avoid these problems is to develop regression equations to estimate the 24-hour average temperature for an extreme day. The benefits to this approach include:

- time index or observation order is not required
- reduced influence of outliers on the regressions reduced due to a “tightening” of the data
- provides a simple technique to construct multi-day sequences.

Regression equations were developed starting with the initial results from a stepwise regression (see Appendix C) and then refined based on residual analysis to estimate the minimum and maximum average daily temperature using readily available information as predictors (in I-P units). The minimum and maximum daily average temperatures were found to be a function of the following variables: monthly average temperature, yearly range, skewness index, standard deviation of monthly average hourly values, location elevation, and the monthly average clearness index. Correlations for the minimum and maximum average daily dry bulb temperatures are given below.

$$\bar{T}_{\min, \text{day}} = -4.32 + 0.923\bar{T}_{\text{mon}} - 0.317\text{Range} + 19.8\text{Skew Index} \quad (3.5)$$

$$s = 3.0 \text{ } ^\circ\text{F}, R^2 = 99\%$$

$$\bar{T}_{\max, \text{day}} = 17.1 + 0.651\bar{T}_{\text{mon}} + 0.796s_{\text{yr}} - 0.00190z + 24.7\bar{K}_T \quad (3.6)$$

$$s = 2.6 \text{ } ^\circ\text{F}, R^2 = 96\%$$

where:	$\bar{T}_{\min, day}$	= daily average dry bulb temperature, extreme cold day, $^\circ\text{F}$
	$\bar{T}_{\max, day}$	= daily average dry bulb temperature, extreme hot day, $^\circ\text{F}$
	$\bar{T}_{mon}$	= monthly average dry bulb temperature, $^\circ\text{F}$
	$\bar{T}_{\max, mon}$	= highest monthly average dry bulb temperature, year, $^\circ\text{F}$
	$\bar{T}_{\min, mon}$	= lowest monthly average dry bulb temperature, year, $^\circ\text{F}$
	$\bar{T}_{yr}$	= average annual dry bulb temperature, $^\circ\text{F}$
Range		= $(\bar{T}_{\max, mon} - \bar{T}_{\min, mon})$ , $^\circ\text{F}$
Skew Index		= $\frac{(\bar{T}_{mon} - \bar{T}_{yr})}{Range}$
$\sigma_{yr}$		= standard deviation of $\bar{T}_{mon}$ , $^\circ\text{F}$
$z$		= elevation, ft
$\bar{K}_T$		= average monthly clearness index
$s$		= standard deviation of the residuals, $^\circ\text{F}$
$R^2$		= coefficient of determination

Results from the regressions were developed using the four principle months of thirty- year hourly data from the seven development locations. The test locations were maintained as independent sets and used to test the regressions. The results of the regressions applied to the development and test locations are shown in Tables 3.2 and 3.3. The standard deviation and the average of the error terms are also listed. These regressions were used in the weather database supplied with the extreme sequence program to provide estimates of each location's

maximum and minimum temperatures. The residuals from the test and development locations were carefully analyzed for any patterns that may have led to improved regressions (see Appendix D). When using the regression equations care must be taken when predictors are used that are outside of the range of those used to formulate the original equations. The

Development Locations				Test Locations			
Location	T <sub>min,act</sub>	T <sub>min,est</sub>	act-est	Location	T <sub>min,act</sub>	T <sub>min,est</sub>	act-est
	°F	°F	°F		°F	°F	°F
alb01	-2.0	2.5	-4.5	cha01	22.0	19.9	2.1
alb03	23.0	20.3	2.7	cha03	26.0	35.7	-9.7
alb07	64.0	62.9	1.1	cha07	70.0	71.2	-1.2
alb10	36.0	34.2	1.8	cha10	43.0	48.7	-5.7
atl01	9.0	10.7	-1.7	chi01	-13.0	-11.9	-1.1
atl03	25.0	29.0	-4.0	chi03	12.0	8.6	3.4
atl07	66.0	65.1	0.9	chi07	57.0	56.7	0.3
atl10	42.0	41.6	0.4	chi10	30.0	29.3	0.7
bal01	5.0	0.9	4.1	kan01	-4.0	-5.8	1.8
bal03	16.0	17.5	-1.5	kan03	6.0	15.7	-9.7
bal07	63.0	62.6	0.4	kan07	62.0	62.8	-0.8
bal10	37.0	34.9	2.1	kan10	35.0	34.3	0.7
hou01	23.0	21.1	1.9	los01	45.0	34.8	10.2
hou03	33.0	37.2	-4.2	los03	49.0	37.9	11.1
hou07	73.0	69.1	3.9	los07	61.0	62.3	-1.3
hou10	48.0	49.5	-1.5	los10	53.0	57.2	-4.2
mad01	-14.0	-16.1	2.1	new01	6.0	0.1	5.9
mad03	-2.0	5.3	-7.3	new03	18.0	13.4	4.6
mad07	55.0	55.6	-0.6	new07	62.0	61.0	1.0
mad10	28.0	26.2	1.8	new10	38.0	35.5	2.5
mia01	43.0	41.9	1.1	san01	37.0	24.6	12.4
mia03	51.0	52.1	-1.1	san03	42.0	34.0	8.0
mia07	76.0	76.5	-0.5	san07	54.0	51.3	2.7
mia10	64.0	66.4	-2.4	san10	50.0	48.5	1.5
sea01	19.0	16.0	3.0	wes01	39.0	39.4	-0.4
sea03	29.0	24.6	4.4	wes03	49.0	49.4	-0.4
sea07	53.0	56.4	-3.4	wes07	75.0	74.2	0.8
sea10	37.0	36.1	0.9	wes10	61.0	64.9	-3.9
Average			0.0	Average			1.1
SD			2.9	SD			5.3

Table 3.2 – Minimum Temperatures

regression may not be valid in these regions. The extreme sequence generation program allows the user to replace the regression result if better data are available.

Development Locations				Test Locations			
Location	T <sub>max,act</sub>	T <sub>max,est</sub>	act-est	Location	T <sub>max,act</sub>	T <sub>max,est</sub>	act-est
	°F	°F	°F		°F	°F	°F
alb01	54.0	57.0	-3.0	cha01	70.0	67.3	2.7
alb03	70.0	66.7	3.3	cha03	75.0	75.8	-0.8
alb07	88.0	87.0	1.0	cha07	89.0	90.8	-1.8
alb10	72.0	73.7	-1.7	cha10	82.0	81.8	0.2
atl01	66.0	62.7	3.3	chi01	52.0	54.4	-2.4
atl03	73.0	72.3	0.7	chi03	69.0	66.0	3.0
atl07	92.0	88.7	3.3	chi07	89.0	91.5	-2.5
atl10	79.0	78.8	0.2	chi10	79.0	77.3	1.7
bal01	61.0	60.0	1.0	kan01	60.0	58.9	1.1
bal03	74.0	69.4	4.6	kan03	73.0	70.0	3.0
bal07	88.0	91.6	-3.6	kan07	94.0	95.8	-1.8
bal10	78.0	79.0	-1.0	kan10	80.0	80.5	-0.5
hou01	74.0	69.1	4.9	los01	70.0	71.1	-1.1
hou03	77.0	77.4	-0.4	los03	77.0	73.3	3.7
hou07	90.0	91.9	-1.9	los07	79.0	80.9	-1.9
hou10	84.0	84.1	-0.1	los10	88.0	78.0	10.0
mad01	48.0	52.1	-4.1	new01	61.0	59.5	1.5
mad03	66.0	64.3	1.7	new03	68.0	66.8	1.2
mad07	89.0	90.4	-1.4	new07	94.0	90.5	3.5
mad10	74.0	74.7	-0.7	new10	76.0	78.1	-2.1
mia01	78.0	78.0	0.0	san01	62.0	64.6	-2.6
mia03	81.0	81.9	-0.9	san03	65.0	69.9	-4.9
mia07	87.0	87.5	-0.5	san07	78.0	77.4	0.6
mia10	85.0	84.7	0.3	san10	78.0	74.3	3.7
sea01	56.0	56.4	-0.4	wes01	77.0	76.7	0.3
sea03	58.0	63.0	-5.0	wes03	80.0	81.0	-1.0
sea07	82.0	80.9	1.1	wes07	87.0	87.5	-0.5
sea10	67.0	67.5	-0.5	wes10	84.0	84.2	-0.2
Average			0.0	Average			0.4
SD			2.4	SD			2.9

**Table 3.3 – Maximum Temperatures**

## 3.2 One Day Sequence

### 3.2.1 Diurnal Variation of Extreme Day

The ambient temperature follows a daily cyclical pattern that is relatively deterministic. In other words, the noise or random component is small enough that it is reasonable to use a completely deterministic model. Erbs developed such a relationship for the normalized hourly diurnal temperature variation (equation 3.7).

$$T_{hour} = \bar{T}_{day} + A(0.4632 \cos(t^* - 3.805) + 0.0984 \cos(2t^* - 0.360) + 0.0168 \cos(3t^* - 0.822) + 0.0138 \cos(4t^* - 3.513)) \quad (3.7)$$

where:  $T_{hour}$  = hourly dry bulb temperature at  $t^*$ , °F

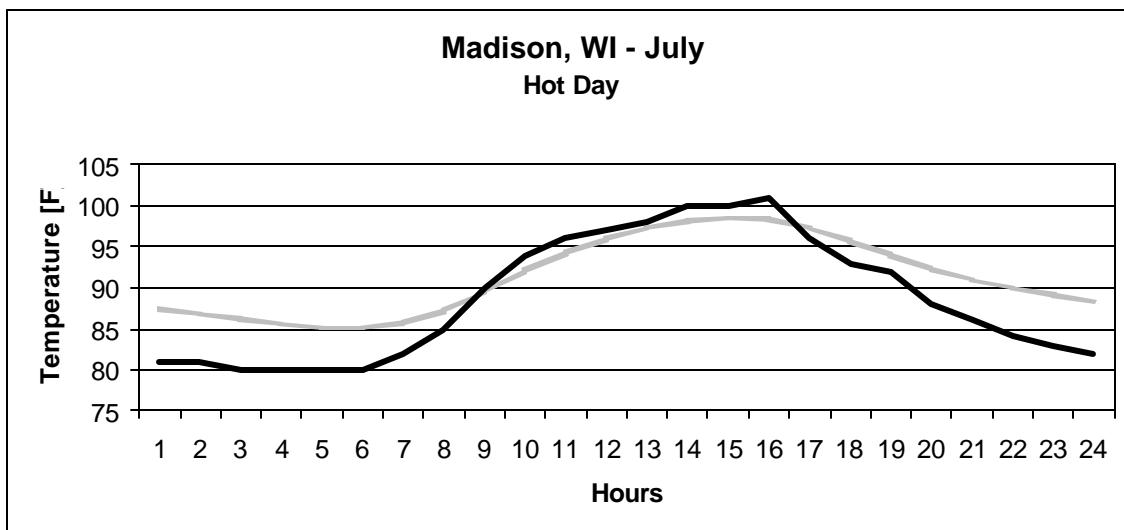
$\bar{T}_{day}$  = average daily dry-bulb temperature, °F

$$t^* = \frac{2p(t-1)}{24}$$

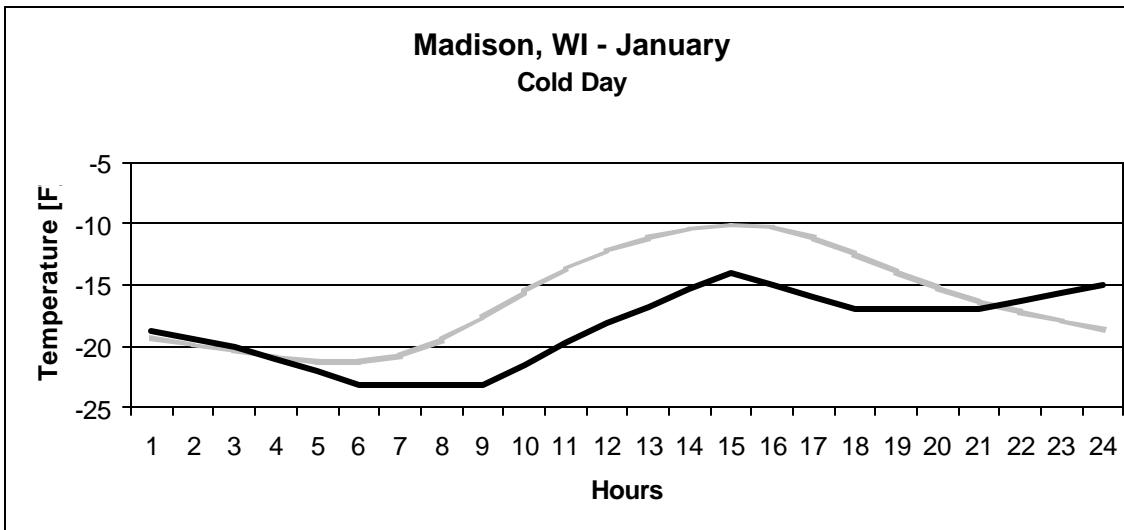
t = hour (1 = 1AM, 24 = midnight)

A = amplitude or  $(T_{high} - T_{low})_{day}$ , °F

Erbs normalized the hourly temperatures using monthly averages. To determine if equation 3.7 could also be used for extreme days, several extreme days were examined to verify that an extreme day followed the same general pattern. Figures 3.8a and 3.8b illustrate the daily diurnal temperature generated using Erbs' relationship compared to a hot and cold 24-hour extreme sequence, WI in January. The shapes of the curves are similar with the high and low temperature occurring at about the same time of the day. Once the daily average temperature for an extreme day is found, using the regressions formulated earlier,<sup>7</sup> the hourly temperature variation may be found using 3.7.



**Figure 3.8a – Actual (dark) vs. Generated (light) Hot Day**



**Figure 3.8b – Actual (dark) vs. Generated (light) Cold Day**

### 3.2.2 Daily Range for an Extreme Day

To completely define the hourly dry bulb temperature the amplitude or daily range is required. Erbs [1983, 1984] found that the diurnal variation of the daily dry bulb temperature was a function of the radiation balances between the daytime and nighttime hours. The solar radiation received during the day is a function of cloud cover and may be expressed by the

clearness index, to the ratio of the total solar radiation striking a horizontal surface in a month to the extraterrestrial radiation on a horizontal surface. The radiation losses at night are also a function of cloud cover. This results in relatively large diurnal variations on clear days and small variations on cloudy days. A correlation that relates the amplitude of the daily diurnal variation or range to the monthly clearness index as follows:

$$A = 1.0 + 35.6 \bar{K}_T - 0.000902 \mathbf{v}_{mon}^3 \quad (3.8)$$

$$s = 2.6^{\circ}\text{F}, R^2 = 66.4\%$$

where:  $A$  = daily amplitude or  $(T_{high} - T_{low})_{day}$ ,  $^{\circ}\text{F}$

$\bar{K}_T$  = monthly average clearness index

$\mathbf{v}_{mon}$  = average monthly humidity ratio\*1000,  $\text{lb}_w/\text{lb}_a$

$s$  = standard deviation of the residuals,  $^{\circ}\text{F}$

$R^2$  = coefficient of determination

This relationship was developed for average days. All locations and months used in this study were examined to determine if the extreme day had a markedly different range than an average day. The results are tabulated in Appendix B. In general, the hot extreme days have a higher diurnal variation than the cold extreme days. However, in many instances the extreme range does differ significantly from the average range. Since no consistent trend is evident for typical design points (e.g. a cold day in January), the average range is used for both hot and cold extreme days. In addition, the amplitudes of individual days within extreme cold and hot multi-day sequences were also examined to see if any identifiable trends were present. The results are similar to the single day amplitudes; no significant differences were

discernable. Table 3.4 lists the results from the regression developed using the four principle months of thirty-year hourly data from the seven development locations.

Development Locations				Test Locations			
Location	A <sub>act</sub>	A <sub>est</sub>	act-est	Location	A <sub>act</sub>	A <sub>est</sub>	act-est
	°F	°F	°F		°F	°F	°F
alb01	22.3	23.4	-1.1	cha01	19.8	16.2	3.6
alb03	26.4	25.2	1.2	cha03	20.8	18.5	2.4
alb07	25.3	24.9	0.5	cha07	16.1	14.6	1.5
alb10	25.4	25.8	-0.4	cha10	20.1	18.6	1.5
atl01	17.8	16.3	1.6	chi01	15.1	15.6	-0.5
atl03	20.7	18.3	2.4	chi03	16.3	17.7	-1.4
atl07	17.2	16.0	1.2	chi07	19.8	18.5	1.2
atl10	19.5	19.4	0.2	chi10	20.0	19.0	1.0
bal01	15.6	15.9	-0.4	kan01	17.2	17.7	-0.5
bal03	18.6	17.7	0.9	kan03	19.4	18.4	1.0
bal07	18.8	17.0	1.8	kan07	18.9	19.3	-0.4
bal10	20.1	18.1	1.9	kan10	20.5	19.9	0.6
hou01	18.9	15.4	3.5	los01	16.0	20.8	-4.8
hou03	20.2	17.1	3.1	los03	13.1	22.4	-9.3
hou07	18.3	14.6	3.7	los07	11.1	22.6	-11.5
hou10	21.2	18.5	2.6	los10	13.7	20.9	-7.2
mad01	16.1	16.7	-0.5	new01	10.9	14.9	-4.0
mad03	17.9	18.8	-0.9	new03	13.1	16.3	-3.2
mad07	22.2	18.6	3.6	new07	13.9	16.0	-2.1
mad10	20.9	18.6	2.2	new10	12.8	17.1	-4.3
mia01	15.1	18.1	-3.0	san01	11.8	17.9	-6.2
mia03	13.9	19.1	-5.3	san03	12.9	21.4	-8.5
mia07	11.5	14.0	-2.4	san07	15.9	24.4	-8.4
mia10	11.7	15.6	-4.0	san10	16.0	21.3	-5.2
sea01	8.6	10.9	-2.3	wes01	16.7	17.5	-0.8
sea03	12.8	15.5	-2.7	wes03	15.6	19.0	-3.4
sea07	18.8	22.9	-4.1	wes07	13.4	14.0	-0.6
sea10	12.8	15.3	-2.5	wes10	12.4	15.2	-2.9
Average			0.0	Average			-2.6
SD			2.6	SD			3.9

**Table 3.4 – Daily Range**

The test locations were maintained as independent sets and used to test the regressions. The standard deviation and the average of the error terms are also listed. The techniques used to

derive this correlation are the same as those used for the dry-bulb temperatures see, Appendix D for further information. Appendix D also contains a better regression equation for the daily amplitude if more predictor variables, such as those used for the temperature regressions, are available.

### 3.2.3 Standard Deviation of the Daily Range

To better characterize the variability of the diurnal variation within a multi-day sequence a correlation was developed which relates the standard deviation of the average daily amplitude to the local elevation, monthly clearness index, longitude and average humidity ratio. The correlation is listed below (3.9). Table 3.5 lists the results from the

$$SD_{Day} = -30.8 - 0.000655z + 8.26\bar{K}_T + 0.756long - 0.00395long^2 - 0.0196V_{mon}^2 \quad (3.9)$$

$$s = 0.586 \text{ } ^\circ\text{F}, R^2 = 89.9\%$$

where:  $z$  = local elevation, ft

$\bar{K}_T$  = monthly clearness index

$long$  = longitude, degrees

$V_{mon}$  = average monthly humidity ratio\*1000, lb<sub>w</sub>/lb<sub>a</sub>

$s$  = standard deviation of the residuals,  $^\circ\text{F}$

$R^2$  = coefficient of determination

regression developed using the four principle months of thirty-year hourly data from the seven development locations. The test locations were maintained as independent sets and used to test the regressions. The standard deviation and the average of the error terms are also listed. The techniques used to derive this correlation are the same as those used for the dry-bulb temperatures. Appendix D contains further information concerning equation 3.9.

Development Locations				Test Locations			
Location	SD <sub>act</sub>	SD <sub>est</sub>	act-est	Location	SD <sub>act</sub>	SD <sub>est</sub>	act-est
	°F	°F	°F		°F	°F	°F
alb01	6.6	6.5	0.1	cha01	8.0	7.4	0.6
alb03	7.8	6.9	0.9	cha03	7.0	7.5	-0.6
alb07	4.7	5.5	-0.8	cha07	3.7	3.0	0.7
alb10	7.0	6.7	0.3	cha10	6.7	6.7	-0.1
atl01	7.8	7.4	0.3	chi01	7.0	8.0	-1.0
atl03	7.6	7.6	0.0	chi03	8.0	8.4	-0.3
atl07	4.2	3.9	0.4	chi07	6.2	6.2	0.0
atl10	6.7	7.2	-0.6	chi10	7.9	8.2	-0.3
bal01	7.0	7.2	-0.2	kan01	7.4	8.6	-1.2
bal03	8.5	7.5	1.0	kan03	8.9	8.6	0.3
bal07	5.4	4.5	0.9	kan07	5.0	5.7	-0.7
bal10	7.5	6.9	0.6	kan10	7.7	8.4	-0.7
hou01	8.8	7.9	0.9	los01	7.2	7.2	0.0
hou03	7.9	7.7	0.2	los03	5.4	7.4	-2.0
hou07	4.1	3.7	0.4	los07	2.8	6.1	-3.3
hou10	7.4	7.1	0.2	los10	6.7	6.4	0.4
mad01	7.4	8.2	-0.8	new01	5.2	6.5	-1.4
mad03	8.5	8.6	-0.1	new03	5.9	6.7	-0.8
mad07	6.1	6.2	-0.1	new07	4.1	4.3	-0.2
mad10	8.3	8.1	0.1	new10	4.6	6.3	-1.7
mia01	5.8	6.4	-0.6	san01	4.9	5.9	-1.0
mia03	5.4	6.3	-0.9	san03	5.3	6.6	-1.3
mia07	2.8	2.6	0.2	san07	5.9	6.8	-0.9
mia10	3.6	4.0	-0.4	san10	6.9	6.2	0.7
sea01	3.8	4.3	-0.5	wes01	6.2	6.5	-0.3
sea03	5.4	5.3	0.1	wes03	5.8	6.4	-0.6
sea07	6.3	6.2	0.1	wes07	3.1	2.5	0.6
sea10	5.4	4.8	0.6	wes10	4.4	4.1	0.3
Average			0.1	Average			-0.5
SD			0.5	SD			0.9

Table 3.5 – Standard Deviation of the Daily Range

### 3.3 Average Temperature Over Multiple Day Sequence

The determination of the average temperature for individual days in a multi-day sequence is based on the observation that the average temperature over a hot sequence decreases as the sequence length increases and conversely the average temperature over a

cold sequence increases as the sequence length increases. This is illustrated in Figures 3.9 and 3.10 for hot and cold sequences respectively. Here the average absolute temperature over the sequence length has been normalized using the absolute 24-hour extreme average temperatures. Absolute temperatures are used to avoid the problems that would arise if negative temperatures were encountered. Equations 3.10 and 3.11 are straight-line regressions developed from the data in Figures 3.9 and 3.10.

$$TR_{hot} = 1.0017 - 0.00208n \quad - \text{ extreme hot sequence} \quad (3.10)$$

$$TR_{cold} = 0.999 + 0.00296n \quad - \text{ extreme cold sequence} \quad (3.11)$$

where:  $TR_{hot} = \frac{\bar{T}_{hot,seq}}{\bar{T}_{max,day}}, {}^{\circ}\text{R}$

$$TR_{cold} = \frac{\bar{T}_{cold,seq}}{\bar{T}_{min,day}}, {}^{\circ}\text{R}$$

n = day number in the sequence

These equations used in conjunction with the average over an extreme day determined using the regression from the previous section allow the generation of an average temperature for each day in the sequence. This allows the generation of a sequence to be constructed that will approximate the average sequence temperature observed in the actual data.

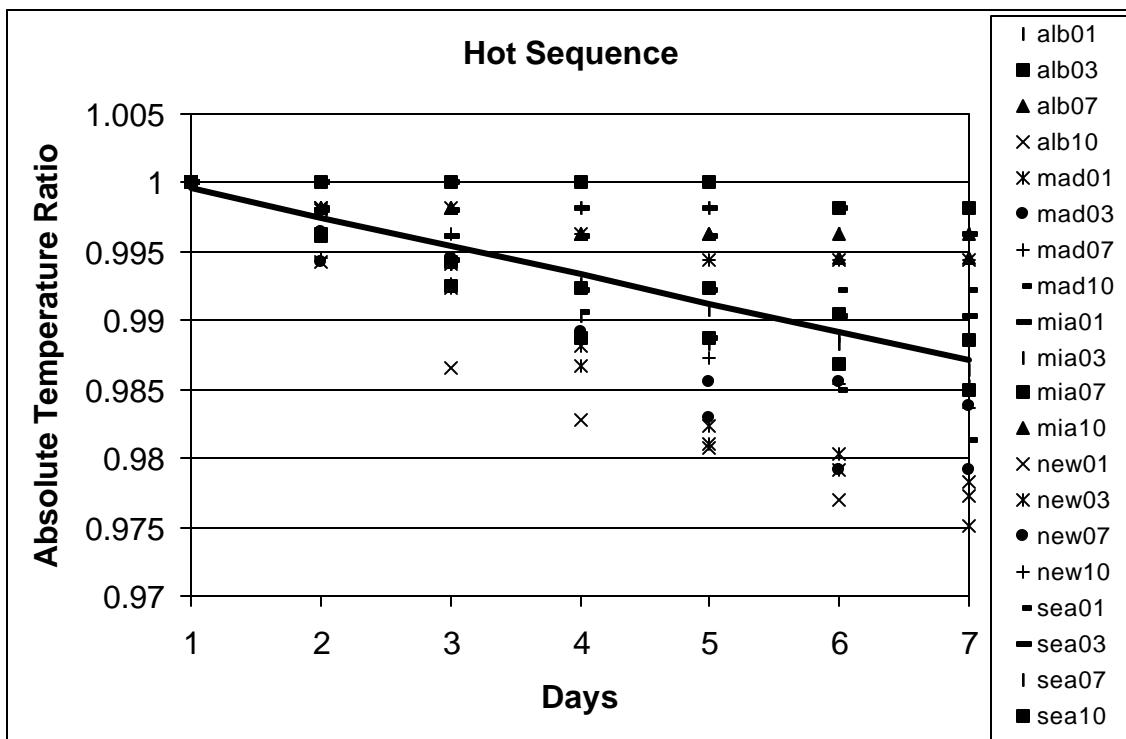


Figure 3.9 - Normalized Hot Sequence (Equation 3.10)

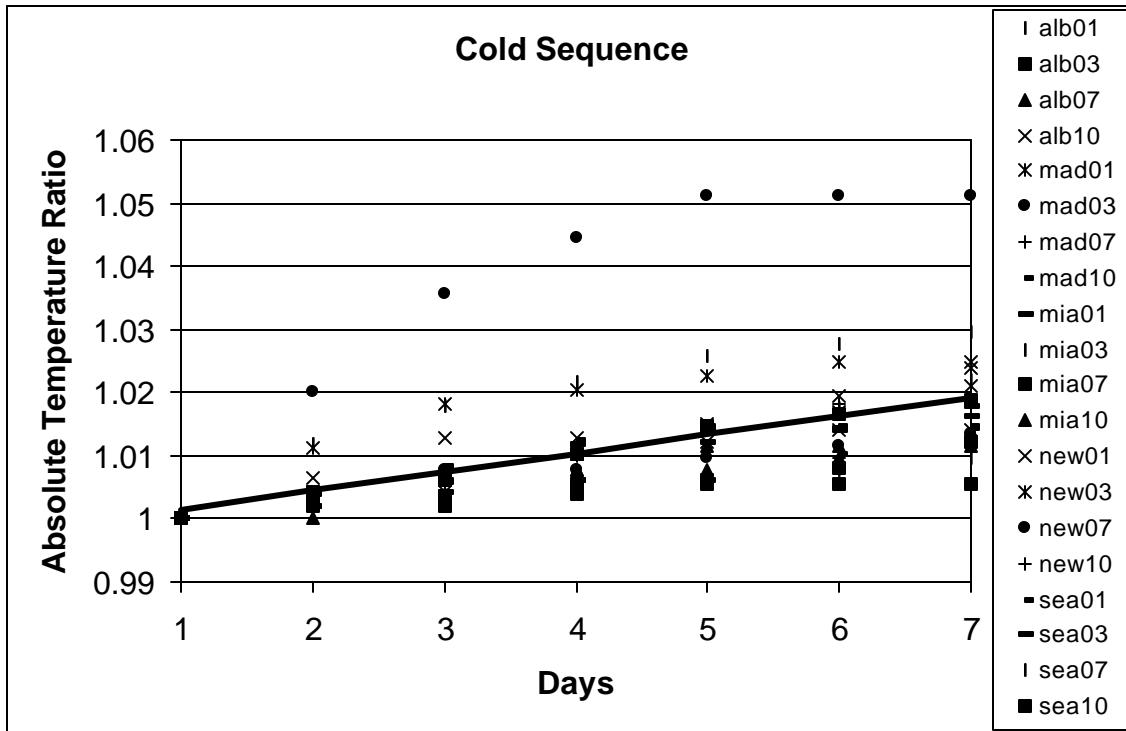


Figure 3.10 - Normalized Cold Sequence (Equation 3.11)

### 3.3.1 Sequence Ordering

The default sequence order generated using the previous algorithm may be unrealistic given the situation. Three options are available to tailor the sequence for particular situations. These include:

- autocorrelated order
- in order of increasing temperature (ramp up)
- in order of decreasing temperature (ramp down)

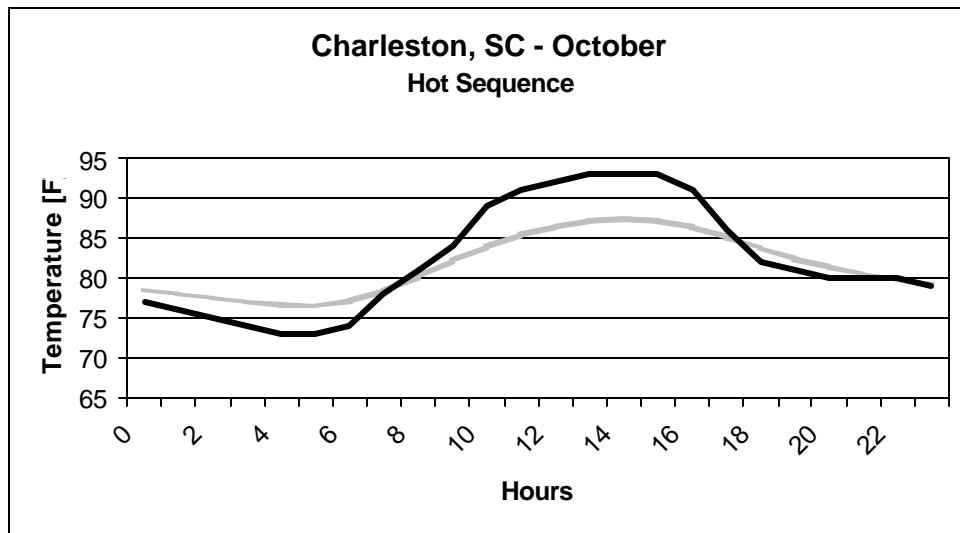
The autocorrelated option is based on the technique used by Knight [1991] that attempts to preserve the auto-correlation for a given set of daily temperatures for a month. In this case, it was adapted for sequences from 2 to seven days. The last two options are ordered based on the average temperature over the day.

### 3.4 Comparison of Generated with Actual Extreme Sequences

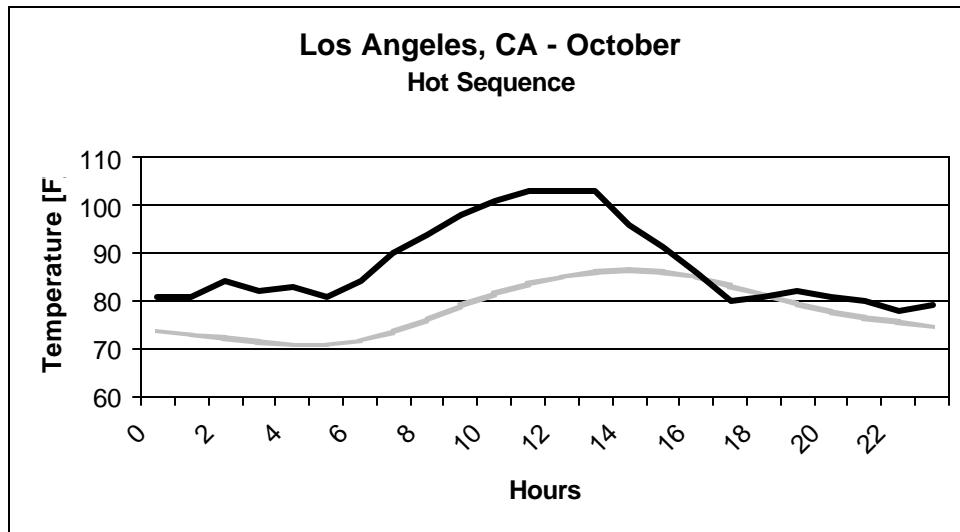
To gauge the accuracy of the generator actual extremes sequences from the test location sites are compared to generated sequences. The test site locations used represent the smallest and largest errors (actual – estimation) of the four months for a 1 and 7 day hot and cold sequence. These locations and sequence are summarized in Table 3.6. The actual versus generated data are plotted in Figures 3.11 through 3.14.

Location	Sequence Type	Error (act-est) °F
cha10	hot	0.2
chi07	cold	0.3
los10	hot	10.0
san01	cold	12.4

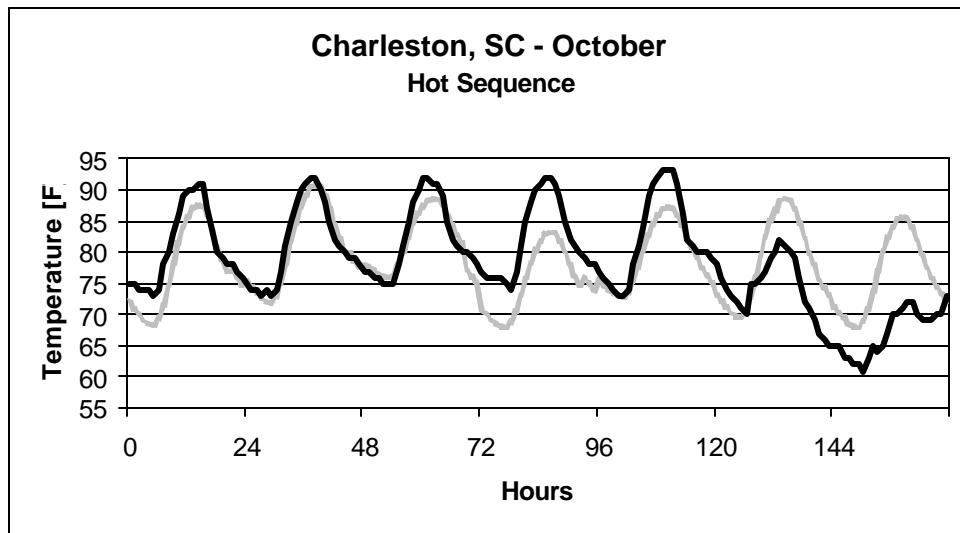
**Table 3.6 – Maximum and Minimum Error for Generated Sequences**



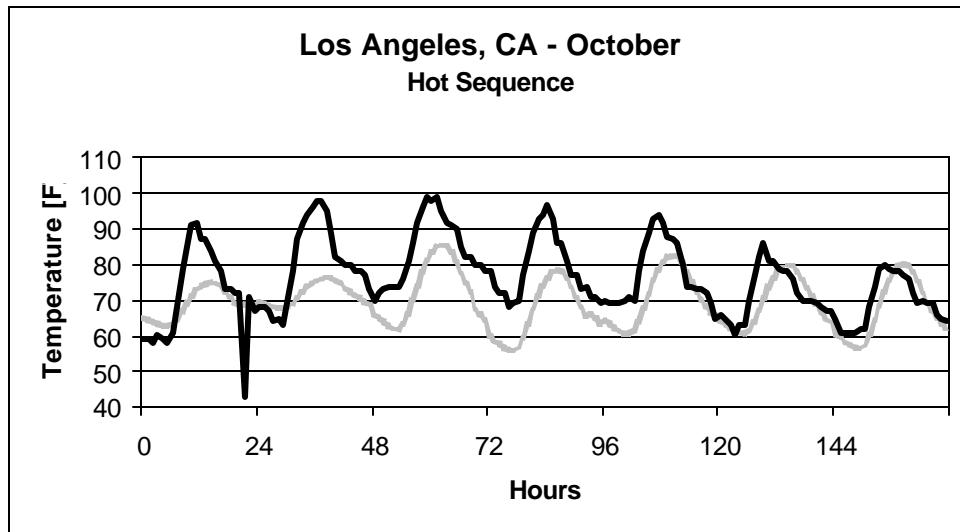
**Figure 3.11a – Actual (dark) vs. Generated (light) Temperature Small Error – One Day Hot Sequence**



**Figure 3.11b – Actual (dark) vs. Generated (light) Temperature Large Error – One Day Hot Sequence**



**Figure 3.12a – Actual (dark) vs. Generated (light) Temperature Small Error –  
7-Day Hot Sequence**



**Figure 3.12b – Actual (dark) vs. Generated (light) Temperature Large Error –  
7-Day Hot Sequence**

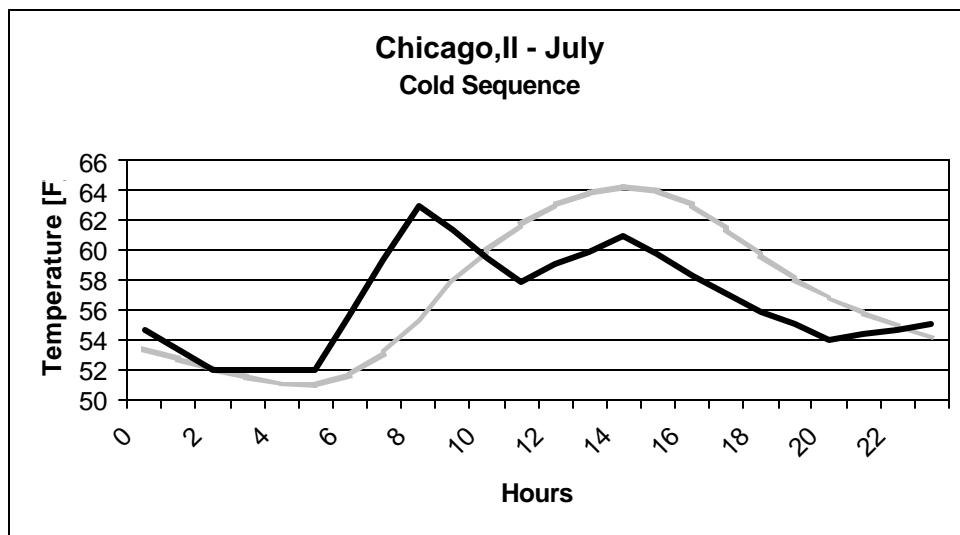


Figure 3.13a – Actual (dark) vs. Generated (light) Temperature Small Error – One Day Cold Sequence

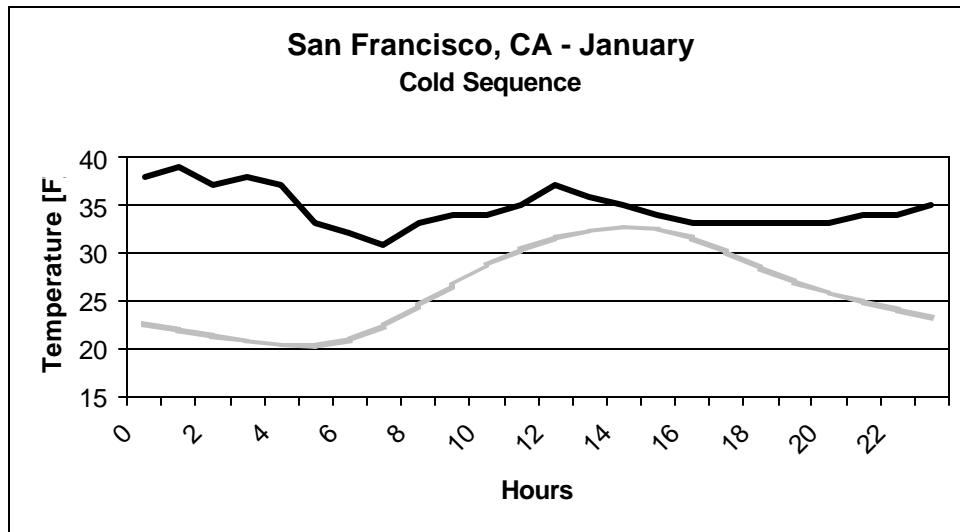
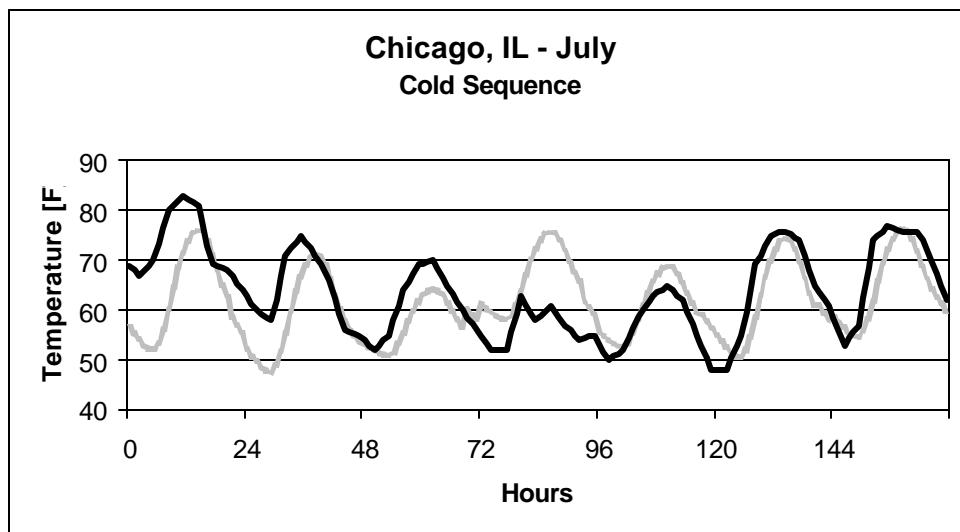
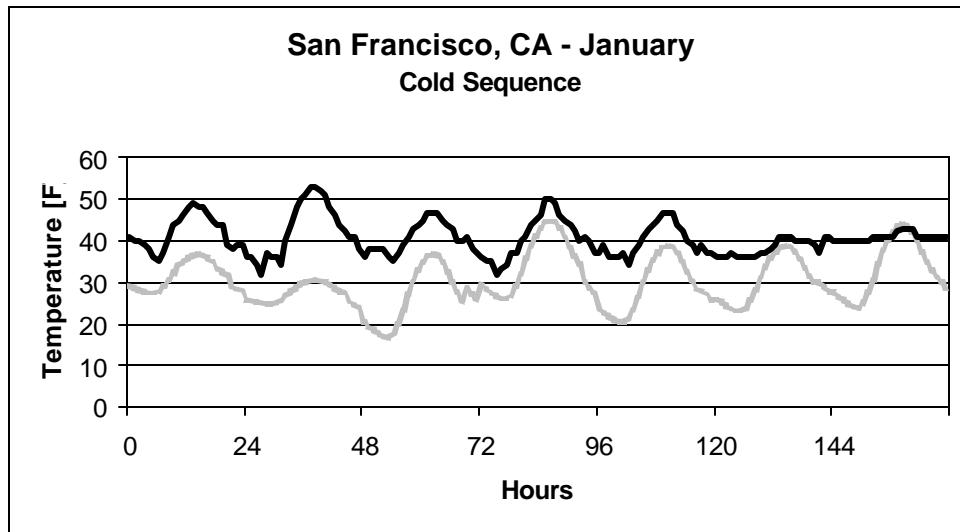


Figure 3.13b – Actual (dark) vs. Generated (light) Temperature Large Error – One Day Cold Sequence



**Figure 3.14a – Actual (dark) vs. Generated (light) Temperature Small Error – 7-Day Cold Sequence**



**Figure 3.14b – Actual (dark) vs. Generated (light) Temperature Large Error – 7-Day Cold Sequence**

## Chapter 4

### Humidity Sequences

---

The goal of this phase of the project is to develop a methodology to characterize maximum humidity sequences. This task includes both maximum “stand-alone” humidity sequences and humidity sequences coincident with maximum dry-bulb temperatures. Minimum humidity sequences, either “stand-alone” or coincident, were deemed to be of little importance and are not displayed by the extreme weather generator (i.e. latent loads due to ventilation would not be important in cooling load calculations during the winter months). Several measures may be used characterize the amount of water vapor contained in the air; however, parameters such as relative humidity, wet bulb or dew point temperatures are highly dependent on the dry bulb temperature. To simplify the characterization of the humidity sequence, a parameter that is less dependent on the dry-bulb temperature is preferred. The humidity ratio was examined and found to be a relatively unaffected by the dry-bulb temperature (compared with the other parameters) for most locations for the month of July. The average humidity ratio was also relatively constant over a one to seven day sequence for the locations and the month examined.

To characterize the humidity ratio sequences a time series analysis was performed and a lag one autoregressive (AR(1)) model was determined to adequately represent both the extreme high “stand-alone” and coincident humidity ratio sequences. Once the humidity ratio sequence is determined it can be used with the dry-bulb temperature sequence to calculate wet bulb and dew point temperatures and the relative humidity.

## 4.1 Psychrometric Calculations

The SAMSON database does not explicitly include the humidity ratio. The humidity ratio was calculated for each hour using the reported dry bulb and dew point temperatures along with station pressure. The program used is listed in Appendix E.

## 4.2 Humidity Ratio Sequence Characterization

### 4.2.1 Time Series Analysis and Model Identification

To analyze the maximum humidity sequences the extreme humidity ratios were retrieved for the month of July for the 14 locations listed in Table 4.1. Unlike the temperature

Location
Albuquerque, NM
Atlanta, GA
Baltimore, MD
Charleston, SC
Chicago, IL
Houston, TX
Kansas, MO
Los Angeles, Ca
Madison, WI
Miami, FL
New York, NY
San Francisco, CA
Seattle, WA
West Palm Beach, FL

**Table 4.1 – Humidity Sequence Locations**

regressions developed in Chapter 3, a different metric is involved when evaluating time series models. The main challenge is to properly identify the model. Therefore, all the locations will be used to determine if a location dependent, time series model may be developed. The following two types of humidity sequences were then examined:

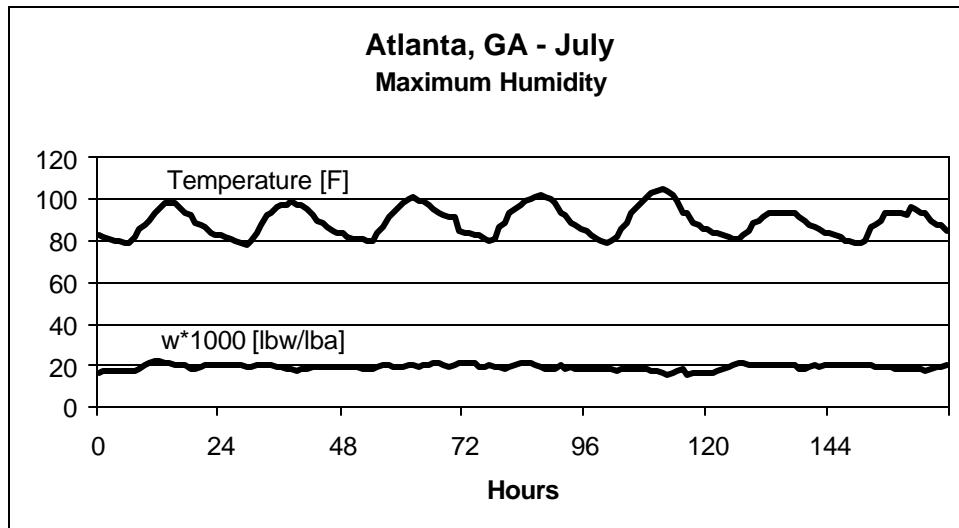
- Highest average dry bulb temperature and coincident humidity ratio for July

- Highest stand-alone humidity ratio and coincident dry bulb temperature for July.

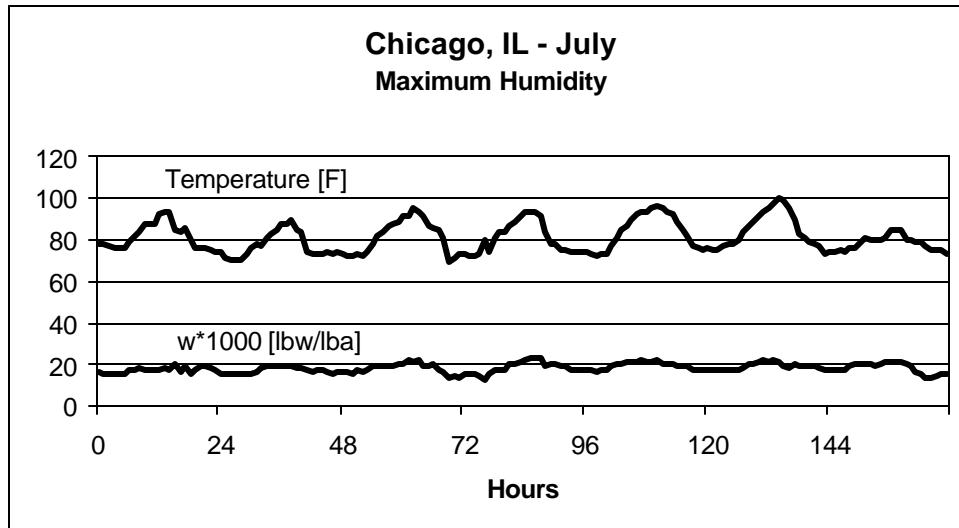
Extreme seven day sequences of humidity ratio ( $lb_w/lb_a$ ) and coincident dry bulb temperatures ( $^{\circ}F$ ) are shown for three of the locations are illustrated in Figures 4.1 through 4.3. Extreme seven day sequences of maximum dry bulb temperature ( $^{\circ}F$ ) and are representative of the 14 inspected. The locations examined exhibited no linear trend over the seven-day sequence length. In addition, most locations examined exhibited no seasonal or periodic trend. In two locations, notably Chicago (maximum) and Houston (coincident), a periodic component was noted. Also since both the maximum and coincident series display coincident humidity ( $lb_w/lb_a$ ) are illustrated in Figures 4.4 through 4.6. These three locations similar behavior, no attempt to was made to model each sequence type differently. The humidity sequences were assumed stationary based on the 28 data sets examined. Therefore, no transformations or differencing of the series was required. See Appendix C for an overview of time series analysis.

To aid in model identification the autocorrelation (ACF) and the partial autocorrelation (PACF) functions were examined. These are shown in Figures 4.6 through 4.18 for both the maximum and coincident humidity sequences for lags up to 42 hours. The dashed lines represent 95% confidence limits. From a purely statistical point of view (i.e. ignoring the physics of the underlying process) the ACF and PACF values below this line do not differ significantly from zero. The ACF exhibited either a slow decay or a sinusoid pattern. The PACF, “cut-off” after one to two lags. Tables 4.2 and 4.3 summarize the ACF and PACF behavior for all the locations examined. This combination of ACF and PACF behavior indicates a borderline stationary autoregressive process of order one (AR(1)).

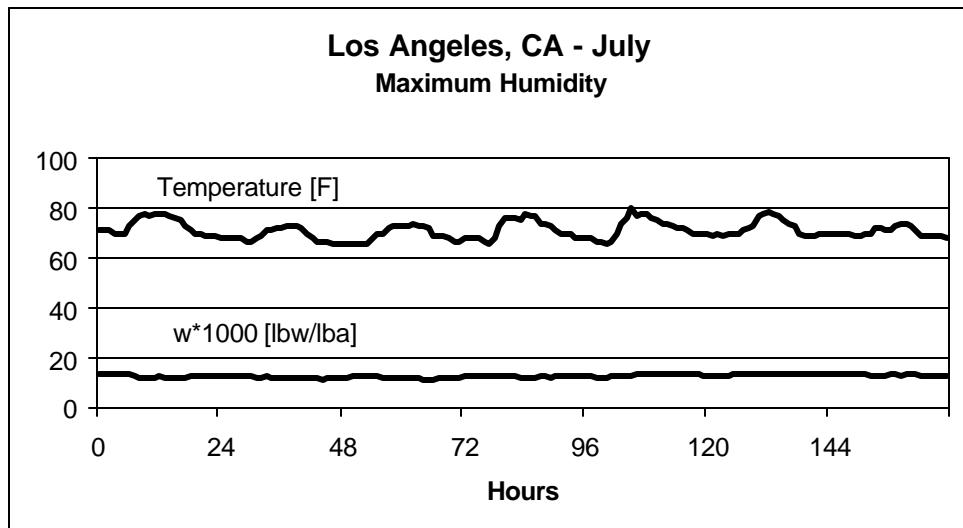
Various time series models must be fit and evaluated to test this hypothesis. The next section examines the appropriateness of an AR(1).



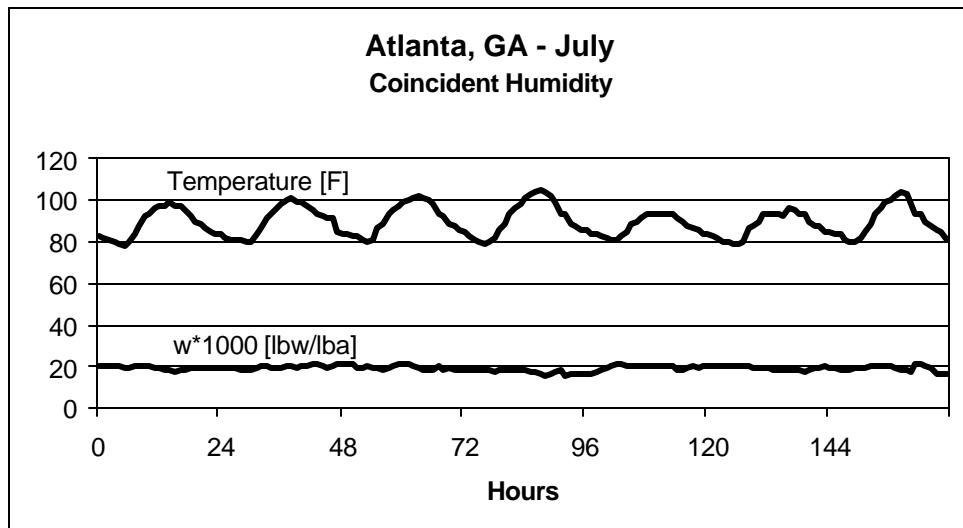
**Figure 4.1 – Atlanta, GA - Maximum Humidity Sequence**



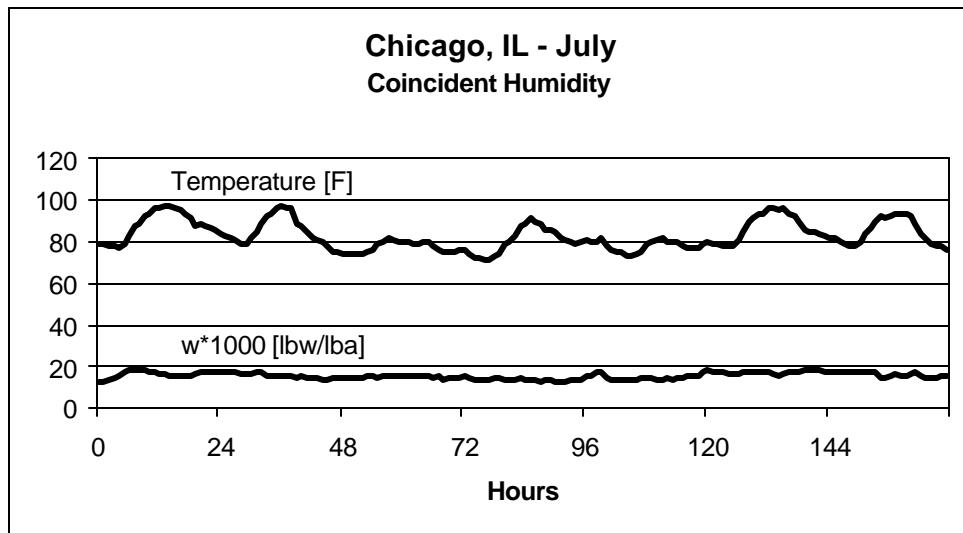
**Figure 4.2 – Chicago, IL - Maximum Humidity Sequence**



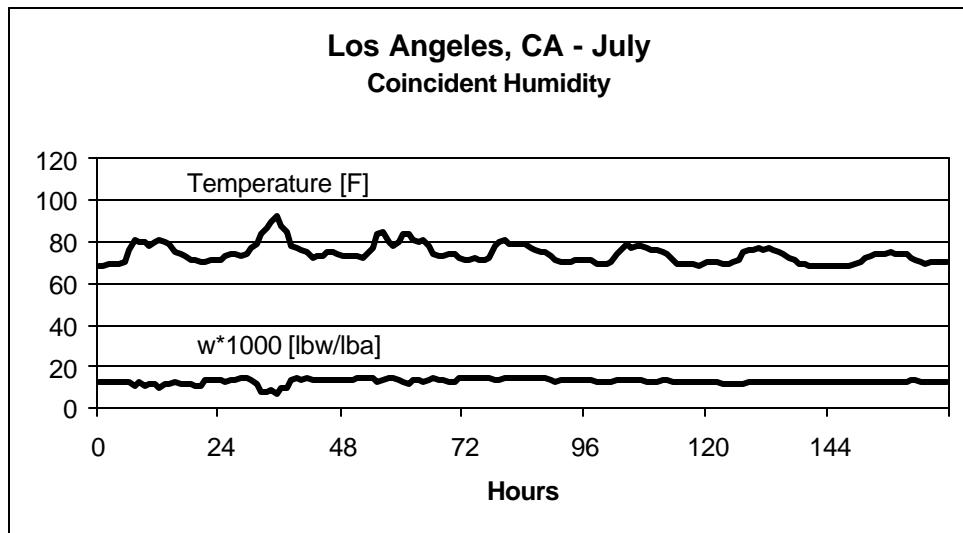
**Figure 4.3 – Los Angeles, CA - Maximum Humidity Sequence**



**Figure 4.4 – Atlanta, GA - Maximum Temperature Sequence**

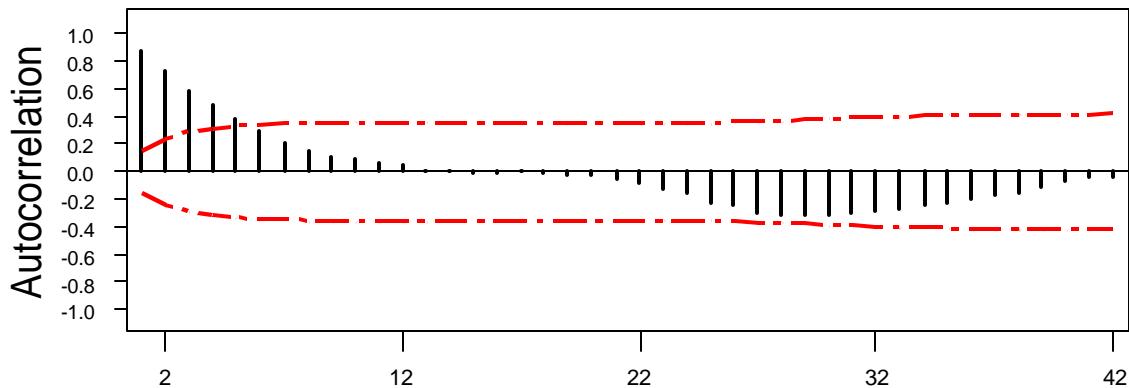


**Figure 4.5 – Chicago, IL - Maximum Temperature Sequence**



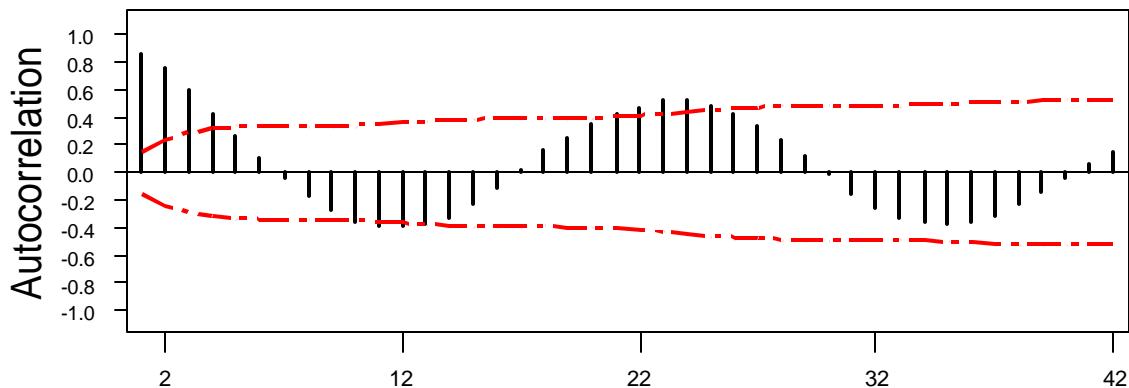
**Figure 4.6 – Los Angeles, CA - Maximum Temperature Sequence**

### Atlanta, GA - Maximum Humidity



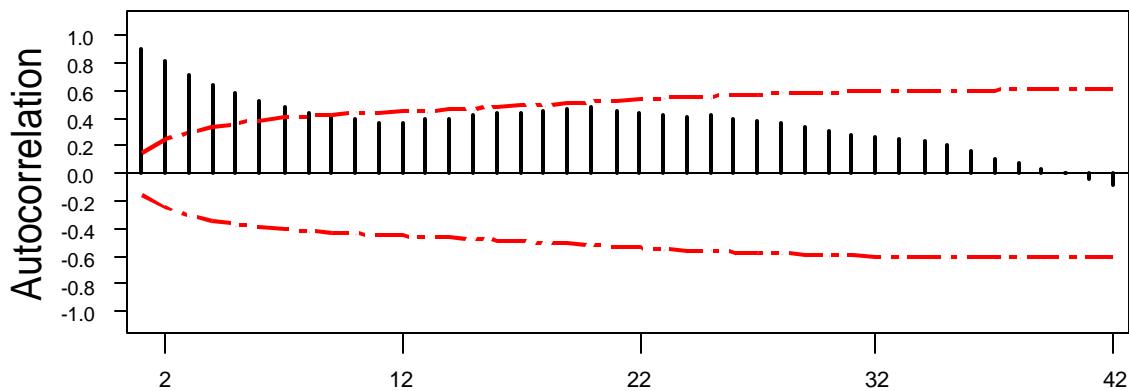
**Figure 4.7 – Atlanta, GA – ACF for Maximum Humidity**

### Chicago, IL - Maximum Humidity

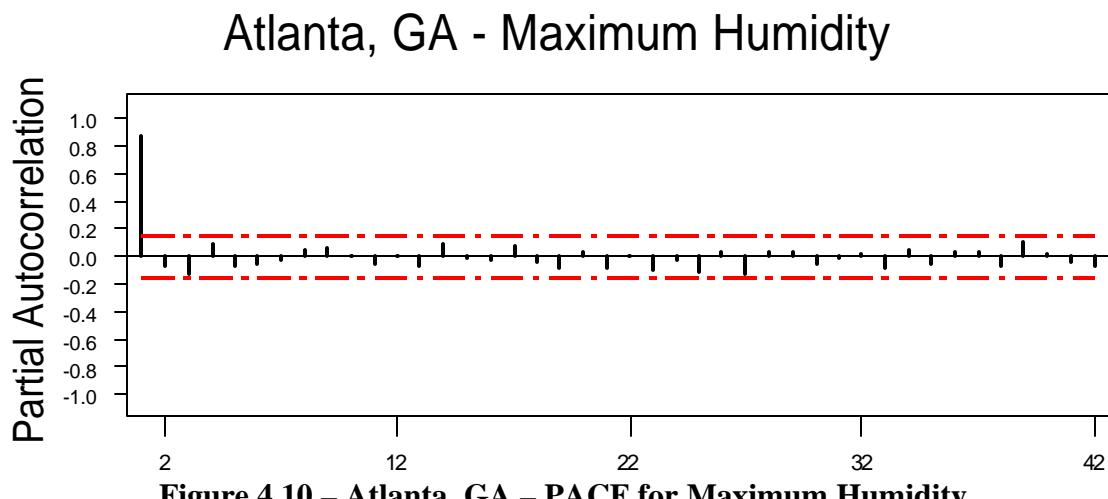


**Figure 4.8 – Chicago, IL – ACF for Maximum Humidity**

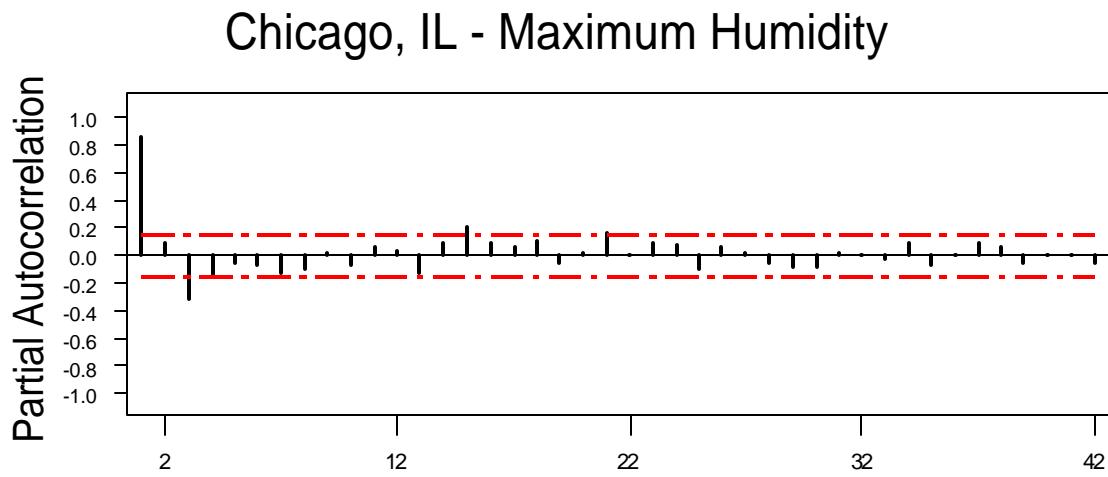
### Los Angeles, CA - Maximum Humidity



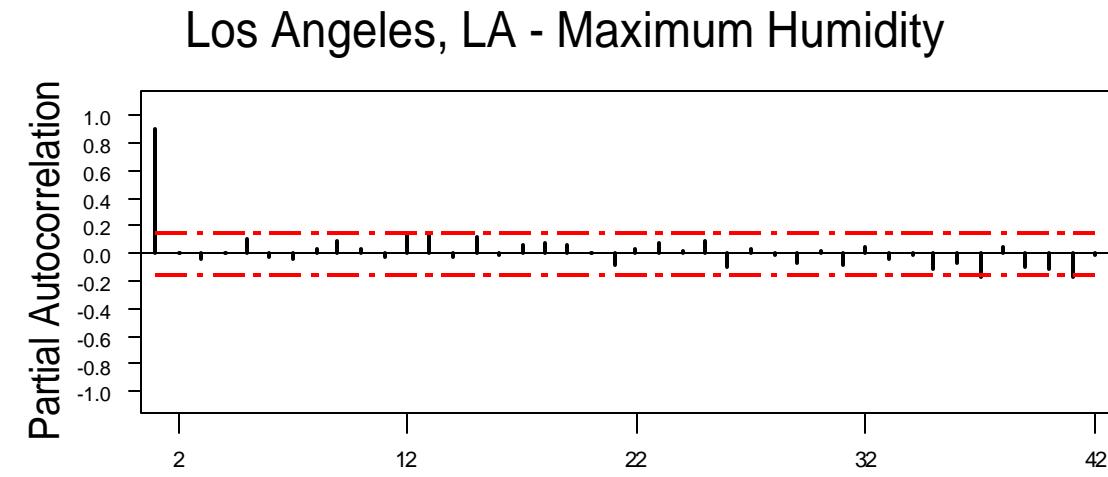
**Figure 4.9 - Los Angeles, CA – ACF for Maximum Humidity**



**Figure 4.10 – Atlanta, GA – PACF for Maximum Humidity**

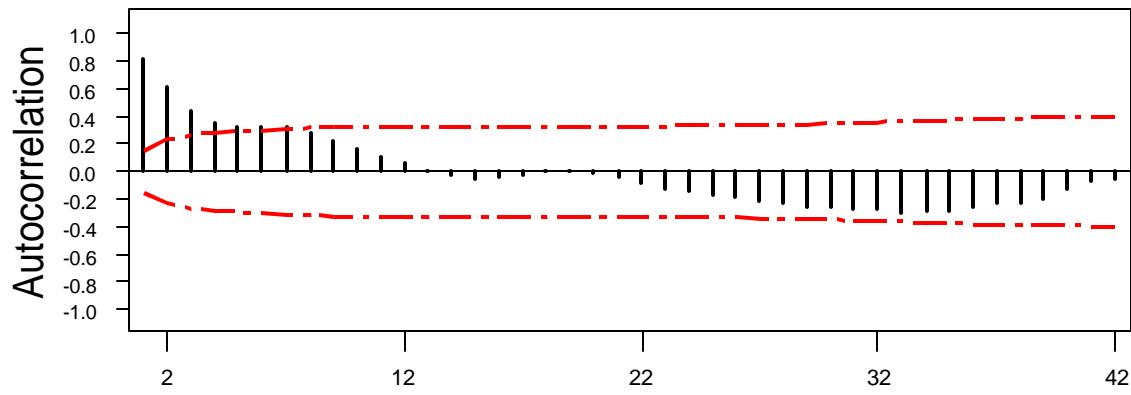


**Figure 4.11 – Chicago, IL – PACF for Maximum Humidity**



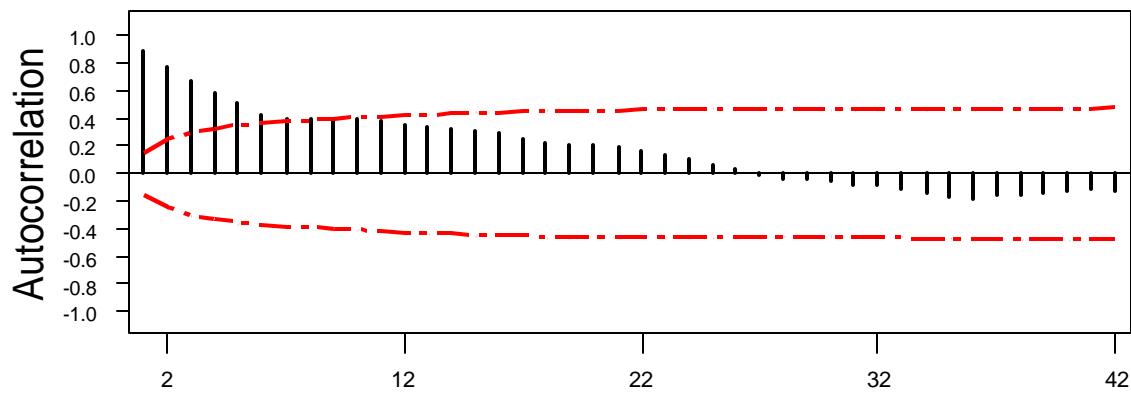
**Figure 4.12 – Los Angeles, CA – PACF for Maximum Humidity**

### Atlanta, GA - Coincident Humidity



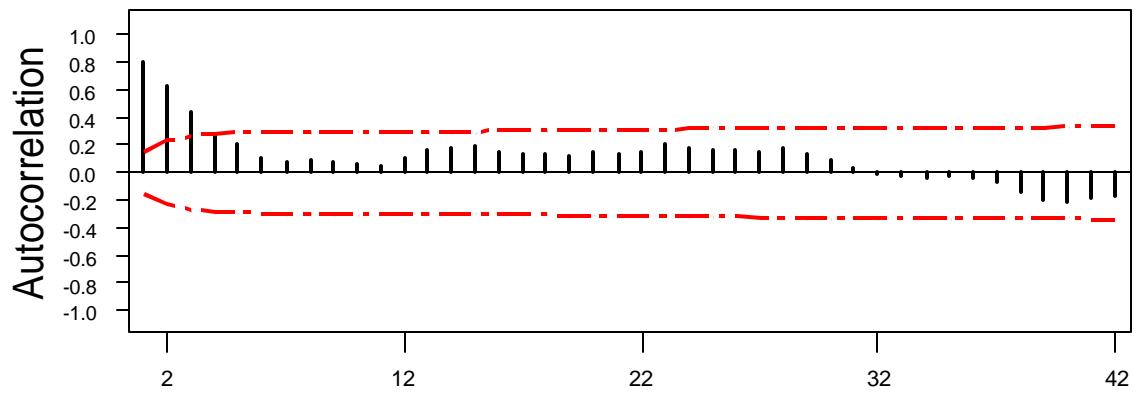
**Figure 4.13 – Atlanta, GA – ACF for Coincident Humidity**

### Chicago, IL - Coincident Humidity



**Figure 4.14 – Chicago, IL – ACF for Coincident Humidity**

### Los Angeles, CA - Coincident Humidity



**Figure 4.15 – Los Angeles, CA – ACF for Coincident Humidity**

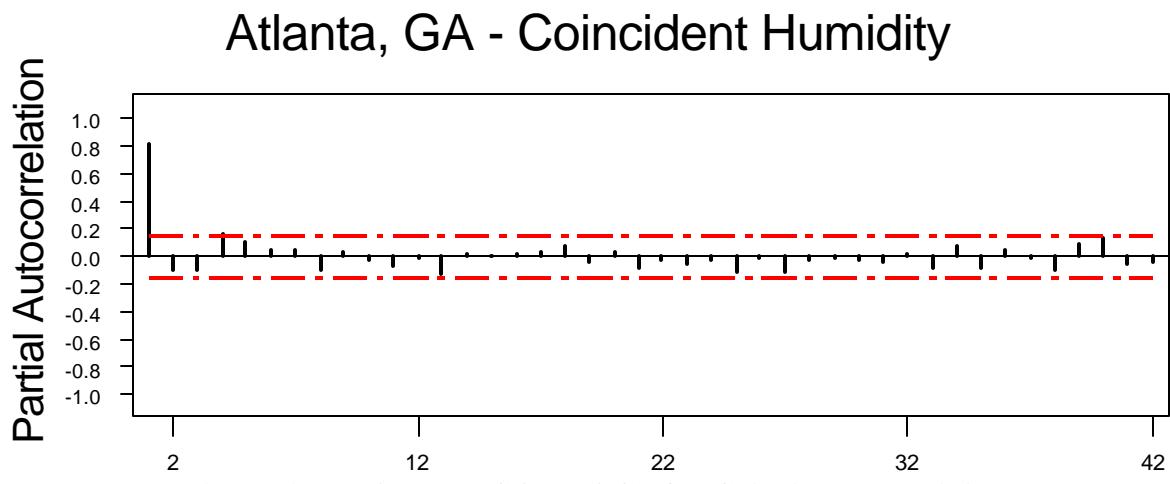


Figure 4.16 – Atlanta, GA – PACF for Coincident Humidity

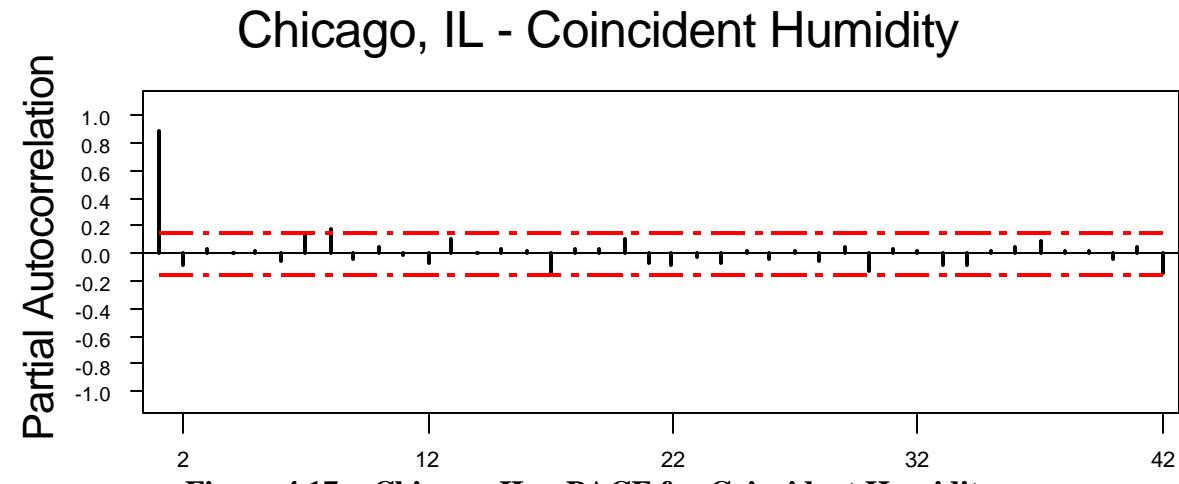


Figure 4.17 – Chicago, IL – PACF for Coincident Humidity

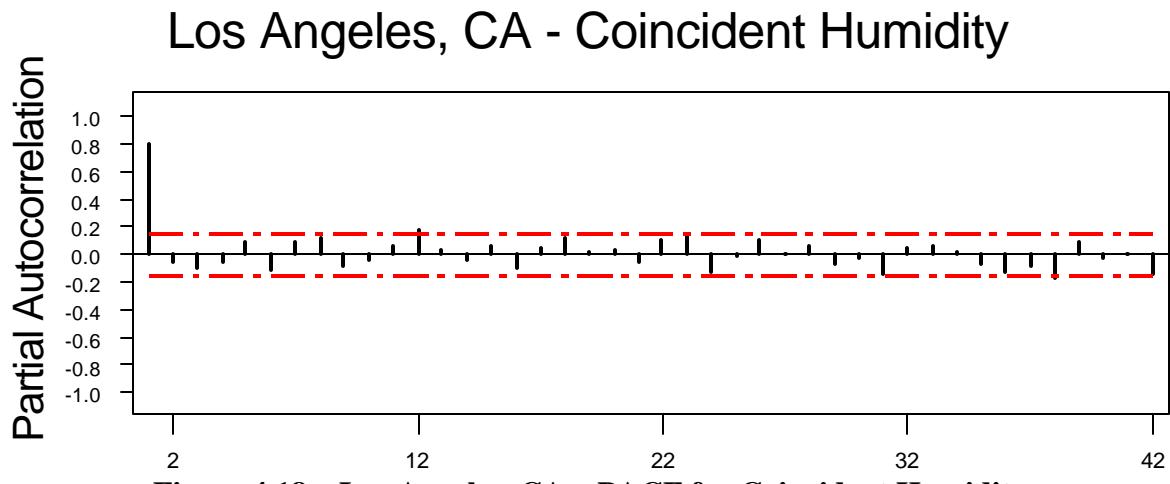


Figure 4.18 – Los Angeles, CA – PACF for Coincident Humidity

<b>Maximum Stand-Alone Humidity</b>		
Location	ACF Behavior	PACF Behavior
alb07	c/o 1 lag	c/o 1 lag
atl07	slow decay	c/o 1 lag
bal07	slow decay	c/o 1 lag
cha07	c/o 3 lags	c/o 1 lag
chi07	sinusoid	c/o 1 lag
hou07	slow decay	c/o 1 lag
kan07	slow decay	c/o 1 lag
los07	slow decay	c/o 1 lag
mad07	slow decay	c/o 1 lag
mia07	c/o 2 lags	c/o 1 lag
new07	slow decay	c/o 1 lag
san07	slow decay	c/o 2 lags
sea07	c/o 1 lag	c/o 1 lag
wes07	slow decay	c/o 2 lags

**Table 4.2 – Stand-Alone Humidity**

<b>Maximum Coincident Humidity</b>		
Location	ACF Behavior	PACF Behavior
alb07	slow decay	c/o 1 lag
atl07	slow decay	c/o 1 lag
bal07	slow decay	c/o 1 lag
cha07	c/o 2 lags	c/o 1 lag
chi07	slow decay	c/o 1 lag
hou07	sinusoid	c/o 2 lags
kan07	slow decay	c/o 1 lag
los07	c/o 3 lags	c/o 1 lag
mad07	slow decay	c/o 1 lag
mia07	c/o 2 lags	c/o 1 lag
new07	c/o 3 lags	c/o 1 lag
san07	c/o 1 lag	c/o 1 lag
sea07	slow decay	c/o 1 lag
wes07	c/o 3 lags	c/o 1 lag

**Table 4.3 – Coincident Humidity**

#### 4.2.2 Model Fitting and Evaluation

Based on the characteristics of the ACF and PCF for the locations studied an AR(1) was fit to the data and the residuals examined to validate the adequacy of this model. The general form of the AR(1) is:

$$\mathbf{w}_t = \mathbf{f}\mathbf{w}_{t-1} + \mathbf{d} + a_t \quad t = 1, 2, \dots \quad (4.1)$$

where:  $\mathbf{w}_t$  = humidity ratio at time  $t$ , lb<sub>w</sub>/lb<sub>a</sub>

$\mathbf{f}$  = first order auto-regressive coefficient

$$\mathbf{d} = (1 - \mathbf{f})\mathbf{m}$$

$\mathbf{m} = E(Y_t)$ , average humidity ratio over the sequence, lb<sub>w</sub>/lb<sub>a</sub>

$a_t$  = white noise process with 0 mean and constant variance

Tables 4.4 and 4.5 summarize the results of the AR(1) fit to the stand-alone and coincident

Maximum Stand-Alone Humidity				
Location	$\mathbf{f}$	$\mathbf{m}$	var( $a_t$ )	ACF of Residuals
alb07	0.562	12.5	1.289	OK
atl07	0.888	19.2	0.355	OK
bal07	0.819	18.0	0.503	OK
cha07	0.737	20.3	0.838	OK
chi07	0.874	18.2	1.171	NOK
hou07	0.731	19.4	0.344	OK
kan07	0.774	18.6	0.549	OK
los07	0.904	13.0	0.091	OK
mad07	0.899	16.4	0.817	OK
mia07	0.612	19.2	1.213	OK
new07	0.851	17.5	0.611	OK
san07	0.595	9.9	0.172	OK
sea07	0.39	10.1	0.385	OK
wes07	0.517	19.1	0.338	OK
Average	0.725		0.620	

Table 4.4 – Stand-Alone Humidity

Maximum Coincident Humidity				
Location	<b>f</b>	<b>m</b>	var( $a_t$ )	ACF of Residuals
alb07	0.852	7.8	0.437	OK
atl07	0.837	19.2	0.466	OK
bal07	0.896	17.1	0.540	OK
cha07	0.704	17	1.363	NOK
chi07	0.907	15.5	0.495	OK
hou07	0.907	17	0.630	OK
kan07	0.914	14.1	0.633	OK
los07	0.799	12.8	0.541	OK
mad07	0.954	15.4	0.463	OK
mia07	0.545	18.3	0.858	OK
new07	0.875	12.2	1.488	OK
san07	0.578	9.2	0.342	OK
sea07	0.924	8.5	0.172	OK
wes07	0.74	18.6	0.807	OK
Average	0.817		0.710	

**Table 4.5 – Coincident Humidity**

humidity ratios. The residuals that result from an adequate fit will behave as white noise. In other words, they should have a mean of zero and be stationary, uncorrelated and normally distributed. Of these criteria uncorrelated residuals are the most important feature. The residual ACF behavior is also summarized in Tables 4.4 and 4.5. The NOK designation indicates that AR(1) did not adequately model the series. The ACF plots of the residuals may be found in Appendix D. A  $f$  of 0.8 was chosen for the generator. To complete the AR(1) model estimates of the series average,  $m$  and the white noise,  $a_t$  are needed and these are provided in the next sections.

### 4.2.3 Estimation of Humidity Series Average

The approach used to develop relationships to estimate the stand-alone and coincident humidity is similar to that used for temperatures in Chapter 3. Stepwise regressions were performed using only the same readily available parameters as in the temperature regressions of Chapter 3 to determine the best predictors. The regression equation was then modified if necessary based on the residual analysis. The same development and test locations used for the regressions of Chapter 3 were used for the humidity sequences.

#### 4.2.3.1 Estimation Stand-Alone Humidity and Coincident Dry-Bulb Temperature

The following relationship for the maximum “stand-alone” humidity as a function of average monthly dry bulb temperature ( $^{\circ}\text{F}$ ), average monthly humidity ratio (\* 1000) and the longitude (degrees) was obtained as shown in equation (4.2).

$$\begin{aligned} \mathbf{w}_{sa,\max} = & -17.8 + 0.0717\bar{T}_{mon} + 2.85\mathbf{v}_{mon} + 0.395long - 0.00235long^2 \\ & - 0.0242\bar{T}_{mon}\mathbf{v}_{mon} \end{aligned} \quad (4.2)$$

$$s = 0.69, R^2 = 98.4\%$$

where:  $\mathbf{w}_{sa,\max}$  = maximum average stand-alone humidity ration\*1000,  $\text{lb}_w/\text{lb}_a$

$\bar{T}_{mon}$  = monthly average dry bulb temperature,  $^{\circ}\text{F}$

$\mathbf{v}_{mon}$  = average monthly humidity ratio\*1000,  $\text{lb}_w/\text{lb}_a$

$long$  = longitude, degrees

$s$  = standard deviation of the residuals,  $^{\circ}\text{F}$

$R^2$  = coefficient of determination

The coincident dry-bulb temperature was found to be related to the average monthly dry-bulb temperature, average annual temperature, latitude, monthly clearness index and the average

humidity ratio (\* 1000) as shown in equation (4.3). Tables 4.5 and 4.6 show the actual and estimated temperature and humidity ratios and the error for each of the test and development locations.

$$T_{sa,max} = -52.7 + 0.916\bar{T}_{mon} + 0.916\bar{T}_{yr} + 1.42f - 45.2\bar{K}_t - 0.00195v_{mon}^3 \quad (4.3)$$

$$s = 3.4 \text{ } ^\circ\text{F}, \quad R^2 = 94.9\%$$

where:  $T_{sa,max}$  = dry bulb temperature coincident with maximum stand alone humidity ratio,  ${}^\circ\text{F}$

$\bar{T}_{mon}$  = monthly average dry bulb temperature,  ${}^\circ\text{F}$

$f$  = latitude, degrees

$\bar{T}_{yr}$  = average annual dry bulb temperature,  ${}^\circ\text{F}$

$\bar{K}_t$  = average monthly clearness index

$v_{mon}$  = average monthly humidity ratio\*1000,  $\text{lb}_w/\text{lb}_a$

$s$  = standard deviation of the residuals,  ${}^\circ\text{F}$

$R^2$  = coefficient of determination

Development Locations				Test Locations			
Location	T <sub>coin,act</sub>	T <sub>coin,est</sub>	act-est	Location	T <sub>coin,act</sub>	T <sub>coin,est</sub>	act-est
	°F	°F	°F		°F	°F	°F
alb01	43.4	41.3	2.1	cha01	67.1	61.8	5.3
alb03	44.8	50.9	-6.1	cha03	68.4	67.7	0.7
alb07	74.6	77.2	-2.6	cha07	83.1	80.4	2.7
alb10	62.3	59.0	3.3	cha10	76.5	73.3	3.2
atl01	59.8	57.5	2.3	chi01	38.6	45.1	-6.5
atl03	61.5	65.9	-4.4	chi03	58.7	56.6	2.1
atl07	89.2	81.0	8.2	chi07	81.2	83.3	-2.1
atl10	68.8	71.2	-2.4	chi10	68.7	68.9	-0.2
bal01	50.2	54.2	-4.0	kan01	45.2	46.1	-0.9
bal03	65.4	62.4	3.0	kan03	59.7	60.0	-0.3
bal07	81.1	85.9	-4.8	kan07	81.5	82.6	-1.1
bal10	72.5	70.6	1.9	kan10	75.0	70.3	4.7
hou01	69.4	68.1	1.3	los01	60.8	66.5	-5.7
hou03	74.7	74.2	0.5	los03	62.4	65.2	-2.8
hou07	80.2	82.8	-2.6	los07	71.2	71.6	-0.4
hou10	81.0	77.3	3.7	los10	68.9	73.4	-4.5
mad01	36.2	36.8	-0.6	new01	47.6	56.5	-8.9
mad03	51.9	49.1	2.8	new03	55.3	63.6	-8.3
mad07	79.5	79.2	0.3	new07	81.1	90.0	-8.9
mad10	64.1	63.5	0.6	new10	73.1	76.5	-3.4
mia01	76.3	75.7	0.6	san01	58.2	64.9	-6.7
mia03	78.6	77.1	1.5	san03	57.2	64.3	-7.1
mia07	81.9	81.8	0.1	san07	64.9	67.0	-2.1
mia10	78.6	81.4	-2.8	san10	61.7	70.1	-8.4
sea01	74.5	76.2	-1.7	wes01	74.5	75.7	-1.2
sea03	75.5	75.0	0.5	wes03	75.5	77.0	-1.5
sea07	83.1	81.7	1.4	wes07	83.1	81.7	1.4
sea10	81.7	80.9	0.8	wes10	81.7	82.8	-1.1
Average			0.1	Average			-2.2
SD			3.1	SD			4.1

**Table 4.6 – Coincident Dry-Bulb Temperature**

Development Locations				Test Locations			
Location	$\omega_{\max,act} (*10^3)$	$\omega_{\max,est} (*10^3)$	act-est (*10 <sup>3</sup> )	Location	$\omega_{\max,act} (*10^3)$	$\omega_{\max,est} (*10^3)$	act-est (*10 <sup>3</sup> )
alb01	5.3	5.3	0.0	cha01	11.4	11.1	0.3
alb03	5.1	5.8	-0.7	cha03	12.0	13.1	-1.1
alb07	12.5	12.1	0.4	cha07	20.4	19.7	0.7
alb10	9.4	9.1	0.3	cha10	16.5	16.0	0.5
atl01	10.2	9.2	1.0	chi01	4.6	5.0	-0.4
atl03	10.3	11.4	-1.1	chi03	8.9	8.3	0.6
atl07	19.3	19.1	0.2	chi07	18.4	17.3	1.1
atl10	14.2	14.5	-0.3	chi10	11.7	12.1	-0.4
bal01	5.7	6.2	-0.5	kan01	5.7	5.5	0.2
bal03	9.2	8.4	0.8	kan03	9.6	9.0	0.6
bal07	18.0	17.5	0.5	kan07	18.6	17.7	0.9
bal10	13.8	13.1	0.7	kan10	14.5	12.6	1.9
hou01	12.2	12.2	0.0	los01	10.0	8.9	1.1
hou03	14.9	14.8	0.1	los03	9.8	10.2	-0.4
hou07	19.4	19.2	0.2	los07	13.0	14.3	-1.3
hou10	18.3	16.8	1.5	los10	12.7	12.4	0.3
mad01	3.9	4.1	-0.2	new01	5.0	5.6	-0.6
mad03	7.5	7.5	0.0	new03	7.0	7.6	-0.6
mad07	16.3	17.4	-1.1	new07	17.6	16.5	1.1
mad10	11.1	11.7	-0.6	new10	14.1	12.6	1.5
mia01	16.2	16.5	-0.3	san01	9.0	8.2	0.8
mia03	15.9	17.0	-1.1	san03	8.7	8.7	0.0
mia07	19.2	19.7	-0.5	san07	9.9	10.9	-1.0
mia10	18.9	19.0	-0.1	san10	10.0	10.3	-0.3
sea01	6.7	6.1	0.6	wes01	14.3	16.1	-1.8
sea03	7.1	6.9	0.2	wes03	15.5	16.7	-1.2
sea07	10.1	10.6	-0.5	wes07	19.1	20.0	-0.9
sea10	9.1	9.6	-0.5	wes10	18.2	18.7	-0.5
Average			0.0	Average			0.0
SD			0.6	SD			0.9

Table 4.7 – Maximum Stand-Alone Humidity

#### 4.2.3.2 Estimation of Coincident Humidity and Maximum Dry-Bulb Temperature

The coincident humidity ratio (\*1000) associated with the maximum dry-bulb temperature was found to be a function of average monthly humidity ratio (\*1000), longitude and the cross product term of  $\mathbf{v}_{mon}$  and  $\bar{T}_{mon}$ .

$$\mathbf{w}_{coin,max} = 0.070 + 4.76\mathbf{v}_{mon} - 0.000510long^2 - 0.0429\mathbf{v}_{mon}\bar{T}_{mon} \quad (4.4)$$

$$s = 1.0, R^2 = 96.8\%$$

where:  $\mathbf{w}_{coin,max}$  = humidity ratio (\*1000) coincident with maximum dry-bulb temperature, lb<sub>w</sub>/lb<sub>a</sub>

$\mathbf{v}_{mon}$  = average monthly humidity ratio\*1000, lb<sub>w</sub>/lb<sub>a</sub>

*long* = longitude, degrees

$\bar{T}_{mon}$  = monthly average dry bulb temperature, °F

s = standard deviation of the residuals, °F

$R^2$  = coefficient of determination

Tables 4.6 and 4.7 compare the actual and estimated coincident humidity for the development and test locations respectively. The maximum dry-bulb temperature correlation is the same as the one developed in chapter 3 (equation 3.6).

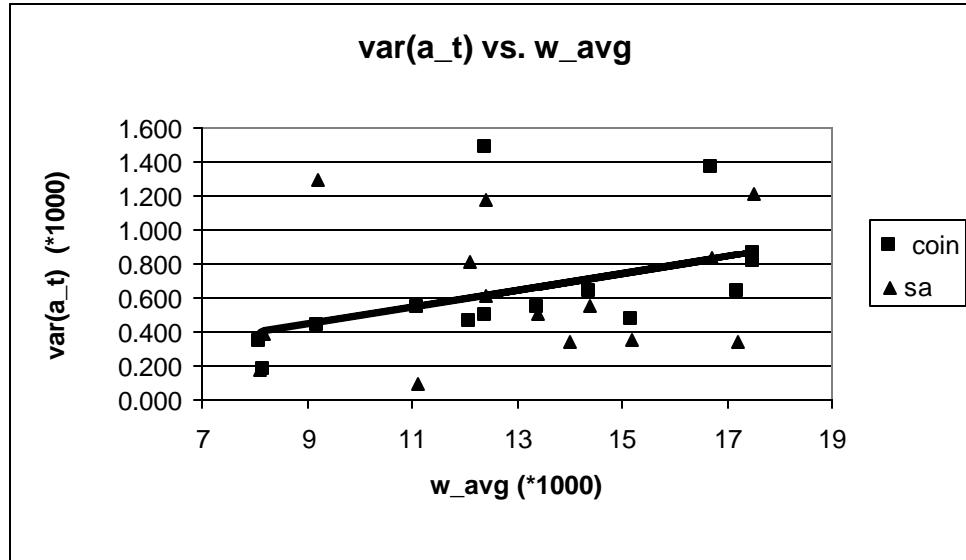
Development Locations				Test Locations			
Location	$\omega_{\text{coin,act}} (*10^3)$	$\omega_{\text{coin,est}} (*10^3)$	act-est (*10 <sup>3</sup> )	Location	$\omega_{\text{coin,act}} (*10^3)$	$\omega_{\text{coin,est}} (*10^3)$	act-est (*10 <sup>3</sup> )
alb01	2.5	2.9	-0.4	cha01	11.4	11.1	0.3
alb03	2.0	2.0	0.0	cha03	11.5	13.0	-1.5
alb07	7.8	7.5	0.3	cha07	16.9	18.9	-2.0
alb10	3.9	5.9	-2.0	cha10	15.4	16.1	-0.7
atl01	9.9	8.5	1.4	chi01	4.4	3.8	0.6
atl03	10.0	10.4	-0.4	chi03	8.8	7.2	1.6
atl07	19.2	18.2	1.0	chi07	15.6	16.0	-0.4
atl10	13.2	14.0	-0.8	chi10	11.7	11.3	0.4
bal01	5.5	5.5	0.0	kan01	5.0	3.8	1.2
bal03	8.7	7.7	1.0	kan03	6.1	7.4	-1.3
bal07	17.2	16.8	0.4	kan07	14.1	15.1	-1.0
bal10	13.8	13.4	0.4	kan10	6.5	11.1	-4.6
hou01	12.2	11.4	0.8	los01	4.3	6.8	-2.5
hou03	14.9	14.0	0.9	los03	6.9	8.8	-1.9
hou07	16.9	16.8	0.1	los07	12.8	13.4	-0.6
hou10	17.9	15.8	2.1	los10	5.8	11.0	-5.2
mad01	3.5	2.9	0.6	new01	5.0	5.1	-0.1
mad03	5.2	6.4	-1.2	new03	4.6	7.2	-2.6
mad07	15.8	16.4	-0.6	new07	12.7	15.9	-3.2
mad10	10.0	11.1	-1.1	new10	12.8	12.9	-0.1
mia01	16.1	16.6	-0.5	san01	9.0	7.5	1.5
mia03	15.1	16.5	-1.4	san03	8.2	7.7	0.5
mia07	18.4	18.3	0.1	san07	9.3	9.9	-0.6
mia10	17.4	18.3	-0.9	san10	6.7	9.2	-2.5
sea01	5.7	5.2	0.5	wes01	14.1	16.4	-2.3
sea03	7.1	5.7	1.4	wes03	14.0	16.5	-2.5
sea07	8.6	8.8	-0.2	wes07	18.6	18.9	-0.3
sea10	7.9	9.1	-1.2	wes10	17.5	18.1	-0.6
Average			0.0	Average			-1.1
SD			1.0	SD			1.7

Table 4.8 – Maximum Coincident Humidity

#### 4.2.4 Estimation of the White Noise

The variance of the white noise or residuals resulting from the AR(1) fits listed in Tables

4.4 and 4.5 was observed to be a weak function of the average monthly humidity



**Figure 4.19 – White Noise vs. Average Humidity Ratio**

ratio. Figure 4.19 plots both the variance of the “stand-alone” and the coincident white noise. A stepwise regression procedure was not used. The following correlation (with no intercept) was developed to estimate the variance of the white noise as a function of the average monthly humidity ratio (\*1000).

$$\text{var}(a_t) = 0.0496 \mathbf{v}_{mon} \quad (4.6)$$

$$s = 0.3637$$

where:  $\text{var}(a_t)$  = variance of the white noise

$\mathbf{v}_{mon}$  = average monthly humidity ratio\*1000,  $\text{lb}_w/\text{lb}_a$

s = standard deviation of the residuals

### 4.3 Comparison of Actual versus Generated Humidity Ratios

To gauge the accuracy of the generator actual extremes high sequences from the test location sites are compared to generated sequences. The test site locations used represent the smallest and largest errors (actual – estimated) of the extreme high “stand-alone” and coincident humidity ratios (\*1000) for the month of July months for a 7 day sequence. These locations and sequence are summarized in Table 4.10. The actual (dark line) versus generated (light line) data are plotted in Figures 4.20 through 4.27.

Location	Sequence Type	Error (act-est)
los07	stand-alone	1.3
cha07	stand-alone	0.7
wes07	coincident	0.3
hou07	coincident	0.1

**Table 4.9 – Maximum and Minimum Error for Generated Sequences**

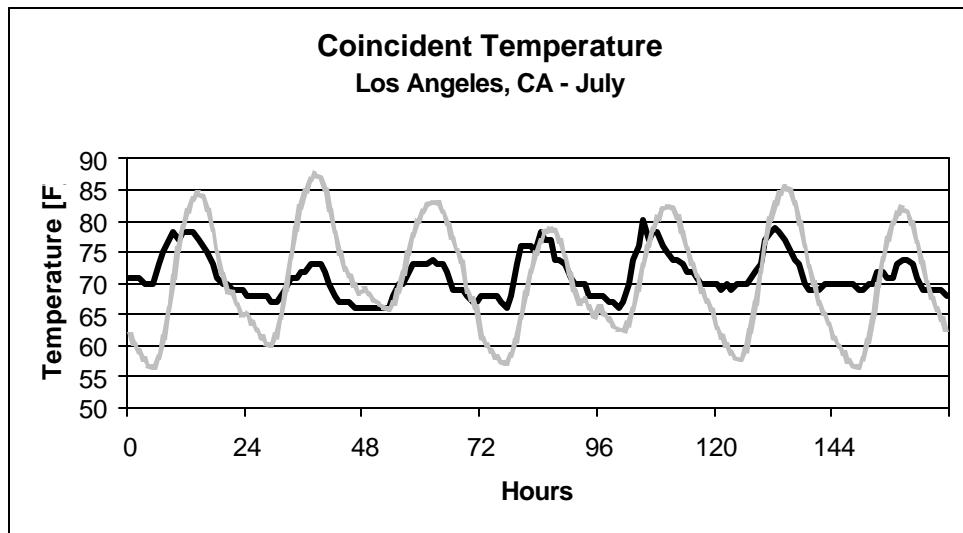


Figure 4.20 – Actual (dark) vs. Generated (light) Coincident Temperature – Large Error

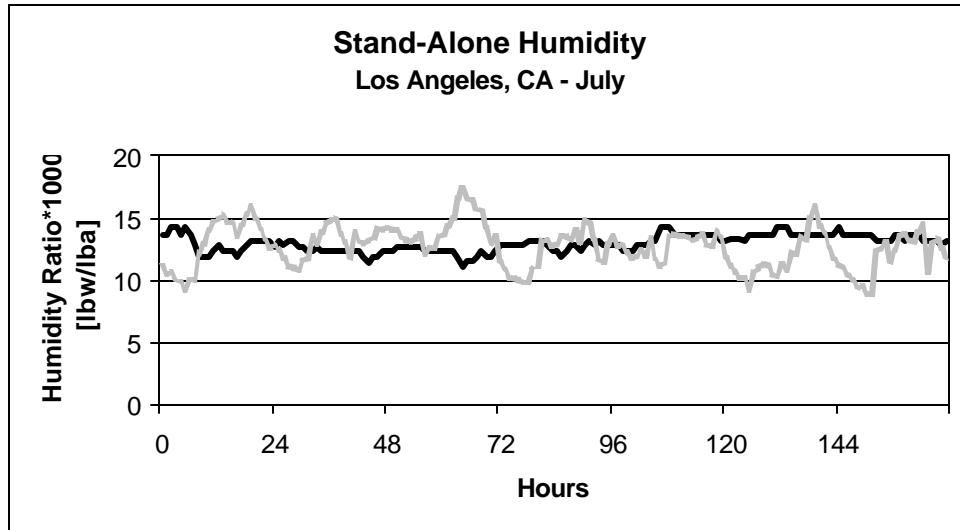
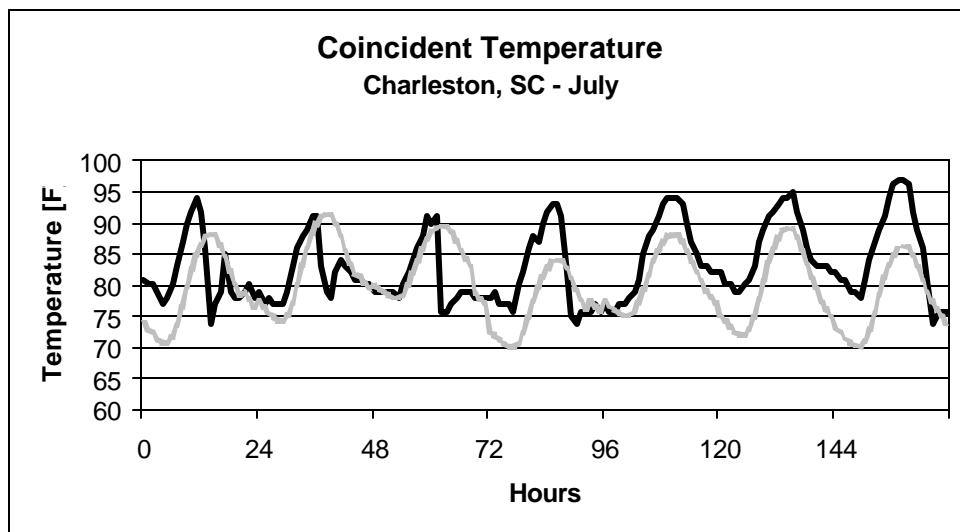
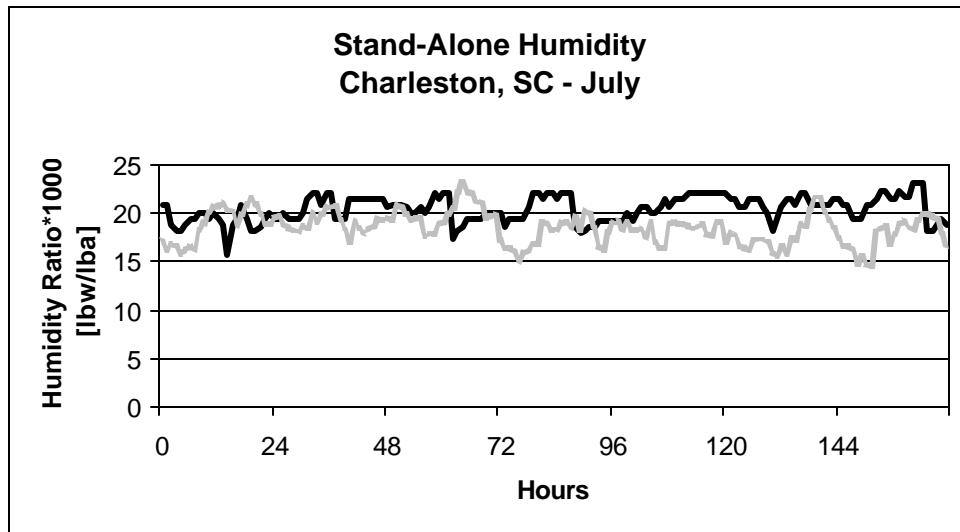


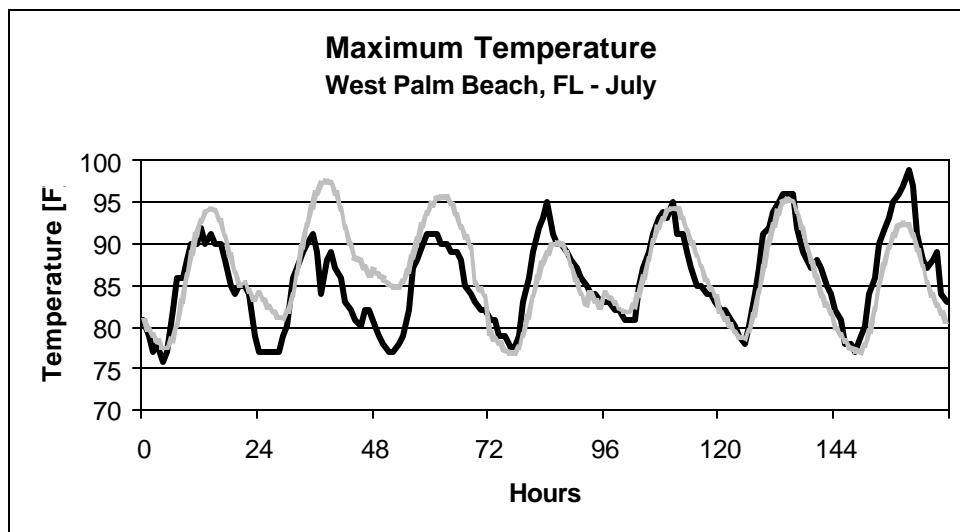
Figure 4.21 – Actual (dark) vs. Generated (light) Stand-Alone Humidity – Large Error



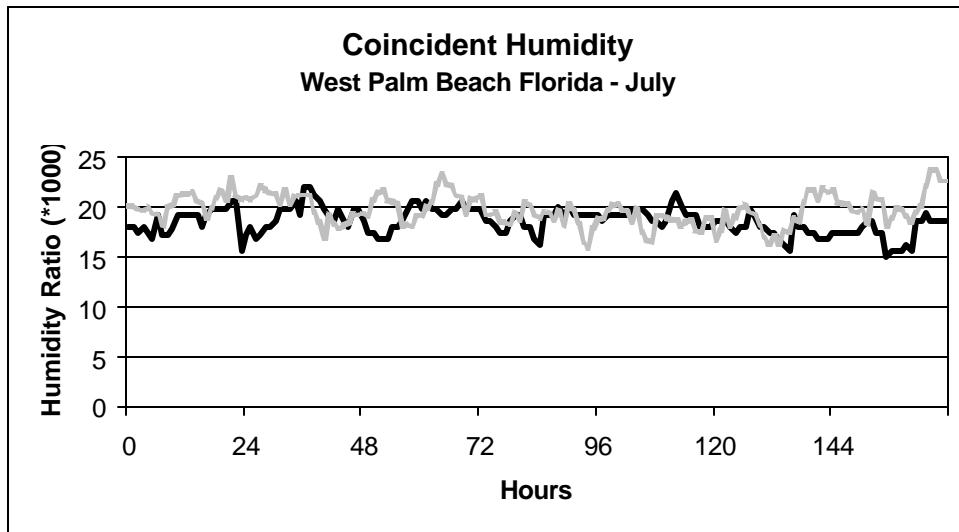
**Figure 4.22 – Actual (dark) vs. Generated (light) Coincident Temperature – Small Error**



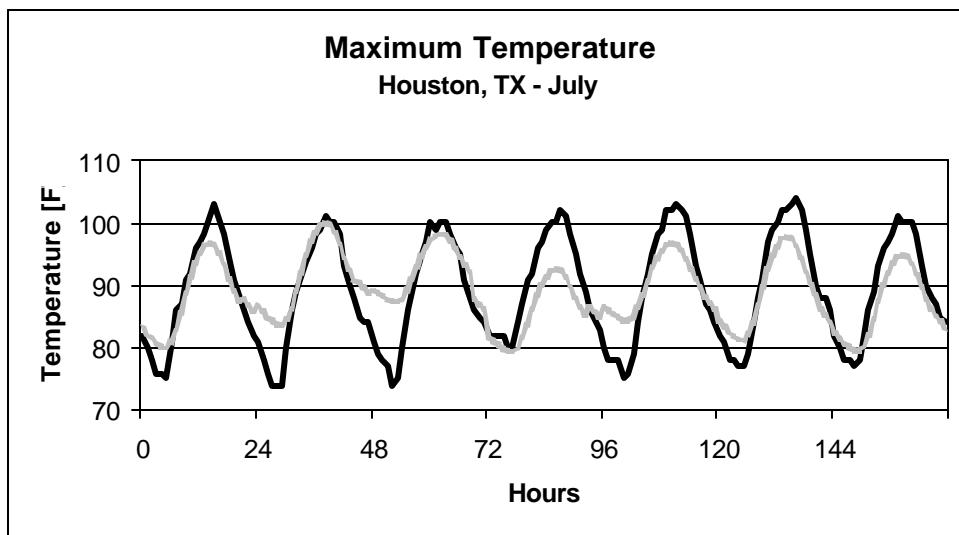
**Figure 4.23 – Actual (dark) vs. Generated (light) Stand-Alone Humidity – Small Error**



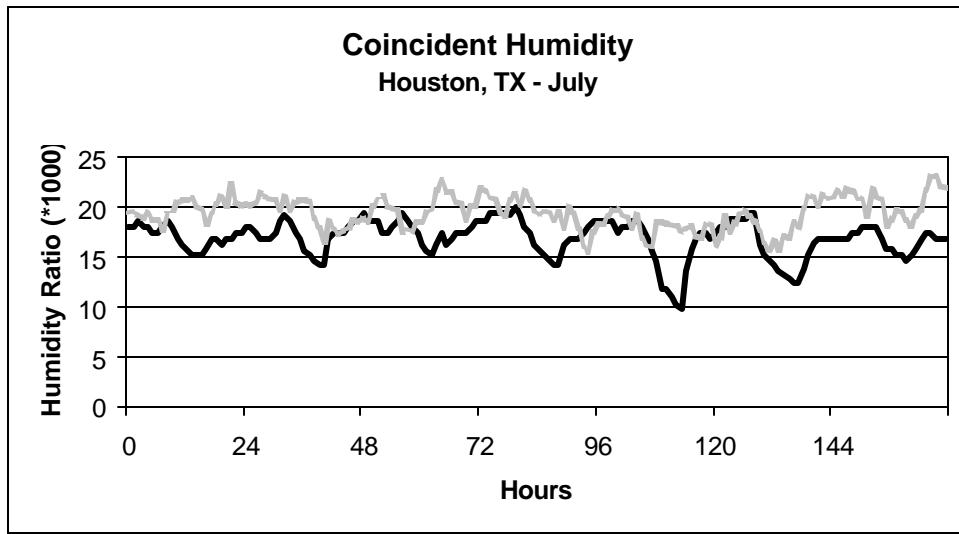
**Figure 4.24 – Actual (dark) vs. Generated (light) Maximum Temperature – Large Error**



**Figure 4.25 – Actual (dark) vs. Generated (light) Coincident Humidity – Large Error**



**Figure 4.26 – Actual (dark) vs. Generated (light) Maximum Temperature – Small Error**



**Figure 4.27 – Actual (dark) vs. Generated (light) Coincident Humidity – Large Error**

## Chapter 5

### Solar and Wind Sequences

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The goal for this phase of the project is to develop a methodology to characterize extreme sequences of total solar radiation on a horizontal surface and windspeed. One approach to characterizing extreme solar and wind sequences might be to apply the same techniques discussed in Chapter 3. Using these methods, correlations would first be developed to find the daily maximum or minimum solar radiation and windspeed. Then an algorithm would be formulated to determine the diurnal variation of solar radiation or windspeed for each day in the sequence followed by establishing a day-to-day ordering technique for multiple day sequence lengths. In addition, as was done on Chapter 4 for the joint relation between humidity and dry bulb temperature, a relationship between the solar radiation and the ambient temperature or windspeed may be investigated.

In some locations during the winter an extremely low dry bulb sequence may be associated with a series of clear days. Erbs [1984] considered the cross-correlation between ambient temperature and solar radiation and found that in most locations a pattern did exist on a seasonal basis. In general, large positive cross-correlations were observed in the summer months while negative or small cross-correlations were noted during the winter months. These cross-correlations are not modeled in the extreme weather generator. However, if it is known that a winter design sequence is associated with high solar radiation generated data that contains a low temperature and high solar sequence can be created.

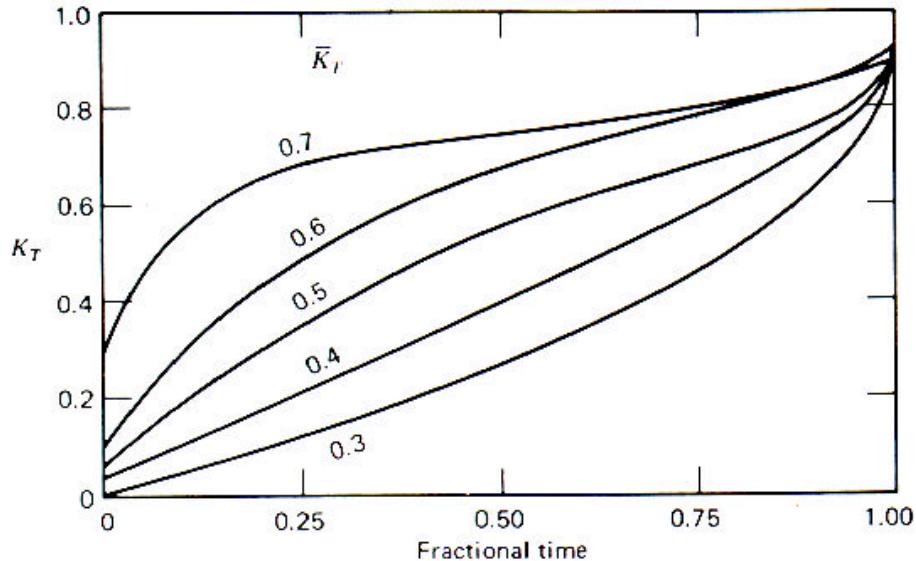
The attempt to follow the methodology of Chapter 3 for sequences of extremes solar radiation was unsuccessful. The predictor variables, that are available to develop correlations

to predict the total solar radiation for a day, were not sufficient. This is a result of the constraint that the generator must only use readily available data as inputs.

Fortunately, extensive work has been previously done to develop a location independent distribution of clear and cloudy days. This approach is outlined in the next section.

## 5.1 Solar Sequence Characterization

Liu and Jordan [Duffie and Beckman, 1991] developed a location independent distribution of clear and cloudy days. This distribution is shown in Figure 5.1. The curves represent the cfd (cumulative frequency distribution) of  $K_T$ , the daily clearness index as a function of  $\bar{K}_T$ , the monthly average daily clearness index. The clearness index is the ratio of the total solar radiation incident on a horizontal surface to the extraterrestrial radiation on a horizontal surface; both integrated over the desired time period. The method for



**Figure 5.1 – Distribution of Clear and Cloudy Days**

characterizing an extreme solar sequence based on these curves relies on selecting a point at the left (for a “low” solar sequence) and right (for a “high” solar sequence) tail of the distribution and centering the generated sequence about that point. Values of the daily  $K_T$  for each day in the sequence are determined by centering the sequence length (assuming a 31-day month) at 0.15 for a cloudy sequence and 0.85 for a clear sequence. This procedure is implemented in the extreme sequence generator using the equations developed by Bendt et al. [Duffie and Beckman, 1991] to mathematically represent the Liu and Jordan curves.

These equations are listed in 5.1 through 5.2 below. The equations fit the curves well for

$$f(K_T) = \frac{\exp(gK_{T,\min}) - \exp(gK_T)}{\exp(gK_{T,\min}) - \exp(gK_{T,\max})} \quad (5.1)$$

$$\bar{K}_T = \frac{\left( K_{T,\min} - \frac{1}{g} \right) \exp(gK_{T,\min}) - \left( K_{T,\max} - \frac{1}{g} \right) \exp(gK_{T,\max})}{\exp(gK_{T,\min}) - \exp(gK_{T,\max})} \quad (5.2)$$

where:  $\bar{K}_T$  = average monthly clearness index

$K_{T,\min}$  = minimum daily clearness index for a location

$K_{T,\max}$  = maximum daily clearness index for a location

$f(K_T)$  less than 0.9; above 0.9 they tend to over-estimate the  $K_T$ . However, these equations are inconvenient since they cannot be solved explicitly for  $g$ . Herzog [Duffie and Beckman, 1991] developed an explicit expression for  $g$  as shown in equations 5.3 and 5.4. A value of

$$g = -1.498 + \frac{1.184x - 27.182 \exp(-1.5x)}{K_{T,\max} - K_{T,\min}} \quad (5.3)$$

$$x = \frac{K_{T,\max} - K_{T,\min}}{K_{T,\max} - \bar{K}_T} \quad (5.4)$$

0.05 was suggested for  $K_{T,\min}$  by Bendt et al (Equation 5.5) and Hollands and Huget [Duffie and Beckman, 1991] recommend that Equation 5.6 be used to estimate  $K_{T,\max}$ . However, the actual implementation used in the extreme weather generator allows the user to specify the

$$K_{T,\min} = 0.05 \quad (5.5)$$

$$K_{T,\max} = 0.6313 + 0.267\bar{K}_T - 11.9(\bar{K}_T - 0.75)^8 \quad (5.6)$$

daily minimum and maximum clearness indices. Once the daily  $K_T$  is determined, the hourly clearness index,  $k_T$  may be estimated. One way to estimate the hourly total solar radiation values from the daily total is to use of generalized charts of  $r_t$  [Liu and Jordan], the ratio of total hourly to total daily radiation as shown in equation 5.7. The generalized  $r_t$  charts are based on monthly average data. The charts work best for clear days with increasingly uncertain results as total daily radiation decreases. The general algorithm is represented numerically in equations 5.8 through 5.9.

$$r_t = \frac{I}{H} \quad (5.7)$$

$$I = r_t H = r_t K_T H_o \quad (5.8)$$

$$r_t = \frac{\mathbf{p}}{24} (a + b + \cos \mathbf{w}) \frac{\cos \mathbf{w} - \cos \mathbf{w}_s}{\sin \mathbf{w} - \frac{\mathbf{p} \mathbf{w}_s}{180} \cos \mathbf{w}_s} \quad (5.9a)$$

$$a = 0.409 + 0.5016 \sin(\mathbf{w}_s - 60) \quad (5.9b)$$

$$b = 0.6609 - 0.4767 \sin(\mathbf{w}_s - 60) \quad (5.9c)$$

where:  $I$  = total hourly radiation,  $\frac{Btu}{ft^2}$

$$H_o = \text{total monthly radiation, } \frac{Btu}{ft^2}$$

$\omega_s$  = sunset hour angle (deg)

$\omega$  = hour angle (deg)

The hour angle,  $\omega$ , is the angular displacement of the sun east or west of the local meridian at a rate of 15°/hour. The sign convention is morning hours are negative while afternoon hours are positive.

## 5.2 Sequence Ordering

The ordering of each day in the sequence follows that developed by Knight [1988, 1991] that attempts to preserve the approximate one-lag autocorrelation.

## 5.3 Comparison of Actual versus Generated Solar Radiation

Tables 5.1 and 5.2 summarize the results of comparing the actual (dark line) and generated (light line) total solar radiation for four locations. Both a clear and a cloudy seven day sequence were used for comparison. Table 5.1 summarizes a hot month and Table 5.2 summarizes a cold month. Figures 5.3 through 5.9 illustrate the hot month sequences and Figures 5.10 through 5.18 show the cold month sequences. The actual and generated radiation data represent the total radiation integrated over the seven-day period. The data for the hot month, July, show that for the four locations investigated both the clear and cloudy generated sequences are within 10% of the actual sequence. However, the clear sequence is consistently biased high while the cloudy sequence is generally biased low. The data for the cold month, January, exhibit a similar trend. The clear sequence is biased high while the cloudy sequence is biased low. Based on these locations the generator tends to provide conservative design sequences. One possible reason for this behavior is that the lower the

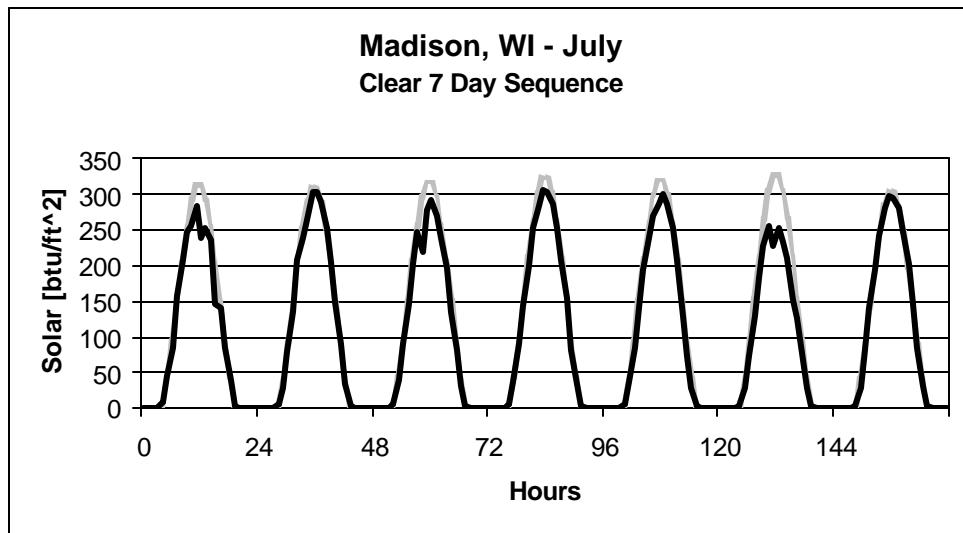
total daily radiation the more variable it becomes. This is evident both in terms of the total radiation over a day and the hourly values of the radiation. For example, a cloudy sequence can contain a sunny day while a clear sequence consists of only sunny days. In addition, the clear sequence does not appear to be affected by cloud cover while the cloudy sequence may display highly variable cloud cover. The cloud cover cannot be modeled using this purely deterministic technique. Of course, more locations need to be examined to determine if these observations are generally correct.

<b>7 Day Sequence - July</b>						
Location	Clear Sequence			Cloudy Sequence		
	Generated [btu/ft <sup>2</sup> ]	Actual [btu/ft <sup>2</sup> ]	% Diff	Generated [btu/ft <sup>2</sup> ]	Actual [btu/ft <sup>2</sup> ]	% Diff
mad07	19068.2	17452.4	9.3	8491.4	9403.5	-9.7
san07	19643.2	18405.3	6.7	12859.6	11521.7	11.6
atl07	18553.2	17436.6	6.4	7731.8	8120.9	-4.8
new07	18782.0	16815.6	11.7	7762.2	8493.7	-8.6

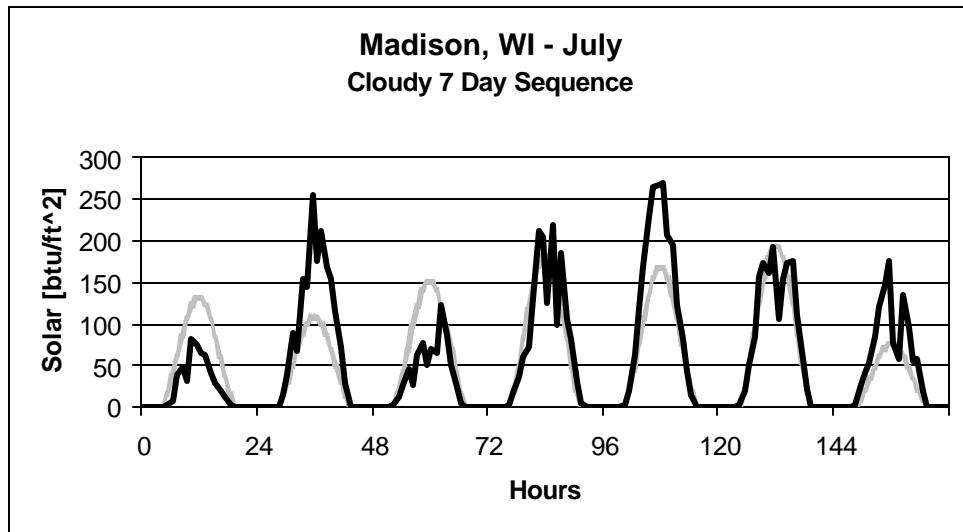
**Table 5.1 - Generated vs. Actual Clear and Cloudy Sequence – Hot Month**

<b>7 Day Sequence - January</b>						
Location	Clear Sequence			Cloudy Sequence		
	Generated [btu/ft <sup>2</sup> ]	Actual [btu/ft <sup>2</sup> ]	% Diff	Generated [btu/ft <sup>2</sup> ]	Actual [btu/ft <sup>2</sup> ]	% Diff
mad07	6472.0	6977.0	-7.2	1866.2	1796.1	3.9
san07	7269.2	6931.8	4.9	2042.4	2564.5	-20.4
atl07	8715.0	8341.5	4.5	2603.8	3329.8	-21.8
new07	6834.6	5947.9	14.9	1775.0	2524.3	-29.7

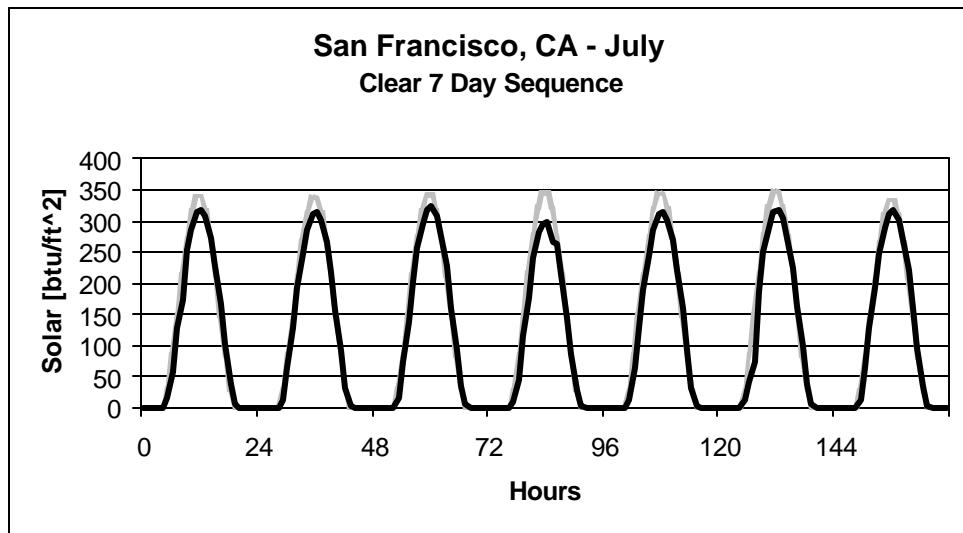
**Table 5.2 – Generated vs. Actual Clear and Cloudy Sequence – Cold Month**



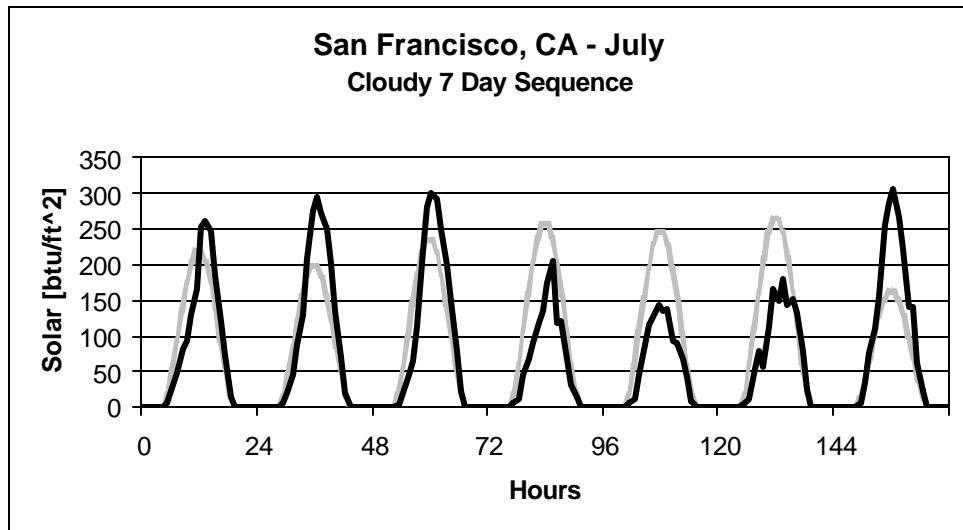
**Figure 5.2 - Actual (dark) vs. Generated (light) High Solar Sequence – Hot Month**



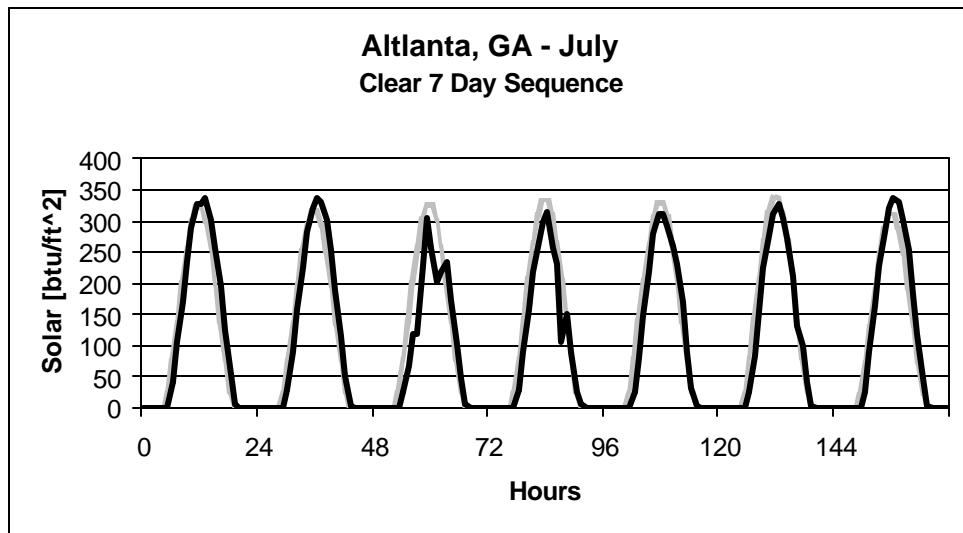
**Figure 5.3 – Actual (dark) vs. Generated (light) Low Solar Sequence – Hot Month**



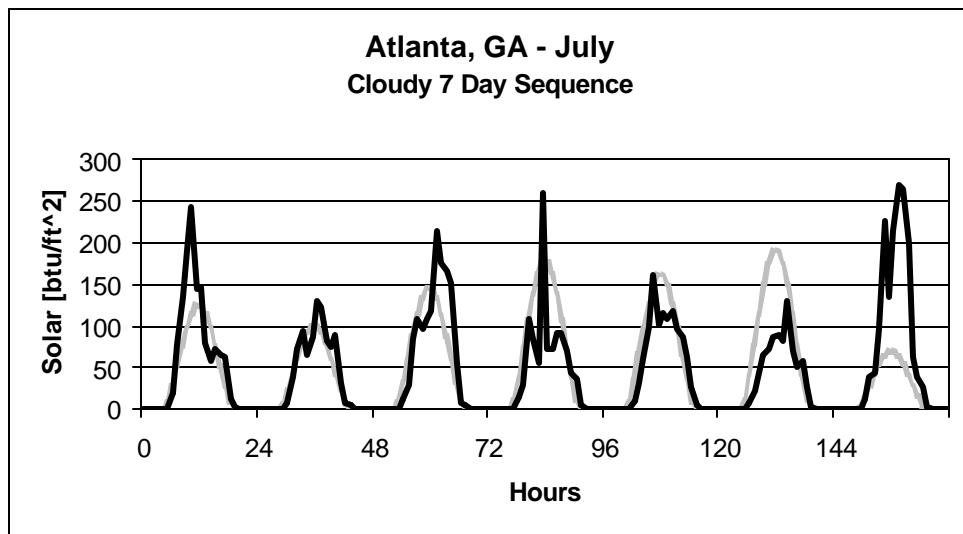
**Figure 5.4 – Actual (dark) vs. Generated (light) High Solar Sequence – Hot Month**



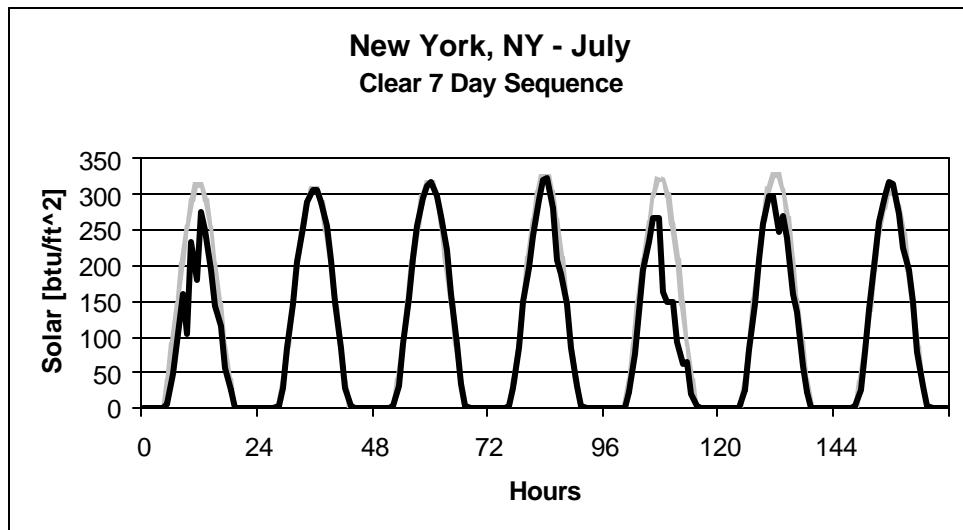
**Figure 5.5 – Actual (dark) vs. Generated (light) Low Solar Sequence – Hot Month**



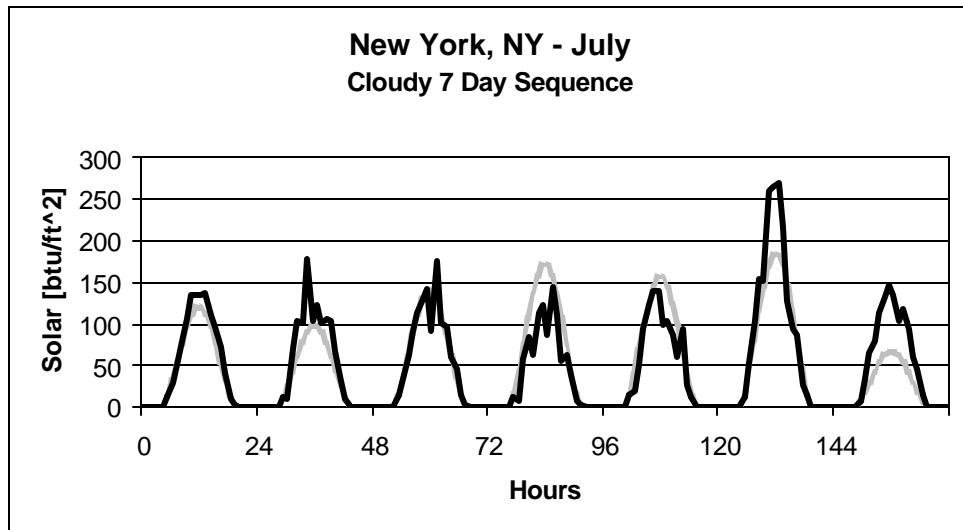
**Figure 5.6 – Actual (dark) vs. Generated (light) High Solar Sequence – Hot Month**



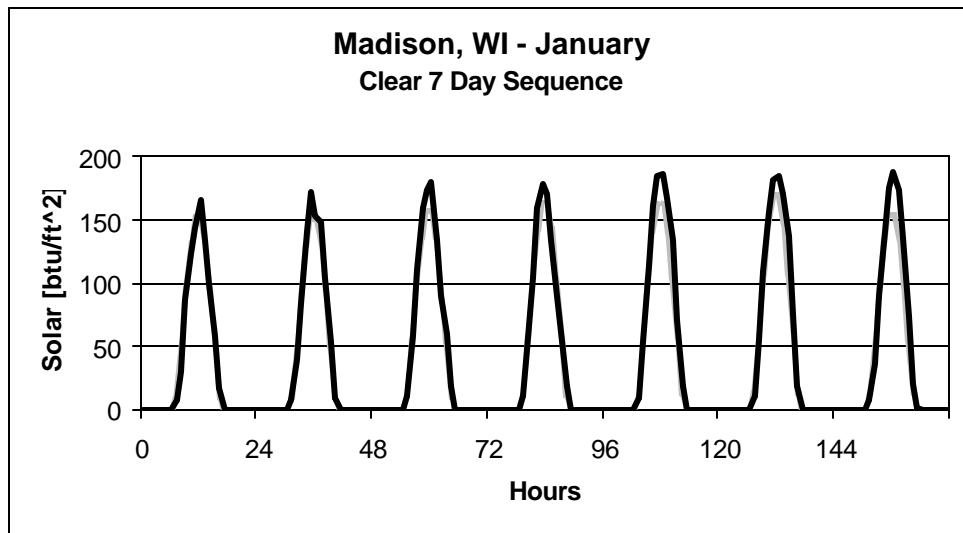
**Figure 5.7 – Actual (dark) vs. Generated (light) Low Solar Sequence – Hot Month**



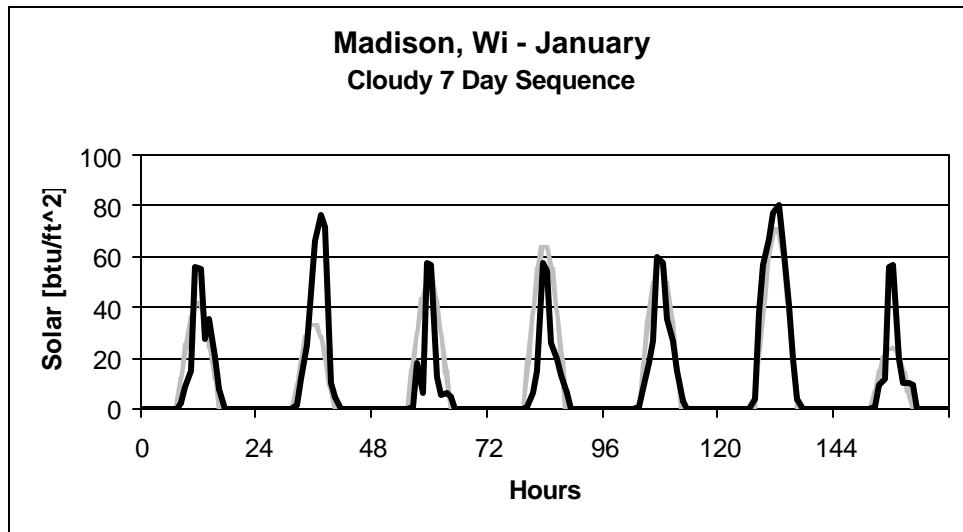
**Figure 5.8 – Actual (dark) vs. Generated (light) High Solar Sequence – Hot Month**



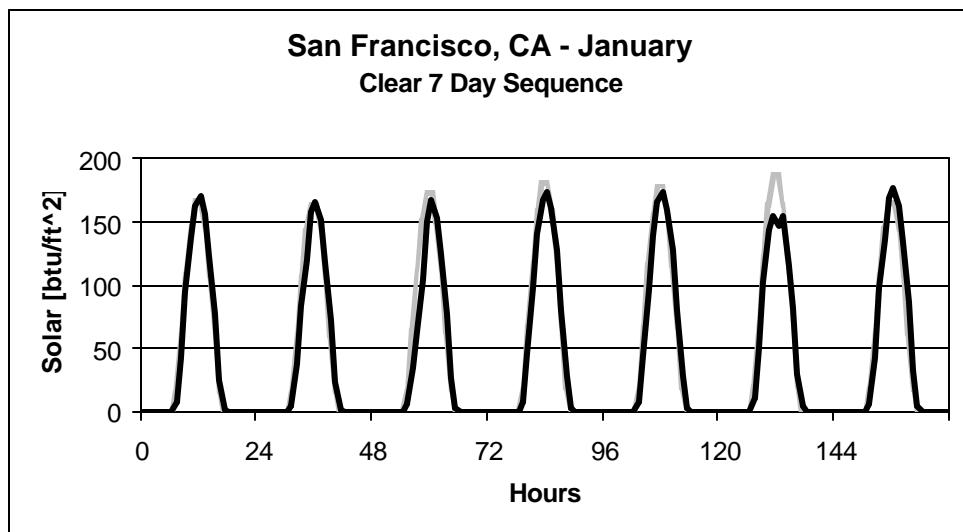
**Figure 5.9 - Actual (dark) vs. Generated (light) Low Solar Sequence – Hot Month**



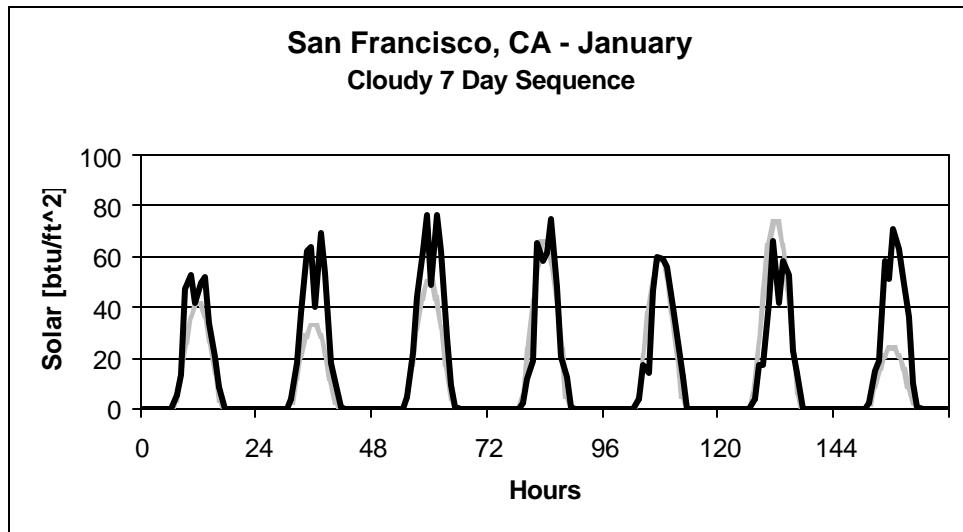
**Figure 5.10 – Actual (dark) vs. Generated (light) High Solar Sequence – Cold Month**



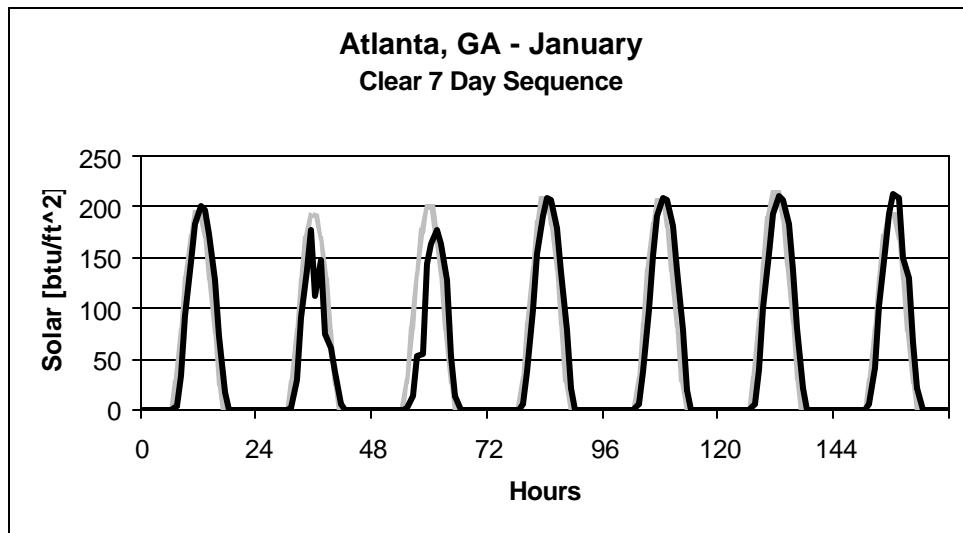
**Figure 5.11 – Actual (dark) vs. Generated (light) Low Solar Sequence – Cold Month**



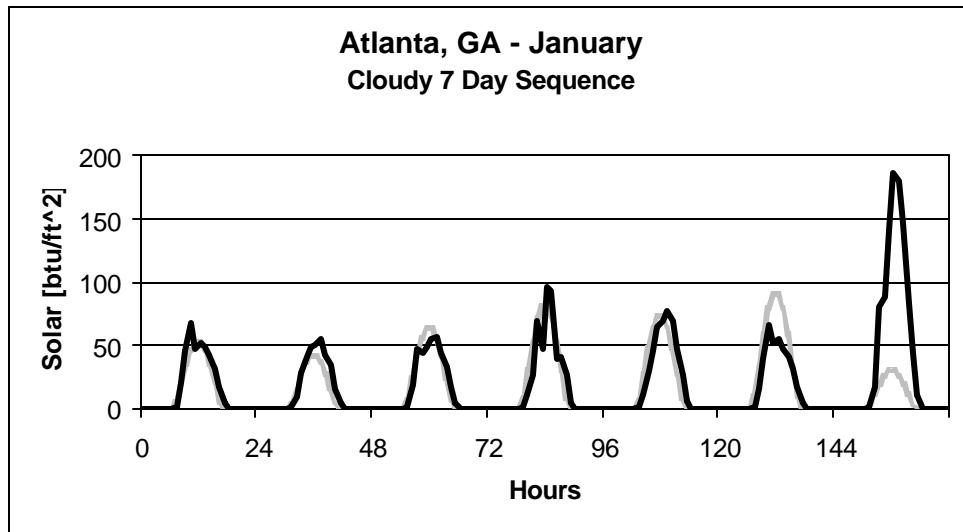
**Figure 5.12 – Actual (dark) vs. Generated (light) High Solar Sequence – Cold Month**



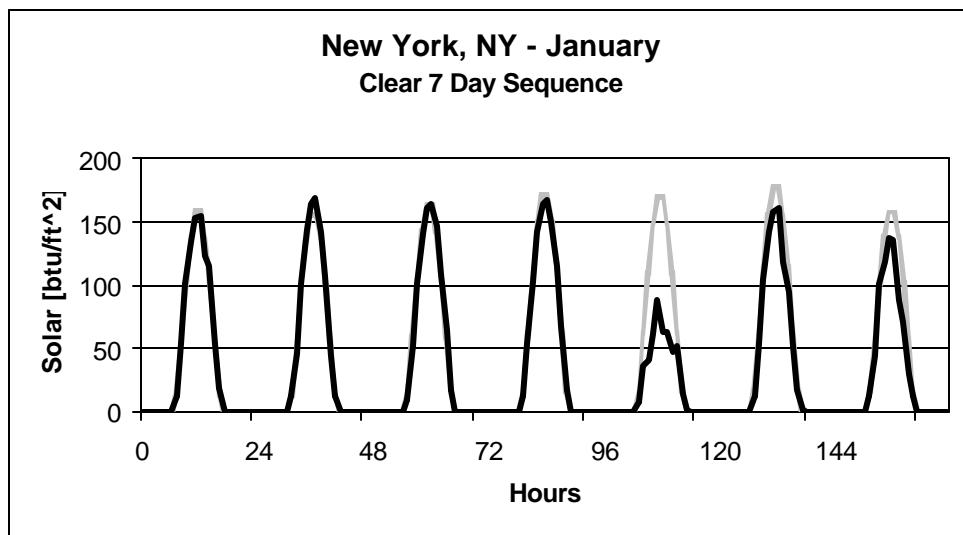
**Figure 5.13 – Actual (dark) vs. Generated (light) Low Solar Sequence – Cold Month**



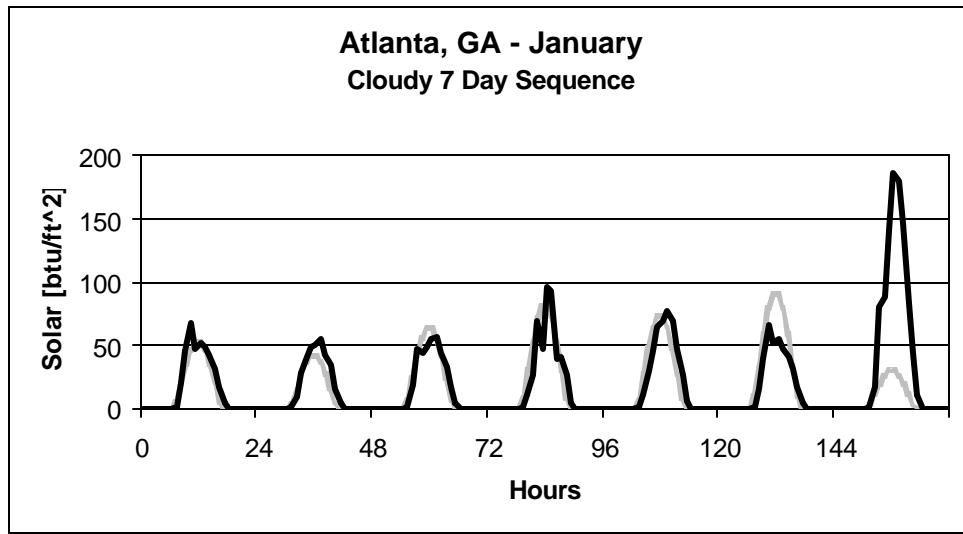
**Figure 5.14 – Actual (dark) vs. Generated (light) High Solar Sequence – Cold Month**



**Figure 5.15 – Actual (dark) vs. Generated (light) Low Solar Sequence – Cold Month**



**Figure 5.16 – Actual (dark) vs. Generated (light) High Solar Sequence – Cold Month**



**Figure 5.17 – Actual (dark) vs. Generated (light) Low Solar Sequence – Cold Month**

## 5.4 Wind Sequence Characterization

### 5.4.1 Wind Sequence Generation

The Degelman [Knight, 1988] wind model is currently used. This model assumes the wind sequence is a normally distributed white noise. Given an average wind speed over the sequence the standard deviation for each day in the sequence is equal to 0.31 times the average value or

$$\overline{ws}_{day} = \overline{ws}_{mon} \pm 0.31\overline{ws}_{mon} \quad (5.10)$$

Then each hour for the day is determined using :

$$\overline{ws}_{hour} = \overline{ws}_{day} \pm 0.35\overline{ws}_{day} \quad (5.11)$$

where:  $\overline{ws}_{mon}$  = average monthly windspeed, [mph]

$\overline{ws}_{day}$  = average daily windspeed, [mph]

$\overline{ws}_{hour}$  average hourly windspeed, [mph]

In addition, Degelman also noted that there is a diurnal variation of hourly windspeeds. This is not incorporated in the current model. Other researchers [Knight, 1988] have used modeled windspeed using other distributions such as Weibull and chi-squared distributions.

### 5.4.2 Sequence Ordering

The ordering of each day in the sequence is adapted from Knight [1988].

## Chapter 6

### Conclusions and Recommendations

---

#### 6.1 Temperature Sequence

The average temperature for an extreme day was estimated using regression equations. Then a technique was developed to estimate the average temperature for each day in a multiple day sequence. The average temperature for each day was then decomposed into hourly values using a deterministic expression that modeled the diurnal temperature variation for a day from average daily data.

The correlations used to estimate the extreme average temperature over a 24-hour period were formulated using data from the continental United States. Extrapolation of these correlations, for example to use them for Canadian or European locations, must be done with care, if at all. If over time, the methodology developed for this project to generate the extreme temperature sequence proves adequate, correlations for any locations can be easily developed given the availability of the data needed to determine them.

No significant difference in the diurnal variation of extreme day compared to an average was found in this study. Therefore, the hourly dry-bulb temperature was modeled using a completely deterministic approach developed for an average day. This procedure appears to be adequate for use at locations in the continental United States. Other investigators [Knight, 1988] have modeled the ambient temperature by removing the deterministic component and modeling the residuals. They found that an AR(2) model adequately represented the residuals for all of the locations examined. However, the

parameters of the AR(2) were different for each location. Knight [1988] fit an AR(2) model to three locations for each month in the year. No pattern was detected in the variation of the AR(2) parameters. Whether the use of a stochastic model compared to a purely deterministic model would make a substantial difference in the final design of a system or component is a possibly area for further study.

## 6.2 Humidity Sequence

The average extreme high “stand-alone” and coincident humidity ratio over a 7-day period is estimated using correlations developed with data from the continental United States. The same cautions that were noted for the temperature correlations also apply to the humidity correlations. A time series analysis was performed on the humidity ratio. It is interesting to note, that for the all of the locations examined in this study, the behavior of the humidity ratio was remarkably similar (except for 3 cases where an AR(2) may have been more appropriate) for both the maximum stand-alone and coincident sequences. This observation may indicate that the underlying physical process is similar regardless of the amount of water in the air. A further area of study would be to test this using other locations.

Both the maximum stand-alone/coincident temperature and the maximum temperature/coincident humidity sequences were tied together using regression equations. Another possible area for further investigation would be to associate these sequences using a transfer function model. The transfer function model relates an output time series to one or more input time series.

### **6.3 Solar Sequence**

The extreme solar sequence generated using the methodology presented in this project is totally deterministic using the cumulative distribution curves developed by Liu and Jordan. Stochastic radiation models have also been developed. The impact of using a stochastic model compared to a deterministic model in an energy simulation program on the final design of a system or component would be an area for further research.

In addition, the cross-correlation between solar radiation and dry-bulb-temperature was not considered in the study. Again this may be another area where the possibility to examine the utility of the times transfer function model.

### **6.4 Wind Speed Sequence**

The wind sequence generation model is an implementation of that developed by Degelman [Knight, 1988]. A time series analysis on the wind speed similar to that performed on the humidity ratio sequence could be done to determine if the white noise model currently used accurately represents the process over a one to seven day period. Again, the extra work to accomplish a more realistic sequence would need to be weighed against the benefit of improved component/system design using an energy simulation program.

### **6.5 Concluding Comments**

The construction of a location-independent, extreme weather sequence generator, using a small number of readily available parameters as input was the goal of this project. Clearly, many simplifications were made to allow the actual implementation of the algorithm. In many cases the relationship between certain parameters, such as solar radiation and ambient temperature was ignored. Perhaps the greatest deficiency is the lack of

knowledge of the importance each output parameter. However, this would require a parametric study that may be highly dependent on the load and system in question.

## Appendix A

### Extremes Program Listing

---

```

module comarea
implicit none

!-----
! Input Record
!
! xin (1) Sequence Length [Days]
!     (2) Sequence Type [Average = 0, Hot = 1, Cold = 2]
!     (3) Maximum Temperature [F]
!     (4) Minimum Temperature [F]
!     (5) Average Monthly Temperature [F]
!     (6) Average Monthly Clearness Index
!     (7) Average Monthly Humidity Ratio * 1000 [lbw/lba]
!     (8) Elevation [ft]
!     (9) Extreme Humidity Ratio * 1000 [lbw/lba]
!     (10) Sequence Order
!         [Autocorrelated = 1, Decreasing = 2, Increasing = 3]
!     (11) Month [ Jan = 1, Feb = 2, ...]
!     (12) Start Day of Sequence
!     (13) Longitude [degrees]
!     (14) Latitude [degrees]
!     (15) Average Monthly Wind Speed [mph]
!     (16) Random Sequence Indicator
!         [Constant Random Sequence = 0, Variable Random Sequence = 1]
!-----
type :: input_record
    double precision :: seqlength
    double precision :: seqtype
    double precision :: maxdbtemp
    double precision :: mindbtemp
    double precision :: avgdbtemp
    double precision :: Kt_bar
    double precision :: w_avg
    double precision :: elev
    double precision :: w_ext
    double precision :: seqorder
    double precision :: month
    double precision :: day
    double precision :: long
    double precision :: lat

```

```

    double precision :: avgwindspd
    double precision :: randseqind
    double precision :: extcall
end type input_record

! Global Constants
    double precision, parameter :: pi = 3.14159265359d0

end module comarea

!-----
! This subroutine is called by Extremes.exe and is the main driver
!-----

subroutine Extremes(XIN,TEMP,HUMID,SOLAR,XKT,WIND,
                     RELHUM,DEWPT,WETBULB,PRESS)

!MS$ATTRIBUTES ALIAS:'EXTREMES' :: EXTREMES
!MS$ATTRIBUTES DLLEXPORT :: EXTREMES

use comarea

implicit none

double precision :: TEMP(1:168),HUMID(1:168),SOLAR(1:168),
                   XKT(1:168),WIND(1:168),RELHUM(1:168),
                   DEWPT(1:168),WETBULB(1:168),PRESS
.
.
.

type (input_record) :: xin

    TEMP  = 0.d0
    HUMID = 0.d0
    SOLAR = 0.d0
    XKT   = 0.d0
    WIND   = 0.d0
    RELHUM = 0.d0
    DEWPT  = 0.d0
    WETBULB = 0.d0
    PRESS  = 0.d0

!-----
! Get the sequences
!-----

call DryBulbTemp(xin,TEMP)
call WindSpeed(xin,WIND)
call Humidity(xin,TEMP,HUMID,RELHUM,DEWPT,WETBULB,PRESS)

```

```

call SolarRad(xin,SOLAR,XKT)
xin%extcall = 0.d0

end subroutine Extremes

!-----
!  

! This subroutine is called by Extremes and generates the  

! extreme dry bulb temperature sequence
!-----

subroutine DryBulbTemp(xin,TEMP)

use comarea

implicit none

integer :: i,j,index,seqorder(1:7)

double precision :: avgseqtemp(1:7),tempratio,avgamp(1:7),
.           tstar,day(-2:24,1:7),std_dev,range,
.           randarray(1:168)

double precision :: TEMP(1:168)

type (input_record) :: xin

!-----
!  

! Initialize data
!-----

avgseqtemp = 0.d0
day      = 0.d0
avgamp   = 0.d0
std_dev  = 0.d0

!-----
!  

! Find the average temperature for the first day
!-----

range = 1.d0+35.6d0*xin%Kt_bar-0.000902d0*xin%w_avg**3
! Check daily range
if (range < 3.d0) then
  range = 3.d0
end if
if (range > 36.d0) then
  range = 36.d0
end if

```

```

std_dev = -30.8d0-0.000655d0*xin%elev+8.26d0*xin%Kt_bar+
.    0.756d0*xin%long-0.0196d0*xin%w_avg**2-
.    0.00395d0*xin%long**2
! Check standard deviation of daily range
if (std_dev < 2.8d0) then
  std_dev = 2.8d0
end if
if (std_dev > 8.9d0) then
  std_dev = 8.9d0
end if

call GaussDev(xin,randarray)

!-----
! Determine the average temperature for each day in the sequence
! after the first day
! Note: tempratio is Rankine/Rankine
!-----
do i=1,nint(xin%seqlength)

  select case (nint(xin%seqtype))
    case (0)                                ! average sequence
      avgseqtemp(i) = xin%avgdbtemp
    case (1)                                ! hot sequence
      tempratio    = 1.00165d0-0.00208d0*dfloat(i)
      avgseqtemp(i) = tempratio*(xin%maxdbtemp+460.d0)-460.d0
    case (2)                                ! cold sequence
      tempratio    = 0.998565d0+0.00296d0*dfloat(i)
      avgseqtemp(i) = tempratio*(xin%mindbtemp+460.d0)-460.d0
  end select

  avgamp(i) = range+std_dev*randarray(i)

end do

!-----
! Calculate the hourly dry bulb temperatures for each day of the
! sequence
!
! Note: Calculate from -2 to 24 hours for smoothing the end points
!       between the 24 hour sequences
!-----
do j=1,nint(xin%seqlength)
  do i=-2,24
    tstar = 2.d0*pi*dfloat(i-1)/24.d0
  end do
end do

```

```

day(i,j) = avgseqtemp(j) +
    avgamp(j)*(0.4632d0*cos(tstar-3.805d0) +
    0.0984d0*cos(2.d0*tstar-0.36d0) +
    0.0168d0*cos(3.d0*tstar-0.822d0) +
    0.0138d0*cos(4.d0*tstar-3.513d0))
end do
end do

!-----  

!     Autocorrelated sequence order  

!-----  

index = 0
if (nint(xin%seqorder) == 1) then
    select case (nint(xin%seqlength))
    case (1)
        do i=1,24
            TEMP(i) = day(i,1)
        end do
    case (2)
        seqorder = (/2,1,0,0,0,0,0/)
        do j=1,nint(xin%seqlength)
            do i=1,24
                TEMP(24*index+i) = day(i,seqorder(j))
            end do
            index = index+1
        end do
    case (3)
        seqorder = (/2,1,3,0,0,0,0/)
        do j=1,nint(xin%seqlength)
            do i=1,24
                TEMP(24*index+i) = day(i,seqorder(j))
            end do
            index = index+1
        end do
    case (4)
        seqorder = (/2,1,3,4,0,0,0/)
        do j=1,nint(xin%seqlength)
            do i=1,24
                TEMP(24*index+i) = day(i,seqorder(j))
            end do
            index = index+1
        end do
    case (5)
        seqorder = (/5,2,1,3,4,0,0/)
        do j=1,nint(xin%seqlength)

```

```

do i=1,24
  TEMP(24*index+i) = day(i,seqorder(j))
end do
  index = index+1
end do
case (6)
  seqorder = (/5,2,1,3,4,6,0/)
  do j=1,nint(xin%seqlength)
    do i=1,24
      TEMP(24*index+i) = day(i,seqorder(j))
    end do
    index = index+1
  end do
case (7)
  seqorder = (/5,2,1,7,3,4,6/)
  do j=1,nint(xin%seqlength)
    do i=1,24
      TEMP(24*index+i) = day(i,seqorder(j))
    end do
    index = index+1
  end do
end select

!-----
! Smooth the points between the 24 hour sequences - 1 through 24
! contains the actual 24 hour sequence. The extra data at -2, -1, 0
! are for smoothing purposes
!-----

index = 1
do j=2,nint(xin%seqlength)
  TEMP(24*index-2) = 0.5d0*
    . (TEMP(24*index-2)+day(-2,seqorder(j)))
  TEMP(24*index-1) = 0.5d0*
    . (TEMP(24*index-1)+day(-1,seqorder(j)))
  TEMP(24*index) = 0.5d0*(TEMP(24*index)+day(0,seqorder(j)))
  TEMP(24*index+1) = 0.5d0*(TEMP(24*index+1)+day(1,seqorder(j)))
  TEMP(24*index+2) = 0.5d0*(TEMP(24*index+2)+day(2,seqorder(j)))
  index = index+1
end do

```

```

!-----
!      Reverse the sequence order
!-----
else if
. ((nint(xin%seqtype) == 1 .and. nint(xin%seqorder) == 3) .or.
. (nint(xin%seqtype) == 2 .and. nint(xin%seqorder) == 2)) then

    do j=-nint(xin%seqlength),1
        do i=1,24
            TEMP(24*index+i) = day(i,-j)
        end do
        index = index+1
    end do

!-----
!      Leave the sequence order as is
!-----
else
    do j=1,nint(xin%seqlength)
        do i=1,24
            TEMP(24*index+i) = day(i,j)
        end do
        index = index+1
    end do
end if

end subroutine DryBulbTemp

!-----
!      This subroutine is called by the main driver and generates the
!      humidity ratio sequence
!-----
subroutine Humidity(xin,TEMP,HUMID,RELHUM,DEWPT,WETBULB,PRESS)

use comarea

implicit none

integer :: i

double precision :: a_t(1:168),phi,std_dev,Rel_Hum,
.           Dew_pt,p_w,p_w_95,w_95,p_sat,delta,
.           Wet_bulb,u(1:2),randarray(1:168)

```

```

double precision :: TEMP(1:168),HUMID(1:168),RELHUM(1:168),
DEWPT(1:168),WETBULB(1:168),PRESS
.
type (input_record) :: xin

!-----
! Initialize data
!-----
phi = 0.8d0
PRESS = 14.696d0*(1.d0-0.3048d0*(2.25577e-5)*xin%elev)**5.2559

!-----
! Calculate the humidity ratio at 95% RH
!-----
p_w_95 = 0.95d0*p_sat(TEMP(1))
w_95 = 1000.d0*(18.d0/29.d0)*p_w_95/(PRESS-p_w_95)

select case (nint(xin%seqtype))
case (0) ! average sequence
  if (xin%w_avg > w_95 .or. xin%w_avg <= 0.0) then
    HUMID(1) = w_95
  else
    HUMID(1) = xin%w_avg
  end if
  delta = xin%w_avg*(1.d0-phi)
  std_dev = dsqrt(0.0497*xin%w_avg)
case (1) ! hot sequence
  if (xin%w_ext > w_95 .or. xin%w_ext <= 0.0) then
    HUMID(1) = w_95
  else
    HUMID(1) = xin%w_ext
  end if
  delta = xin%w_ext*(1.d0-phi)
  std_dev = dsqrt(0.0497*xin%w_avg)
case (2) ! cold sequence
  if (xin%w_ext > w_95 .or. xin%w_ext <= 0.0) then
    HUMID(1) = w_95
  else
    HUMID(1) = xin%w_ext
  end if
  delta = xin%w_ext*(1.d0-phi)
  std_dev = dsqrt(0.0282*xin%w_avg)
end select

RELHUM(1) = Rel_Hum(TEMP(1),HUMID(1)/1000.d0,PRESS)

```

```

p_w      = HUMID(1)/1000.d0*PRESS/(18.d0/29.d0+HUMID(1)/1000.d0)
DEWPT(1) = Dew_pt(TEMP(1),p_w)
WETBULB(1) = Wet_bulb(TEMP(1),DEWPT(1),PRESS)

!-----
!      AR(1) to calculate the humidity ratio
!-----

call GaussDev( xin,randarray)
a_t = std_dev*randarray

do i=2,nint(24.0*xin%seqlength)
10   HUMID(i) = delta+phi*HUMID(i-1)+a_t(i)
      RELHUM(i) = Rel_Hum(TEMP(i),HUMID(i)/1000.d0,PRESS)
      ! Check to insure that relhum is between 0% and 100%
      if (RELHUM(i) < 0.d0 .or. RELHUM(i) > 100.d0) then
         call random_number(u)
         a_t(i) = std_dev*dsqrt(-2.d0*dlog(u(1)))*dcos(2.d0*pi*u(2))
         goto 10
      end if
      p_w = HUMID(i)/1000.d0*PRESS/((18.d0/29.d0)+HUMID(i)/1000.d0)
      DEWPT(i) = Dew_pt(TEMP(i),p_w)
      WETBULB(i) = Wet_bulb(TEMP(i),DEWPT(i),PRESS)
end do

end subroutine Humidity

!-----
!      FUNCTION Rel_Hum - Calculate the relative humidity [%]
!-----

function Rel_Hum(db_temp,w_act,p) result(rh)
  implicit none
  double precision :: rh,p_ws,db_temp,w_act,W_sat,mu,p_sat,p

  p_ws = p_sat(db_temp)
  w_sat = (18.d0/29.d0)*p_ws/(p-p_ws)
  mu   = w_act/w_sat
  rh   = 100.d0*(mu/(1.d0-(1.d0-mu)*(p_ws/p)))

end function Rel_Hum

```

```
!
!-----  

! FUNCTION p_sat - Calculate the saturation pressure at a given  

!           dry bulb temperature [psia]  

!-----  

function p_sat(temp) result(p_ws)  

implicit none  

double precision :: temp,p_ws,temp_abs  

temp_abs = temp+459.67d0  

if (temp < 32.d0) then  

    p_ws = dexp((-1.0214165e+04)/temp_abs      +  

.     (-4.8932428e+00)      +  

.     (-5.3765794e-03)*temp_abs      +  

.     ( 1.9202377e-07)*temp_abs**2  +  

.     ( 3.5575832e-10)*temp_abs**3 +  

.     (-9.0344688e-14)*temp_abs**4 +  

.     ( 4.1635019e+00)*dlog(temp_abs))  

else  

    p_ws = dexp((-1.0440397e+04)/temp_abs      +  

.     (-1.1294650e+01)      +  

.     (-2.7022355e-02)*temp_abs      +  

.     ( 1.2890360e-05)*temp_abs**2  +  

.     (-2.4780681e-09)*temp_abs**3 +  

.     ( 6.5459673e+00)*dlog(temp_abs))  

end if  

end function p_sat
```

```
!
!-----  

! FUNCTION Dew_pt - calculates the dew point temperature  

!-----
```

```
function Dew_pt(db_temp,p_w) result(dp_temp)  

implicit none  

double precision :: db_temp,p_w,alpha,dp_temp  

alpha = dlog(p_w)  

if (db_temp < 32.d0) then  

    dp_temp = 90.12d0+26.412*alpha+0.8927d0*alpha**2  

else  

    dp_temp = 100.45      +  

.     33.193*alpha      +  

.     2.319*alpha**2      +
```

```

.      0.17074*alpha**3      +
.      1.2063*(p_w**0.1984)
end if

end function Dew_pt

!-----
!  FUNCTION Wet_bulb - calculates the wet bulb temperature
!-----

function Wet_bulb(db_temp,dp_temp,p) result(wb_temp)
implicit none
integer :: i

double precision :: db_temp,dp_temp,p,p_ws_dp,W_dp,p_sat,W_sat,
.      wb_temp,wb_temp_lo,wb_temp_hi,wb_temp_guess,
.      W_guess,W

! get the water saturation pressure at the dew point
p_ws_dp = p_sat(dp_temp)

! get the humidity ratio at saturation at the dew point
W_dp = W_sat(p_ws_dp,p)

! provide initial guess values
wb_temp_lo = dp_temp
wb_temp_hi = db_temp
wb_temp_guess = wb_temp_lo+(wb_temp_hi-wb_temp_lo)/2.d0

! iterate to find the wet bulb temp
i = 0
do while (wb_temp_hi-wb_temp_lo > 0.001)
W_guess = W(db_temp,wb_temp_guess,p)
if (W_guess > W_dp) then
    wb_temp_hi = wb_temp_guess
    wb_temp_guess = wb_temp_lo+(wb_temp_hi-wb_temp_lo)/2.d0
else
    wb_temp_lo = wb_temp_guess
    wb_temp_guess = wb_temp_lo+(wb_temp_hi-wb_temp_lo)/2.d0
end if
i = i+1
end do

wb_temp = wb_temp_guess

end function Wet_bulb

```

```

!-----
!  FUNCTION W - Calculate the humidity ratio
!-----

      function W(db_temp,wb_temp,stn_press) result(W_act)
      implicit none
      double precision :: db_temp,wb_temp,stn_press,p_ws_wb,W_s_star,
     .                   W_act,p_sat,w_sat,num,den

      ! saturation press at the wet bulb temp
      p_ws_wb = p_sat(wb_temp)

      ! humidity ratio at the wet bulb temp
      W_s_star = W_sat(p_ws_wb,stn_press)

      ! humidity ratio at actual dry and wet bulb temps
      num = (1093.d0-0.556d0*wb_temp)*W_s_star-0.24d0*(db_temp-wb_temp)
      den = 1093.d0+0.444d0*db_temp-wb_temp
      W_act=num/den

   end function W

!-----
!  FUNCTION W_sat
!-----

      function W_sat(p_ws,p) result(W_s)
      implicit none
      double precision :: p_ws,p,W_s

      W_s = (18.d0/29.d0)*p_ws/(p-p_ws)

   end function W_sat

!-----
! This subroutine is called by the main driver and generates the
! wind sequence
!-----

      subroutine WindSpeed(xin,WIND)

      use comarea

      implicit none

      integer :: i,j,index,seqorder(1:7)

      double precision :: randarray1(1:168),randarray2(1:168),total,
```

```

.      day(1:24,1:7),avgdaywndspd,avgwindspd

double precision :: WIND(1:168)

type (input_record) :: xin

total = 0.d0
index = 0
call GaussDev(xin,randarray1)
call GaussDev(xin,randarray2)

do j=1,nint(xin%seqlength)
!   average wind speed for the day
    avgdaywndspd = xin%avgwindspd+
    .      0.31d0*xin%avgwindspd*randarray1(j)
!   average wind speed for the hour
    do i=1,24
        day(i,j) = avgdaywndspd+
        .      0.35d0*xin%avgwindspd*randarray2(24*index+i)
        if (day(i,j) < 0.d0) then
            day(i,j) = 0.d0
        end if
        total = total+day(i,j)
    end do
    index = index+1
end do

!-----
!   Order the wind sequence
!-----

index = 0
select case (nint(xin%seqlength))
  case (1)
    do j=1,24
      WIND(j) = day(j,1)
    end do
  case (2)
    seqorder = (/1,2,0,0,0,0,0/)
    do j=1,nint(xin%seqlength)
      do i=1,24
        WIND(24*index+i) = day(i,seqorder(j))
      end do
      index = index+1
    end do
  case (3)

```

```

seqorder = (/1,3,2,0,0,0,0/)
do j=1,nint(xin%seqlength)
  do i=1,24
    WIND(24*index+i) = day(i,seqorder(j))
  end do
  index = index+1
end do
case (4)
seqorder = (/1,4,3,2,0,0,0/)
do j=1,nint(xin%seqlength)
  do i=1,24
    WIND(24*index+i) = day(i,seqorder(j))
  end do
  index = index+1
end do
case (5)
seqorder = (/5,1,4,3,2,0,0/)
do j=1,nint(xin%seqlength)
  do i=1,24
    WIND(24*index+i) = day(i,seqorder(j))
  end do
  index = index+1
end do
case (6)
seqorder = (/5,1,6,4,3,2,0/)
do j=1,nint(xin%seqlength)
  do i=1,24
    WIND(24*index+i) = day(i,seqorder(j))
  end do
  index = index+1
end do
case (7)
seqorder = (/5,1,6,7,4,3,2/)
do j=1,nint(xin%seqlength)
  do i=1,24
    WIND(24*index+i) = day(i,seqorder(j))
  end do
  index = index+1
end do
end select

```

! Adjust the sequence average  
avgwindspd = total/dfloat(24\*nint(xin%seqlength))  
WIND = (xin%avgwindspd/avgwindspd)\*WIND

```
end subroutine WindSpeed
```

```
!-----  
!  FUNCTION GaussDev - Returns an array of normally distributed  
!  random numbers - N(0,1)  
!-----
```

```
!  Reference: Handbook of Mathematical Functions, p.953
```

```
!  
!  Creates a normally distributed random number from a  
!  uniform distribution with a mean of 0 and a standard  
!  deviation of 1  
!-----
```

```
subroutine GaussDev(xin,randarray)
```

```
use comarea
```

```
implicit none
```

```
integer :: i,seed(1:2)
```

```
double precision :: randarray(1:168),u(1:2)
```

```
type (input_record) :: xin
```

```
randarray = 0.d0
```

```
if (nint(xin%randseqind) == 0 .and. nint(xin%extcall) == 0 ) then  
  seed = (/987654321,123456789/)  
  call random_seed(put=seed(1:2))  
  xin%extcall = 1.d0  
end if
```

```
if (nint(xin%randseqind) == 1) then  
  call random_seed()  
end if
```

```
do i=1,24*nint(xin%seqlength)  
  call random_number(u)  
  randarray(i) = dsqrt(-2.d0*dlog(u(1)))*dcos(2.d0*pi*u(2))  
end do
```

```
end subroutine GaussDev
```

```

!-----  

! This subroutine is called by the main driver and generates the  

! solar sequence  

!-----  

subroutine SolarRad(xin,SOLAR,XKT)  

use comarea  

implicit none  

integer :: i,j,index,day_number,DayofYear,sunrise,sunset  

double precision :: phi,delta,omega_sunrise,omega_sunset,a,b,  

.      r_t,HourAngle,Ho,Io,omega,omega1,omega2,  

.      Kt(1:7)  

double precision :: SOLAR(1:168),XKT(1:168)  

type (input_record) :: xin  

index = 0  

! get the daily Kt's  

call DailyKt(xin,Kt)  

phi      = xin%lat*pi/180.d0  

day_number = DayofYear(nint(xin%month),nint(xin%day))  

do j=1,nint(xin%seqlength)
    delta = 0.40927d0*dsin(2.d0*pi*(284.d0+
        dfloat(day_number))/365.d0)  

.  

! calculate the sunset hour angle for the day
omega_sunset = dacos(-dtan(phi)*dtan(delta))
omega_sunrise = -omega_sunset  

! find the sunrise and sunset for the day
sunrise     = int(12.d0+omega_sunrise*180.d0/(15.d0*pi))
sunset      = nint(12.5d0+omega_sunset*180.d0/(15.d0*pi))  

Ho = (24.d0*3600.d0*1367.d0/pi)*(88.06e-6)*
.      (1.0+0.033d0*dcos(2.d0*pi*dfloat(day_number)/365.d0))*  

.      (dcos(phi)*dcos(delta)*dsin(omega_sunset)+  

.      omega_sunset*dsin(phi)*dsin(delta))
.
```

```
do i=sunrise,sunset
```

```

    omega1 = HourAngle(i-1)*pi/180.d0
    omega2 = HourAngle(i)*pi/180.d0

    omega = (omega1+omega2)/2.d0
    a   = 0.409d0+0.5016d0*dsin(omega_sunset-60.d0*pi/180.d0)
    b   = 0.6609d0-0.4767d0*dsin(omega_sunset-60.d0*pi/180.d0)
    r_t = pi/24.d0*(a+b*dcos(omega))*
    .   (dcos(omega)-dcos(omega_sunset))/(
    .   (dsin(omega_sunset)-(omega_sunset*
    .   dcos(omega_sunset)))
```

```

if (r_t <= 0.d0) then
    SOLAR(24*index+i) = 0.d0
    XKT(24*index+i)  = 0.d0
    goto 10
end if
```

! Make sure hour1 is > sunrise hour angle and < sunset hour angle

```

if (omega1 < omega_sunrise) then
    omega1 = omega_sunrise
end if
if (omega1 > omega_sunset) then
    omega1 = omega_sunset
end if
```

! Make sure hour2 is < sunset angle and > sunrise hour angle

```

if (omega2 > omega_sunset) then
    omega2 = omega_sunset
end if
if (omega2 < omega_sunrise) then
    omega2 = omega_sunrise
end if
```

```

    Io = (12.d0*3600.d0*1367.d0/pi)*(88.06e-6)*
    . (1.0d0+0.033d0*dcos(2.d0*pi*dfloat(day_number)/365.d0))*(
    . (dcos(phi)*dcos(delta)*(dsin(omega2)-dsin(omega1))+(
    . (omega2-omega1)*dsin(phi)*dsin(delta))

    if (Io <= 0.d0) then
        Io = 0.001d0
    end if
```

```
SOLAR(24*index+i) = r_t*Kt(j)*Ho
```

```

XKT(24*index+i) = SOLAR(24*index+i)/Io

10      end do
        index    = index+1
        day_number = day_number+1
end do

end subroutine SolarRad

!-----
! FUNCTION HourAngle - Convert the hour to hour angle
!-----
function HourAngle(hour) result(omega)
implicit none
integer :: hour
double precision :: omega

if (hour <= 12) then
    omega = -15.d0*dfloat(12-hour)
else
    omega = 15.d0*dfloat(hour-12)
end if

end function HourAngle

!-----
! FUNCTION DayofYear - Determine the day of the year
!-----
function DayofYear(month,day) result(day_number)
implicit none
integer :: month,day,day_number

select case (month)
case (1)
    day_number = day
case (2)
    day_number = day+31
case (3)
    day_number = day+59
case (4)
    day_number = day+90
case (5)
    day_number = day+120
case (6)
    day_number = day+151

```

```

case (7)
    day_number = day+181
case (8)
    day_number = day+212
case (9)
    day_number = day+243
case (10)
    day_number = day+273
case (11)
    day_number = day+304
case (12)
    day_number = day+334
end select

end function DayofYear

```

```
!-----
!  SUBROUTINE DailyKt - Determine the daily Kt for each day
!          in the sequence
!-----
```

```

subroutine DailyKt(xin,Kt)

use comarea

implicit none

integer :: i,seqorder(1:7)

double precision :: Kt(1:7),epsilon,Kt_min,Kt_max,gamma,
.           fraction,Kt_hold(1:7)

type (input_record) :: xin

Kt_max = 0.6313d0+0.267d0*xin%Kt_bar-11.9d0*
.       (xin%Kt_bar-0.75d0)**8
Kt_min = 0.05d0
epsilon = (Kt_max-Kt_min)/(Kt_max-xin%Kt_bar)
gamma = -1.498d0+(1.184*epsilon-27.182d0*dexp(-1.5d0*epsilon))/(
.       (Kt_max-Kt_min))

select case (nint(xin%seqtype))
  case (0)                               ! average sequence
    fraction = (0.5d0*31.d0-xin%seqlength/2.d0)/31.d0
  case (1)                               ! hot sequence

```

```

fraction = (0.85d0*31.d0-xin%seqlength/2.d0)/31.d0
case (2)                                ! cold sequence
  fraction = (0.15d0*31.d0-xin%seqlength/2.d0)/31.d0
end select

do i=1,nint(xin%seqlength)
  Kt_hold(i) = dlog(-fraction*(dexp(gamma*Kt_min)-
    dexp(gamma*Kt_max))+
    dexp(gamma*Kt_min))/gamma
  fraction = fraction+1.d0/31.d0
end do

!-----
!      Order the daily Kt's
!-----

select case (nint(xin%seqlength))
  case (2)
    seqorder = (/2,1,0,0,0,0,0/)
    do i=1,nint(xin%seqlength)
      Kt(i) = Kt_hold(seqorder(i))
    end do
  case (3)
    seqorder = (/3,2,1,0,0,0,0/)
    do i=1,nint(xin%seqlength)
      Kt(i) = Kt_hold(seqorder(i))
    end do
  case (4)
    seqorder = (/3,2,4,1,0,0,0/)
    do i=1,nint(xin%seqlength)
      Kt(i) = Kt_hold(seqorder(i))
    end do
  case (5)
    seqorder = (/3,2,4,5,1,0,0/)
    do i=1,nint(xin%seqlength)
      Kt(i) = Kt_hold(seqorder(i))
    end do
  case (6)
    seqorder = (/3,2,4,6,5,1,0/)
    do i=1,nint(xin%seqlength)
      Kt(i) = Kt_hold(seqorder(i))
    end do
  case (7)
    seqorder = (/3,2,4,6,5,7,1/)
    do i=1,nint(xin%seqlength)
      Kt(i) = Kt_hold(seqorder(i))
    end do
end select

```

```
    end do  
end select  
  
end subroutine DailyKt
```

## Appendix B

### Extreme Sequences

---

Summary pages listing extreme sequence information for each location and month examined are contained in this Appendix. The format of each page is presented below.

<b>Extreme Sequence Summary Page Format</b>	
Column Number	Description
1	Location and month
2	Sequence length [days]
3	Sequence type (see table below)
4	Year
5	End day of sequence
6	Extreme
7	Coincident
8 through 14	Daily clearness index

Sequence Type	Description
DB/MHR	Maximum and minimum dry bulb temperature and coincident humidity ratio
HR/MDB	Maximum and minimum humidity ratio and coincident dry bulb temperature
G/MDB	Maximum and minimum total global radiation and coincident dry bulb temperature
DB/MG	Maximum and minimum coincident dry bulb temperature and coincident total global radiation
WB/MDB	Maximum and minimum wet bulb temperature and coincident dry bulb temperature
Wind	Maximum and minimum wind speed

Parameter	Units
dry bulb temperature	°F
humidity ratio	lb <sub>w</sub> /lb <sub>a</sub>
total global radiation	btu/ft <sup>2</sup>
wet bulb temperature	°F
wind speed	mph

alb01x.dat	1	DB/MHR	71	31	54.3	3.3							
alb01x.dat	2	DB/MHR	71	31	52.5	2.8							
alb01x.dat	3	DB/MHR	71	31	50.6	2.5							
alb01x.dat	4	DB/MHR	71	31	49.4	2.6							
alb01x.dat	5	DB/MHR	71	31	48.3	2.7							
alb01x.dat	6	DB/MHR	71	31	47.6	2.6							
alb01x.dat	7	DB/MHR	71	31	46.5	2.5							
alb01x.dat	1	DB/MHR	71	5	-2.4	0.6							
alb01x.dat	2	DB/MHR	71	6	-2.2	0.5							
alb01x.dat	3	DB/MHR	71	7	-2.3	0.5							
alb01x.dat	4	DB/MHR	71	8	0.2	0.6							
alb01x.dat	5	DB/MHR	71	8	1.8	0.7							
alb01x.dat	6	DB/MHR	71	9	4.8	0.9							
alb01x.dat	7	DB/MHR	71	9	7.1	1.1							
alb01x.dat	1	HR/MDB	65	7	6.6	50.8							
alb01x.dat	2	HR/MDB	80	14	6	46.5							
alb01x.dat	3	HR/MDB	80	15	5.8	45.8							
alb01x.dat	4	HR/MDB	80	15	5.7	44.3							
alb01x.dat	5	HR/MDB	80	15	5.5	43							
alb01x.dat	6	HR/MDB	80	16	5.4	42.9							
alb01x.dat	7	HR/MDB	80	18	5.3	43.4							
alb01x.dat	1	HR/MDB	63	13	0.3	4.8							
alb01x.dat	2	HR/MDB	63	13	0.4	5.7							
alb01x.dat	3	HR/MDB	63	14	0.5	8.2							
alb01x.dat	4	HR/MDB	63	15	0.6	11.5							
alb01x.dat	5	HR/MDB	64	16	0.7	18.9							
alb01x.dat	6	HR/MDB	64	17	0.7	21.1							
alb01x.dat	7	HR/MDB	64	18	0.7	23.3							
alb01x.dat	1	G/MDB	69	30	1421.4	25.1	0.8	0	0	0	0	0	0
alb01x.dat	2	G/MDB	69	31	1408.7	27.3	0.8	0.78	0	0	0	0	0
alb01x.dat	3	G/MDB	69	31	1398.8	30.1	0.79	0.8	0.78	0	0	0	0
alb01x.dat	4	G/MDB	71	29	1382.3	45.1	0.8	0.79	0.8	0.81	0	0	0
alb01x.dat	5	G/MDB	71	29	1376.4	44.1	0.8	0.8	0.79	0.8	0.81	0	0
alb01x.dat	6	G/MDB	71	29	1374.4	42.8	0.81	0.8	0.8	0.79	0.8	0.81	0
alb01x.dat	7	G/MDB	71	29	1355.9	42.2	0.74	0.81	0.8	0.8	0.79	0.8	0.81
alb01x.dat	1	G/MDB	80	7	112.2	40.6	0.07	0	0	0	0	0	0
alb01x.dat	2	G/MDB	80	7	299.1	38.6	0.32	0.07	0	0	0	0	0
alb01x.dat	3	G/MDB	79	17	388	41.7	0.19	0.29	0.25	0	0	0	0
alb01x.dat	4	G/MDB	80	12	401.8	39.7	0.28	0.35	0.14	0.27	0	0	0
alb01x.dat	5	G/MDB	80	11	426.9	40	0.07	0.54	0.28	0.35	0.14	0	0
alb01x.dat	6	G/MDB	80	12	424.7	40	0.07	0.54	0.28	0.35	0.14	0.27	0
alb01x.dat	7	G/MDB	80	12	433.4	39.5	0.32	0.07	0.54	0.28	0.35	0.14	0.27



alb03x.dat	1	DB/MHR	71	27	70	4							
alb03x.dat	2	DB/MHR	71	27	67.6	3.3							
alb03x.dat	3	DB/MHR	71	28	66.2	3							
alb03x.dat	4	DB/MHR	71	28	64.3	2.6							
alb03x.dat	5	DB/MHR	71	28	64	2.4							
alb03x.dat	6	DB/MHR	71	28	63.5	2.2							
alb03x.dat	7	DB/MHR	71	28	62.4	2							
alb03x.dat	1	DB/MHR	65	3	20.9	1.2							
alb03x.dat	2	DB/MHR	66	4	22.6	0.9							
alb03x.dat	3	DB/MHR	65	4	24.2	1.2							
alb03x.dat	4	DB/MHR	65	4	26.2	1.3							
alb03x.dat	5	DB/MHR	65	5	28.2	1.3							
alb03x.dat	6	DB/MHR	62	15	29.3	1.7							
alb03x.dat	7	DB/MHR	69	11	29.6	2.2							
alb03x.dat	1	HR/MDB	78	1	7.2	47.6							
alb03x.dat	2	HR/MDB	78	2	6.6	47.6							
alb03x.dat	3	HR/MDB	85	12	6.4	51.9							
alb03x.dat	4	HR/MDB	85	12	5.8	52.3							
alb03x.dat	5	HR/MDB	78	5	5.4	44.3							
alb03x.dat	6	HR/MDB	78	6	5.2	44.4							
alb03x.dat	7	HR/MDB	78	7	5.1	44.8							
alb03x.dat	1	HR/MDB	76	22	0.7	45.7							
alb03x.dat	2	HR/MDB	66	5	0.7	24.8							
alb03x.dat	3	HR/MDB	76	22	0.8	42.9							
alb03x.dat	4	HR/MDB	66	6	0.9	28.3							
alb03x.dat	5	HR/MDB	71	22	0.9	46.9							
alb03x.dat	6	HR/MDB	71	22	1	48							
alb03x.dat	7	HR/MDB	71	23	1	49.9							
alb03x.dat	1	G/MDB	72	30	2404.1	41.3	0.84	0	0	0	0	0	0
alb03x.dat	2	G/MDB	72	31	2400.3	42.4	0.84	0.83	0	0	0	0	0
alb03x.dat	3	G/MDB	69	30	2337.1	56	0.82	0.81	0.82	0	0	0	0
alb03x.dat	4	G/MDB	69	30	2327.2	54.4	0.81	0.82	0.81	0.82	0	0	0
alb03x.dat	5	G/MDB	69	30	2319.2	52.6	0.82	0.81	0.82	0.81	0.82	0	0
alb03x.dat	6	G/MDB	69	30	2315.5	50.6	0.83	0.82	0.81	0.82	0.81	0.82	0
alb03x.dat	7	G/MDB	69	31	2286	52.4	0.83	0.82	0.81	0.82	0.81	0.82	0.73
alb03x.dat	1	G/MDB	78	1	430.8	47.6	0.19	0	0	0	0	0	0
alb03x.dat	2	G/MDB	82	13	578	48.4	0.26	0.2	0	0	0	0	0
alb03x.dat	3	G/MDB	82	13	728.3	49.8	0.41	0.26	0.2	0	0	0	0
alb03x.dat	4	G/MDB	85	12	873.2	52.3	0.42	0.38	0.33	0.28	0	0	0
alb03x.dat	5	G/MDB	85	12	880.8	52.1	0.37	0.42	0.38	0.33	0.28	0	0
alb03x.dat	6	G/MDB	85	12	867.9	51.9	0.33	0.37	0.42	0.38	0.33	0.28	0
alb03x.dat	7	G/MDB	85	12	861.9	51.9	0.34	0.33	0.37	0.42	0.38	0.33	0.28



alb07x.dat	1	DB/MHR	63	24	87.6	7.1							
alb07x.dat	2	DB/MHR	78	17	87.2	7.7							
alb07x.dat	3	DB/MHR	63	24	86.5	7.6							
alb07x.dat	4	DB/MHR	63	25	86	7.9							
alb07x.dat	5	DB/MHR	63	26	85.8	7.9							
alb07x.dat	6	DB/MHR	63	26	85.5	8							
alb07x.dat	7	DB/MHR	63	27	85	7.8							
alb07x.dat	1	DB/MHR	64	12	62	11.9							
alb07x.dat	2	DB/MHR	64	13	64.1	11							
alb07x.dat	3	DB/MHR	64	13	65.6	11.4							
alb07x.dat	4	DB/MHR	68	6	66.5	11							
alb07x.dat	5	DB/MHR	68	6	67.6	10.6							
alb07x.dat	6	DB/MHR	89	28	68.2	11.5							
alb07x.dat	7	DB/MHR	89	28	68.8	11.3							
alb07x.dat	1	HR/MDB	73	17	14.3	69.4							
alb07x.dat	2	HR/MDB	73	18	14.2	68.7							
alb07x.dat	3	HR/MDB	73	18	13.9	69.4							
alb07x.dat	4	HR/MDB	73	18	13.5	69.9							
alb07x.dat	5	HR/MDB	73	19	13.1	70.7							
alb07x.dat	6	HR/MDB	73	19	12.9	71.2							
alb07x.dat	7	HR/MDB	70	25	12.5	74.6							
alb07x.dat	1	HR/MDB	87	3	1.9	78.4							
alb07x.dat	2	HR/MDB	87	4	2	78.9							
alb07x.dat	3	HR/MDB	87	5	2	78.5							
alb07x.dat	4	HR/MDB	87	6	2	78.4							
alb07x.dat	5	HR/MDB	87	7	2.1	78.5							
alb07x.dat	6	HR/MDB	87	7	2.3	78.7							
alb07x.dat	7	HR/MDB	87	8	2.6	79.1							
alb07x.dat	1	G/MDB	87	5	2917	77.8	0.8	0	0	0	0	0	0
alb07x.dat	2	G/MDB	87	6	2908	77.9	0.8	0.8	0	0	0	0	0
alb07x.dat	3	G/MDB	87	6	2884.9	78.4	0.78	0.8	0.8	0	0	0	0
alb07x.dat	4	G/MDB	87	6	2884.7	78.4	0.79	0.78	0.8	0.8	0	0	0
alb07x.dat	5	G/MDB	87	6	2885.1	78.6	0.79	0.79	0.78	0.8	0.8	0	0
alb07x.dat	6	G/MDB	87	7	2838.5	78.7	0.79	0.79	0.78	0.8	0.8	0.72	0
alb07x.dat	7	G/MDB	87	8	2830.9	79.1	0.79	0.79	0.78	0.8	0.8	0.72	0.77
alb07x.dat	1	G/MDB	88	24	140.1	78.6	0.04	0	0	0	0	0	0
alb07x.dat	2	G/MDB	85	29	862.4	67.2	0.27	0.22	0	0	0	0	0
alb07x.dat	3	G/MDB	85	30	1159.7	68	0.27	0.22	0.5	0	0	0	0
alb07x.dat	4	G/MDB	85	31	1406.2	68.9	0.27	0.22	0.5	0.62	0	0	0
alb07x.dat	5	G/MDB	88	27	1599.8	79.5	0.63	0.04	0.71	0.34	0.55	0	0
alb07x.dat	6	G/MDB	83	30	1674.2	75.6	0.49	0.57	0.35	0.7	0.29	0.48	0
alb07x.dat	7	G/MDB	83	31	1758.3	75.6	0.49	0.57	0.35	0.7	0.29	0.48	0.65



alb10x.dat	1	DB/MHR	79	1	71.8	4							
alb10x.dat	2	DB/MHR	79	2	71.4	4.2							
alb10x.dat	3	DB/MHR	79	3	71	4.4							
alb10x.dat	4	DB/MHR	78	4	69.5	6.3							
alb10x.dat	5	DB/MHR	79	5	69.2	4.4							
alb10x.dat	6	DB/MHR	79	6	68.9	4.1							
alb10x.dat	7	DB/MHR	79	7	68.9	3.9							
alb10x.dat	1	DB/MHR	71	30	34.4	2.1							
alb10x.dat	2	DB/MHR	76	28	36.2	3.1							
alb10x.dat	3	DB/MHR	76	29	37.1	3.3							
alb10x.dat	4	DB/MHR	76	30	38.9	3.3							
alb10x.dat	5	DB/MHR	76	30	40.5	3.4							
alb10x.dat	6	DB/MHR	84	24	40.6	5.1							
alb10x.dat	7	DB/MHR	84	25	40.7	5.1							
alb10x.dat	1	HR/MDB	77	6	11.4	64							
alb10x.dat	2	HR/MDB	72	13	10.6	65.4							
alb10x.dat	3	HR/MDB	77	6	10.4	65.5							
alb10x.dat	4	HR/MDB	72	15	9.9	63.7							
alb10x.dat	5	HR/MDB	72	16	9.8	64.1							
alb10x.dat	6	HR/MDB	72	17	9.5	63.6							
alb10x.dat	7	HR/MDB	72	18	9.4	62.8							
alb10x.dat	1	HR/MDB	89	31	1.3	41.9							
alb10x.dat	2	HR/MDB	89	31	1.4	41.5							
alb10x.dat	3	HR/MDB	89	31	1.4	41.9							
alb10x.dat	4	HR/MDB	89	31	1.6	44.1							
alb10x.dat	5	HR/MDB	89	31	1.7	45							
alb10x.dat	6	HR/MDB	89	31	1.9	46.4							
alb10x.dat	7	HR/MDB	67	28	2.1	55.2							
alb10x.dat	1	G/MDB	63	1	2035.8	68.7	0.82	0	0	0	0	0	0
alb10x.dat	2	G/MDB	63	2	1986.3	69.5	0.82	0.79	0	0	0	0	0
alb10x.dat	3	G/MDB	63	3	1964.2	69.3	0.82	0.79	0.79	0	0	0	0
alb10x.dat	4	G/MDB	61	4	1939.4	56.6	0.79	0.8	0.79	0.78	0	0	0
alb10x.dat	5	G/MDB	63	5	1949	67.5	0.82	0.79	0.79	0.76	0.83	0	0
alb10x.dat	6	G/MDB	63	6	1944.7	66.9	0.82	0.79	0.79	0.76	0.83	0.81	0
alb10x.dat	7	G/MDB	63	7	1934.5	66.8	0.82	0.79	0.79	0.76	0.83	0.81	0.79
alb10x.dat	1	G/MDB	78	21	263.4	55.6	0.13	0	0	0	0	0	0
alb10x.dat	2	G/MDB	83	20	469.2	52	0.22	0.22	0	0	0	0	0
alb10x.dat	3	G/MDB	80	28	604.9	41.2	0.34	0.32	0.25	0	0	0	0
alb10x.dat	4	G/MDB	78	24	665.9	50.7	0.13	0.64	0.17	0.35	0	0	0
alb10x.dat	5	G/MDB	78	25	701.3	50.4	0.13	0.64	0.17	0.35	0.42	0	0
alb10x.dat	6	G/MDB	78	26	833.4	49.9	0.13	0.64	0.17	0.35	0.42	0.75	0
alb10x.dat	7	G/MDB	84	26	885.1	41.2	0.3	0.5	0.59	0.36	0.26	0.6	0.4



atl01x.dat	1	DB/MHR	82	20	66.1	12.2							
atl01x.dat	2	DB/MHR	82	21	64.7	12.1							
atl01x.dat	3	DB/MHR	75	31	63	9.3							
atl01x.dat	4	DB/MHR	75	31	62.2	9.2							
atl01x.dat	5	DB/MHR	74	28	61.5	10.6							
atl01x.dat	6	DB/MHR	74	28	60.7	10.4							
atl01x.dat	7	DB/MHR	74	28	60.1	9.9							
atl01x.dat	1	DB/MHR	85	21	4.9	0.5							
atl01x.dat	2	DB/MHR	85	21	8.6	0.7							
atl01x.dat	3	DB/MHR	82	12	12.6	1							
atl01x.dat	4	DB/MHR	70	10	16.3	1							
atl01x.dat	5	DB/MHR	82	14	17.8	1.7							
atl01x.dat	6	DB/MHR	82	15	19.1	1.9							
atl01x.dat	7	DB/MHR	82	15	20.8	1.9							
atl01x.dat	1	HR/MDB	72	13	12.3	64.3							
atl01x.dat	2	HR/MDB	82	21	12.1	64.7							
atl01x.dat	3	HR/MDB	74	26	11	62							
atl01x.dat	4	HR/MDB	74	26	10.6	60.6							
atl01x.dat	5	HR/MDB	74	28	10.6	61.5							
atl01x.dat	6	HR/MDB	74	28	10.4	60.7							
atl01x.dat	7	HR/MDB	74	29	10.2	59.8							
atl01x.dat	1	HR/MDB	77	17	0.4	12.5							
atl01x.dat	2	HR/MDB	82	11	0.6	9.6							
atl01x.dat	3	HR/MDB	77	19	0.7	14.7							
atl01x.dat	4	HR/MDB	77	19	0.9	17.1							
atl01x.dat	5	HR/MDB	77	21	1	19.6							
atl01x.dat	6	HR/MDB	77	22	1	21.2							
atl01x.dat	7	HR/MDB	77	23	1.1	22.7							
atl01x.dat	1	G/MDB	77	31	1396.4	27.3	0.75	0	0	0	0	0	0
atl01x.dat	2	G/MDB	70	31	1356.6	37	0.72	0.75	0	0	0	0	0
atl01x.dat	3	G/MDB	76	30	1334.3	39.8	0.74	0.71	0.75	0	0	0	0
atl01x.dat	4	G/MDB	88	29	1313.6	36.1	0.74	0.73	0.74	0.71	0	0	0
atl01x.dat	5	G/MDB	88	29	1243.1	37.1	0.54	0.74	0.73	0.74	0.71	0	0
atl01x.dat	6	G/MDB	68	21	1190.3	42.7	0.74	0.67	0.73	0.71	0.68	0.69	0
atl01x.dat	7	G/MDB	88	29	1191.6	38.3	0.72	0.5	0.54	0.74	0.73	0.74	0.71
atl01x.dat	1	G/MDB	81	22	171.8	39.8	0.1	0	0	0	0	0	0
atl01x.dat	2	G/MDB	81	22	186.7	40.5	0.12	0.1	0	0	0	0	0
atl01x.dat	3	G/MDB	81	22	184.5	41.3	0.11	0.12	0.1	0	0	0	0
atl01x.dat	4	G/MDB	68	4	383.3	39.9	0.24	0.21	0.24	0.29	0	0	0
atl01x.dat	5	G/MDB	68	6	394.6	37.2	0.21	0.24	0.29	0.28	0.23	0	0
atl01x.dat	6	G/MDB	68	6	391.8	37.1	0.24	0.21	0.24	0.29	0.28	0.23	0
atl01x.dat	7	G/MDB	68	7	475.7	36.2	0.24	0.21	0.24	0.29	0.28	0.23	0.61



atl03x.dat	1	DB/MHR	74	10	72.5	8.8							
atl03x.dat	2	DB/MHR	89	29	72	10.8							
atl03x.dat	3	DB/MHR	82	20	71.2	10.9							
atl03x.dat	4	DB/MHR	89	30	70	10.2							
atl03x.dat	5	DB/MHR	90	15	69.9	9.6							
atl03x.dat	6	DB/MHR	90	15	69	9.7							
atl03x.dat	7	DB/MHR	90	16	68.2	10							
atl03x.dat	1	DB/MHR	80	2	20.9	1.9							
atl03x.dat	2	DB/MHR	80	3	25.2	1.7							
atl03x.dat	3	DB/MHR	80	3	28.5	2.4							
atl03x.dat	4	DB/MHR	80	4	32.4	2.6							
atl03x.dat	5	DB/MHR	65	8	34.5	3.5							
atl03x.dat	6	DB/MHR	65	9	36.1	3.4							
atl03x.dat	7	DB/MHR	65	10	36.8	3.3							
atl03x.dat	1	HR/MDB	77	29	12.6	65.3							
atl03x.dat	2	HR/MDB	77	30	12.5	65.1							
atl03x.dat	3	HR/MDB	73	16	11.5	68.5							
atl03x.dat	4	HR/MDB	82	20	10.9	68.9							
atl03x.dat	5	HR/MDB	82	21	10.7	68.1							
atl03x.dat	6	HR/MDB	73	11	10.5	61.5							
atl03x.dat	7	HR/MDB	73	11	10.3	61.5							
atl03x.dat	1	HR/MDB	65	21	1.1	34.1							
atl03x.dat	2	HR/MDB	65	21	1.5	33.8							
atl03x.dat	3	HR/MDB	75	4	1.6	31.3							
atl03x.dat	4	HR/MDB	75	5	1.8	33.9							
atl03x.dat	5	HR/MDB	69	14	1.9	36.1							
atl03x.dat	6	HR/MDB	69	15	2	38.1							
atl03x.dat	7	HR/MDB	69	16	2.2	39.6							
atl03x.dat	1	G/MDB	71	30	2250.7	48	0.77	0	0	0	0	0	0
atl03x.dat	2	G/MDB	86	31	2236.8	67.9	0.76	0.77	0	0	0	0	0
atl03x.dat	3	G/MDB	86	31	2234.4	66.5	0.77	0.76	0.77	0	0	0	0
atl03x.dat	4	G/MDB	86	31	2221.1	65	0.76	0.77	0.76	0.77	0	0	0
atl03x.dat	5	G/MDB	86	31	2187.6	64.2	0.72	0.76	0.77	0.76	0.77	0	0
atl03x.dat	6	G/MDB	86	31	2113	63.9	0.61	0.72	0.76	0.77	0.76	0.77	0
atl03x.dat	7	G/MDB	86	31	2114.9	63.4	0.75	0.61	0.72	0.76	0.77	0.76	0.77
atl03x.dat	1	G/MDB	81	4	352.2	50.1	0.15	0	0	0	0	0	0
atl03x.dat	2	G/MDB	78	9	546.2	40.3	0.21	0.22	0	0	0	0	0
atl03x.dat	3	G/MDB	78	9	611.3	42.5	0.3	0.21	0.22	0	0	0	0
atl03x.dat	4	G/MDB	89	5	681.1	49.8	0.32	0.34	0.24	0.23	0	0	0
atl03x.dat	5	G/MDB	89	5	685.5	49.1	0.3	0.32	0.34	0.24	0.23	0	0
atl03x.dat	6	G/MDB	89	6	717.5	49	0.3	0.32	0.34	0.24	0.23	0.36	0
atl03x.dat	7	G/MDB	89	7	741.2	47.8	0.3	0.32	0.34	0.24	0.23	0.36	0.36



atl07x.dat	1	DB/MHR	80	13	91.7	17.7							
atl07x.dat	2	DB/MHR	80	13	91.4	18.7							
atl07x.dat	3	DB/MHR	80	13	91	19.1							
atl07x.dat	4	DB/MHR	80	13	90.4	19.2							
atl07x.dat	5	DB/MHR	80	14	89.8	19.2							
atl07x.dat	6	DB/MHR	80	16	89.7	19.2							
atl07x.dat	7	DB/MHR	80	16	89.6	19.2							
atl07x.dat	1	DB/MHR	67	15	65	8.8							
atl07x.dat	2	DB/MHR	67	15	66.2	9.7							
atl07x.dat	3	DB/MHR	67	16	66.8	9.7							
atl07x.dat	4	DB/MHR	67	17	67.7	9.9							
atl07x.dat	5	DB/MHR	67	17	68.4	11							
atl07x.dat	6	DB/MHR	67	18	68.9	10.9							
atl07x.dat	7	DB/MHR	67	19	69.7	10.9							
atl07x.dat	1	HR/MDB	80	12	19.8	91.1							
atl07x.dat	2	HR/MDB	80	12	19.8	90.6							
atl07x.dat	3	HR/MDB	80	12	19.6	89.9							
atl07x.dat	4	HR/MDB	80	12	19.6	89.4							
atl07x.dat	5	HR/MDB	80	14	19.2	89.8							
atl07x.dat	6	HR/MDB	80	14	19.3	89.5							
atl07x.dat	7	HR/MDB	80	15	19.3	89.2							
atl07x.dat	1	HR/MDB	67	15	8.8	65							
atl07x.dat	2	HR/MDB	67	16	9.3	66.4							
atl07x.dat	3	HR/MDB	67	17	9.6	67.8							
atl07x.dat	4	HR/MDB	67	18	9.8	68.8							
atl07x.dat	5	HR/MDB	67	18	10	68.5							
atl07x.dat	6	HR/MDB	67	19	10.2	69.5							
atl07x.dat	7	HR/MDB	67	20	10.7	70							
atl07x.dat	1	G/MDB	80	1	2841.9	79.3	0.78	0	0	0	0	0	0
atl07x.dat	2	G/MDB	80	8	2734.4	84	0.77	0.74	0	0	0	0	0
atl07x.dat	3	G/MDB	80	3	2619.1	82.2	0.78	0.71	0.67	0	0	0	0
atl07x.dat	4	G/MDB	80	4	2549.8	83.2	0.78	0.71	0.67	0.64	0	0	0
atl07x.dat	5	G/MDB	80	5	2532.7	83.9	0.78	0.71	0.67	0.64	0.68	0	0
atl07x.dat	6	G/MDB	90	10	2469.1	84.2	0.68	0.69	0.67	0.66	0.67	0.72	0
atl07x.dat	7	G/MDB	80	13	2490.9	88.2	0.77	0.74	0.58	0.62	0.68	0.69	0.75
atl07x.dat	1	G/MDB	62	6	715.8	72.4	0.2	0	0	0	0	0	0
atl07x.dat	2	G/MDB	79	9	806	66.6	0.22	0.23	0	0	0	0	0
atl07x.dat	3	G/MDB	84	31	842.5	68.6	0.26	0.21	0.26	0	0	0	0
atl07x.dat	4	G/MDB	84	31	900.6	69.3	0.31	0.26	0.21	0.26	0	0	0
atl07x.dat	5	G/MDB	84	31	1031	70.3	0.44	0.31	0.26	0.21	0.26	0	0
atl07x.dat	6	G/MDB	79	11	1080.2	69.8	0.33	0.34	0.22	0.23	0.34	0.33	0
atl07x.dat	7	G/MDB	85	29	1160.1	75.1	0.37	0.26	0.38	0.29	0.31	0.23	0.47



atl10x.dat	1	DB/MHR	86	3	79	14.8							
atl10x.dat	2	DB/MHR	86	3	78.6	15.3							
atl10x.dat	3	DB/MHR	86	3	78.3	15.5							
atl10x.dat	4	DB/MHR	86	4	78.1	15.4							
atl10x.dat	5	DB/MHR	86	5	77.7	15.2							
atl10x.dat	6	DB/MHR	86	6	75.9	14							
atl10x.dat	7	DB/MHR	86	7	74.3	13.2							
atl10x.dat	1	DB/MHR	89	20	40.2	3.1							
atl10x.dat	2	DB/MHR	89	20	41.8	4							
atl10x.dat	3	DB/MHR	62	26	43.7	2.2							
atl10x.dat	4	DB/MHR	62	27	44.5	2.2							
atl10x.dat	5	DB/MHR	76	31	46.2	4.3							
atl10x.dat	6	DB/MHR	76	31	46.9	4.5							
atl10x.dat	7	DB/MHR	76	31	48.5	5.3							
atl10x.dat	1	HR/MDB	80	18	16.4	72.5							
atl10x.dat	2	HR/MDB	86	2	15.8	77.9							
atl10x.dat	3	HR/MDB	86	3	15.5	78.3							
atl10x.dat	4	HR/MDB	86	4	15.4	78.1							
atl10x.dat	5	HR/MDB	86	5	15.2	77.7							
atl10x.dat	6	HR/MDB	82	11	14.4	70.9							
atl10x.dat	7	HR/MDB	82	13	14.2	68.8							
atl10x.dat	1	HR/MDB	62	26	1.9	42.1							
atl10x.dat	2	HR/MDB	62	27	2	44.3							
atl10x.dat	3	HR/MDB	62	27	2.2	44.5							
atl10x.dat	4	HR/MDB	62	27	2.2	44.5							
atl10x.dat	5	HR/MDB	62	28	2.5	46.3							
atl10x.dat	6	HR/MDB	62	29	2.8	48.2							
atl10x.dat	7	HR/MDB	62	29	3.1	49.3							
atl10x.dat	1	G/MDB	67	1	1920.4	61	0.76	0	0	0	0	0	0
atl10x.dat	2	G/MDB	87	4	1878.4	54.7	0.75	0.75	0	0	0	0	0
atl10x.dat	3	G/MDB	87	3	1877.7	61	0.76	0.73	0.75	0	0	0	0
atl10x.dat	4	G/MDB	87	4	1875.7	59.5	0.76	0.73	0.75	0.75	0	0	0
atl10x.dat	5	G/MDB	87	5	1867.4	59.9	0.76	0.73	0.75	0.75	0.75	0	0
atl10x.dat	6	G/MDB	74	7	1822.6	57.4	0.71	0.73	0.75	0.73	0.74	0.75	0
atl10x.dat	7	G/MDB	74	7	1811.5	57.8	0.69	0.71	0.73	0.75	0.73	0.74	0.75
atl10x.dat	1	G/MDB	80	30	237.8	50.6	0.12	0	0	0	0	0	0
atl10x.dat	2	G/MDB	80	30	312.1	52.4	0.19	0.12	0	0	0	0	0
atl10x.dat	3	G/MDB	80	30	298	54.3	0.13	0.19	0.12	0	0	0	0
atl10x.dat	4	G/MDB	80	30	518.9	55.4	0.58	0.13	0.19	0.12	0	0	0
atl10x.dat	5	G/MDB	85	31	540.5	57.5	0.22	0.29	0.33	0.22	0.27	0	0
atl10x.dat	6	G/MDB	85	31	594	58.6	0.42	0.22	0.29	0.33	0.22	0.27	0
atl10x.dat	7	G/MDB	82	13	657.1	68.8	0.21	0.19	0.41	0.35	0.31	0.2	0.27



bal01x.dat	1	DB/MHR	75	11	60.9	9.1							
bal01x.dat	2	DB/MHR	67	25	59.7	6.9							
bal01x.dat	3	DB/MHR	67	26	58.4	6.7							
bal01x.dat	4	DB/MHR	67	26	56.8	6.5							
bal01x.dat	5	DB/MHR	67	27	55	6.4							
bal01x.dat	6	DB/MHR	67	27	52.9	6.1							
bal01x.dat	7	DB/MHR	67	28	50.4	5.5							
bal01x.dat	1	DB/MHR	82	17	-1.5	0.2							
bal01x.dat	2	DB/MHR	82	18	5	0.5							
bal01x.dat	3	DB/MHR	82	19	9.6	0.8							
bal01x.dat	4	DB/MHR	61	28	12.4	0.8							
bal01x.dat	5	DB/MHR	61	28	13.3	0.8							
bal01x.dat	6	DB/MHR	61	26	13.5	0.9							
bal01x.dat	7	DB/MHR	61	28	13.5	0.9							
bal01x.dat	1	HR/MDB	75	11	9.1	60.9							
bal01x.dat	2	HR/MDB	79	2	7.5	51.3							
bal01x.dat	3	HR/MDB	72	13	7.2	52							
bal01x.dat	4	HR/MDB	72	13	6.9	51.1							
bal01x.dat	5	HR/MDB	67	27	6.4	55							
bal01x.dat	6	HR/MDB	67	27	6.1	52.9							
bal01x.dat	7	HR/MDB	67	27	5.7	50.2							
bal01x.dat	1	HR/MDB	82	17	0.2	-1.5							
bal01x.dat	2	HR/MDB	82	11	0.4	8.5							
bal01x.dat	3	HR/MDB	82	12	0.5	11.5							
bal01x.dat	4	HR/MDB	85	23	0.7	14.7							
bal01x.dat	5	HR/MDB	61	29	0.8	13.9							
bal01x.dat	6	HR/MDB	61	30	0.8	14.9							
bal01x.dat	7	HR/MDB	61	30	0.8	15.2							
bal01x.dat	1	G/MDB	87	28	1154.2	17.1	0.76	0	0	0	0	0	0
bal01x.dat	2	G/MDB	87	29	1130.7	22.6	0.76	0.72	0	0	0	0	0
bal01x.dat	3	G/MDB	87	29	1103.3	20.3	0.7	0.76	0.72	0	0	0	0
bal01x.dat	4	G/MDB	87	29	1025.1	20.6	0.53	0.7	0.76	0.72	0	0	0
bal01x.dat	5	G/MDB	87	30	964.7	23.1	0.53	0.7	0.76	0.72	0.47	0	0
bal01x.dat	6	G/MDB	87	29	958.5	18.3	0.72	0.4	0.53	0.7	0.76	0.72	0
bal01x.dat	7	G/MDB	87	29	953	18.9	0.63	0.72	0.4	0.53	0.7	0.76	0.72
bal01x.dat	1	G/MDB	83	5	192.7	35.9	0.15	0	0	0	0	0	0
bal01x.dat	2	G/MDB	79	2	281.7	51.3	0.24	0.21	0	0	0	0	0
bal01x.dat	3	G/MDB	85	4	314.4	38.5	0.26	0.23	0.25	0	0	0	0
bal01x.dat	4	G/MDB	85	4	317.4	41.8	0.26	0.26	0.23	0.25	0	0	0
bal01x.dat	5	G/MDB	84	6	346.6	34.9	0.29	0.33	0.24	0.26	0.24	0	0
bal01x.dat	6	G/MDB	69	23	347.1	41	0.17	0.29	0.29	0.21	0.3	0.2	0
bal01x.dat	7	G/MDB	69	24	356.2	41.5	0.17	0.29	0.29	0.21	0.3	0.2	0.28

bal01x.dat	1	DB/MG	75	11	60.9	529.1	0.4	0	0	0	0	0
bal01x.dat	2	DB/MG	67	25	59.7	887.1	0.64	0.57	0	0	0	0
bal01x.dat	3	DB/MG	67	26	58.4	879	0.64	0.57	0.58	0	0	0
bal01x.dat	4	DB/MG	67	26	56.8	869.5	0.58	0.64	0.57	0.58	0	0
bal01x.dat	5	DB/MG	67	27	55	768.2	0.58	0.64	0.57	0.58	0.24	0
bal01x.dat	6	DB/MG	67	27	52.9	779.4	0.58	0.58	0.64	0.57	0.58	0.24
bal01x.dat	7	DB/MG	67	28	50.4	740.6	0.58	0.58	0.64	0.57	0.58	0.24
bal01x.dat	8	DB/MG	67	28	48.9	740.6	0.58	0.58	0.64	0.57	0.58	0.33
bal01x.dat	9	DB/MG	67	28	47.4	740.6	0.58	0.58	0.64	0.57	0.58	0.33
bal01x.dat	10	DB/MG	67	28	46.0	740.6	0.58	0.58	0.64	0.57	0.58	0.33
bal01x.dat	11	DB/MG	67	28	44.7	740.6	0.58	0.58	0.64	0.57	0.58	0.33
bal01x.dat	12	DB/MG	67	28	43.5	740.6	0.58	0.58	0.64	0.57	0.58	0.33
bal01x.dat	13	DB/MG	67	28	42.4	740.6	0.58	0.58	0.64	0.57	0.58	0.33
bal01x.dat	14	DB/MG	67	28	41.4	740.6	0.58	0.58	0.64	0.57	0.58	0.33
bal01x.dat	15	DB/MG	67	28	40.5	740.6	0.58	0.58	0.64	0.57	0.58	0.33
bal01x.dat	16	DB/MG	67	28	39.7	740.6	0.58	0.58	0.64	0.57	0.58	0.33
bal01x.dat	17	DB/MG	67	28	39.0	740.6	0.58	0.58	0.64	0.57	0.58	0.33
bal01x.dat	18	DB/MG	67	28	38.4	740.6	0.58	0.58	0.64	0.57	0.58	0.33
bal01x.dat	19	DB/MG	67	28	37.9	740.6	0.58	0.58	0.64	0.57	0.58	0.33
bal01x.dat	20	DB/MG	67	28	37.4	740.6	0.58	0.58	0.64	0.57	0.58	0.33
bal01x.dat	21	WB/MDB	75	11	56.8	60.9						
bal01x.dat	22	WB/MDB	67	25	52.7	59.7						
bal01x.dat	23	WB/MDB	67	26	51.7	58.4						
bal01x.dat	24	WB/MDB	67	26	50.3	56.8						
bal01x.dat	25	WB/MDB	67	27	49.4	55						
bal01x.dat	26	WB/MDB	67	27	47.8	52.9						
bal01x.dat	27	WB/MDB	67	27	45.4	50.2						
bal01x.dat	28	WB/MDB	67	27	44.2	50.2						
bal01x.dat	29	WB/MDB	67	27	43.1	50.2						
bal01x.dat	30	WB/MDB	67	27	42.1	50.2						
bal01x.dat	31	WB/MDB	67	27	41.2	50.2						
bal01x.dat	32	WB/MDB	67	27	40.4	50.2						
bal01x.dat	33	WB/MDB	67	27	39.7	50.2						
bal01x.dat	34	WB/MDB	67	27	39.0	50.2						
bal01x.dat	35	WB/MDB	67	27	38.4	50.2						
bal01x.dat	36	WB/MDB	67	27	37.9	50.2						
bal01x.dat	37	WB/MDB	67	27	37.4	50.2						
bal01x.dat	38	WB/MDB	67	27	37.0	50.2						
bal01x.dat	39	WB/MDB	67	27	36.6	50.2						
bal01x.dat	40	WB/MDB	67	27	36.2	50.2						
bal01x.dat	41	WB/MDB	67	27	35.9	50.2						
bal01x.dat	42	WB/MDB	67	27	35.6	50.2						
bal01x.dat	43	WB/MDB	67	27	35.3	50.2						
bal01x.dat	44	WB/MDB	67	27	35.0	50.2						
bal01x.dat	45	WB/MDB	67	27	34.7	50.2						
bal01x.dat	46	WB/MDB	67	27	34.4	50.2						
bal01x.dat	47	WB/MDB	67	27	34.1	50.2						
bal01x.dat	48	WB/MDB	67	27	33.8	50.2						
bal01x.dat	49	WB/MDB	67	27	33.5	50.2						
bal01x.dat	50	WB/MDB	67	27	33.2	50.2						
bal01x.dat	51	WB/MDB	67	27	33.0	50.2						
bal01x.dat	52	WB/MDB	67	27	32.8	50.2						
bal01x.dat	53	WB/MDB	67	27	32.6	50.2						
bal01x.dat	54	WB/MDB	67	27	32.4	50.2						
bal01x.dat	55	WB/MDB	67	27	32.2	50.2						
bal01x.dat	56	WB/MDB	67	27	32.0	50.2						
bal01x.dat	57	WB/MDB	67	27	31.8	50.2						
bal01x.dat	58	WB/MDB	67	27	31.6	50.2						
bal01x.dat	59	WB/MDB	67	27	31.4	50.2						
bal01x.dat	60	WB/MDB	67	27	31.2	50.2						
bal01x.dat	61	WB/MDB	67	27	31.0	50.2						
bal01x.dat	62	WB/MDB	67	27	30.8	50.2						
bal01x.dat	63	WB/MDB	67	27	30.6	50.2						
bal01x.dat	64	WB/MDB	67	27	30.4	50.2						
bal01x.dat	65	WB/MDB	67	27	30.2	50.2						
bal01x.dat	66	WB/MDB	67	27	30.0	50.2						
bal01x.dat	67	WB/MDB	67	27	29.8	50.2						
bal01x.dat	68	WB/MDB	67	27	29.6	50.2						
bal01x.dat	69	WB/MDB	67	27	29.4	50.2						
bal01x.dat	70	WB/MDB	67	27	29.2	50.2						
bal01x.dat	71	WB/MDB	67	27	29.0	50.2						
bal01x.dat	72	WB/MDB	67	27	28.8	50.2						
bal01x.dat	73	WB/MDB	67	27	28.6	50.2						
bal01x.dat	74	WB/MDB	67	27	28.4	50.2						
bal01x.dat	75	WB/MDB	67	27	28.2	50.2						
bal01x.dat	76	WB/MDB	67	27	28.0	50.2						
bal01x.dat	77	WB/MDB	67	27	27.8	50.2						
bal01x.dat	78	WB/MDB	67	27	27.6	50.2						
bal01x.dat	79	WB/MDB	67	27	27.4	50.2						
bal01x.dat	80	WB/MDB	67	27	27.2	50.2						
bal01x.dat	81	WB/MDB	67	27	27.0	50.2						
bal01x.dat	82	WB/MDB	67	27	26.8	50.2						
bal01x.dat	83	WB/MDB	67	27	26.6	50.2						
bal01x.dat	84	WB/MDB	67	27	26.4	50.2						
bal01x.dat	85	WB/MDB	67	27	26.2	50.2						
bal01x.dat	86	WB/MDB	67	27	26.0	50.2						
bal01x.dat	87	WB/MDB	67	27	25.8	50.2						
bal01x.dat	88	WB/MDB	67	27	25.6	50.2						
bal01x.dat	89	WB/MDB	67	27	25.4	50.2						
bal01x.dat	90	WB/MDB	67	27	25.2	50.2						
bal01x.dat	91	WB/MDB	67	27	25.0	50.2						
bal01x.dat	92	WB/MDB	67	27	24.8	50.2						
bal01x.dat	93	WB/MDB	67	27	24.6	50.2						
bal01x.dat	94	WB/MDB	67	27	24.4	50.2						
bal01x.dat	95	WB/MDB	67	27	24.2	50.2						
bal01x.dat	96	WB/MDB	67	27	24.0	50.2						
bal01x.dat	97	WB/MDB	67	27	23.8	50.2						
bal01x.dat	98	WB/MDB	67	27	23.6	50.2						
bal01x.dat	99	WB/MDB	67	27	23.4	50.2						
bal01x.dat	100	WB/MDB	67	27	23.2	50.2						
bal01x.dat	101	WB/MDB	67	27	23.0	50.2						
bal01x.dat	102	WB/MDB	67	27	22.8	50.2						
bal01x.dat	103	WB/MDB	67	27	22.6	50.2						
bal01x.dat	104	WB/MDB	67	27	22.4	50.2						
bal01x.dat	105	WB/MDB	67	27	22.2	50.2						
bal01x.dat	106	WB/MDB	67	27	22.0	50.2						
bal01x.dat	107	WB/MDB	67	27	21.8	50.2						
bal01x.dat	108	WB/MDB	67	27	21.6	50.2						
bal01x.dat	109	WB/MDB	67	27	21.4	50.2						
bal01x.dat	110	WB/MDB	67	27	21.2	50.2						
bal01x.dat	111	WB/MDB	67	27	21.0	50.2						
bal01x.dat	112	WB/MDB	67	27	20.8	50.2						
bal01x.dat	113	WB/MDB	67	27	20.6	50.2						
bal01x.dat	114	WB/MDB	67	27	20.4	50.2						
bal01x.dat	115	WB/MDB	67	27	20.2	50.2						
bal01x.dat	116	WB/MDB	67	27	20.0	50.2						
bal01x.dat	117	WB/MDB	67	27	19.8	50.2						
bal01x.dat	118	WB/MDB	67	27	19.6	50.2						
bal01x.dat	119	WB/MDB	67	27	19.4	50.2						
bal01x.dat	120	WB/MDB	67	27	19.2	50.2						
bal01x.dat	121	WB/MDB	67	27	19.0	50.2						
bal01x.dat	122	WB/MDB	67	27	18.8	50.2						
bal01x.dat	123	WB/MDB	67	27	18.6	50.2						
bal01x.dat	124	WB/MDB	67	27	18.4	50.2						
bal01x.dat	125	WB/MDB	67	27	18.2	50.2						
bal01x.dat	126	WB/MDB	67	27	18.0	50.2						
bal01x.dat	127	WB/MDB	67	27	17.8	50.2						
bal01x.dat	128	WB/MDB	67	27	17.6	50.2						
bal01x.dat	129	WB/MDB	67	27	17.4	50.2						
bal01x.dat	130	WB/MDB	67	27	17.2	50.2						
bal01x.dat	131	WB/MDB	67	27	17.0	50.2						
bal01x.dat	132	WB/MDB	67	27	16.8	50.2						
bal01x.dat	133	WB/MDB	67	27	16.6	50.2						
bal01x.dat	134	WB/MDB	67	27	16.4	50.2						
bal01x.dat	135	WB/MDB	67	27	16.2	50.2						

bal03x.dat	1	DB/MHR	89	28	73.8	9.3							
bal03x.dat	2	DB/MHR	89	29	72.6	10.4							
bal03x.dat	3	DB/MHR	90	14	69.3	8.6							
bal03x.dat	4	DB/MHR	90	15	68.6	8.7							
bal03x.dat	5	DB/MHR	90	16	68.3	9.2							
bal03x.dat	6	DB/MHR	90	17	67.3	9.5							
bal03x.dat	7	DB/MHR	90	18	65.4	8.7							
bal03x.dat	1	DB/MHR	80	1	14.7	0.8							
bal03x.dat	2	DB/MHR	80	2	16.5	0.9							
bal03x.dat	3	DB/MHR	80	3	19.4	0.9							
bal03x.dat	4	DB/MHR	80	4	23.2	1							
bal03x.dat	5	DB/MHR	84	12	26.2	1.6							
bal03x.dat	6	DB/MHR	84	13	27.1	1.8							
bal03x.dat	7	DB/MHR	78	8	28.4	1.5							
bal03x.dat	1	HR/MDB	89	29	11.4	71.4							
bal03x.dat	2	HR/MDB	90	17	11	64.6							
bal03x.dat	3	HR/MDB	90	17	10.3	65.2							
bal03x.dat	4	HR/MDB	90	17	9.9	65.9							
bal03x.dat	5	HR/MDB	90	17	9.7	67.2							
bal03x.dat	6	HR/MDB	90	17	9.5	67.3							
bal03x.dat	7	HR/MDB	90	17	9.2	65.4							
bal03x.dat	1	HR/MDB	86	8	0.7	21.7							
bal03x.dat	2	HR/MDB	80	2	0.9	16.5							
bal03x.dat	3	HR/MDB	80	3	0.9	19.4							
bal03x.dat	4	HR/MDB	80	4	1	23.2							
bal03x.dat	5	HR/MDB	62	5	1.4	28.1							
bal03x.dat	6	HR/MDB	78	7	1.4	28.3							
bal03x.dat	7	HR/MDB	78	8	1.5	28.4							
bal03x.dat	1	G/MDB	82	28	2053.2	32.2	0.76	0	0	0	0	0	0
bal03x.dat	2	G/MDB	82	29	2024.4	36.8	0.76	0.73	0	0	0	0	0
bal03x.dat	3	G/MDB	82	29	1976.5	35.5	0.7	0.76	0.73	0	0	0	0
bal03x.dat	4	G/MDB	86	31	1944.7	57.5	0.71	0.71	0.71	0.71	0	0	0
bal03x.dat	5	G/MDB	86	26	1907.7	46.2	0.72	0.73	0.72	0.74	0.73	0	0
bal03x.dat	6	G/MDB	86	26	1889	42.9	0.7	0.72	0.73	0.72	0.74	0.73	0
bal03x.dat	7	G/MDB	86	31	1830.4	56.1	0.74	0.73	0.42	0.71	0.71	0.71	0.71
bal03x.dat	1	G/MDB	84	5	372.5	38	0.17	0	0	0	0	0	0
bal03x.dat	2	G/MDB	82	7	475.2	34.7	0.23	0.19	0	0	0	0	0
bal03x.dat	3	G/MDB	67	6	503.2	39.1	0.24	0.24	0.21	0	0	0	0
bal03x.dat	4	G/MDB	67	7	540.4	38.5	0.24	0.24	0.21	0.29	0	0	0
bal03x.dat	5	G/MDB	83	10	587.9	45.7	0.3	0.29	0.23	0.24	0.23	0	0
bal03x.dat	6	G/MDB	83	11	602.5	45.4	0.3	0.29	0.23	0.24	0.23	0.29	0
bal03x.dat	7	G/MDB	83	12	613.1	44.9	0.3	0.29	0.23	0.24	0.23	0.29	0.29



bal07x.dat	1	DB/MHR	78	23	88.5	16.8							
bal07x.dat	2	DB/MHR	78	23	87.6	17.3							
bal07x.dat	3	DB/MHR	88	17	86.9	17							
bal07x.dat	4	DB/MHR	88	17	86.2	16.8							
bal07x.dat	5	DB/MHR	88	18	85.7	16.9							
bal07x.dat	6	DB/MHR	87	25	85.4	17.2							
bal07x.dat	7	DB/MHR	87	26	85.2	17.2							
bal07x.dat	1	DB/MHR	72	5	62	9.7							
bal07x.dat	2	DB/MHR	72	6	63.2	9.7							
bal07x.dat	3	DB/MHR	79	6	64.2	8.3							
bal07x.dat	4	DB/MHR	72	8	64.8	10							
bal07x.dat	5	DB/MHR	72	9	65.8	10.5							
bal07x.dat	6	DB/MHR	72	9	66.8	10.6							
bal07x.dat	7	DB/MHR	79	7	67.7	9.5							
bal07x.dat	1	HR/MDB	65	25	19.4	85.3							
bal07x.dat	2	HR/MDB	65	25	19.1	84.4							
bal07x.dat	3	HR/MDB	72	21	18.4	84.4							
bal07x.dat	4	HR/MDB	72	21	18.3	83.4							
bal07x.dat	5	HR/MDB	72	23	18.2	85.1							
bal07x.dat	6	HR/MDB	72	23	18.1	84.3							
bal07x.dat	7	HR/MDB	87	13	18	81.1							
bal07x.dat	1	HR/MDB	66	21	5.4	70.4							
bal07x.dat	2	HR/MDB	66	22	6.6	71.6							
bal07x.dat	3	HR/MDB	66	22	7.1	72.8							
bal07x.dat	4	HR/MDB	66	23	7.5	73							
bal07x.dat	5	HR/MDB	66	24	7.9	73.2							
bal07x.dat	6	HR/MDB	66	25	8.4	73.9							
bal07x.dat	7	HR/MDB	63	10	8.6	71.3							
bal07x.dat	1	G/MDB	80	7	2673.3	70.1	0.73	0	0	0	0	0	0
bal07x.dat	2	G/MDB	71	5	2633.6	71.3	0.72	0.72	0	0	0	0	0
bal07x.dat	3	G/MDB	71	5	2610.4	71.4	0.7	0.72	0.72	0	0	0	0
bal07x.dat	4	G/MDB	63	6	2539.3	72	0.66	0.72	0.72	0.68	0	0	0
bal07x.dat	5	G/MDB	63	7	2494.1	72.6	0.66	0.72	0.72	0.68	0.63	0	0
bal07x.dat	6	G/MDB	63	6	2475.9	75.3	0.67	0.61	0.66	0.72	0.72	0.68	0
bal07x.dat	7	G/MDB	63	7	2452.7	75.3	0.67	0.61	0.66	0.72	0.72	0.68	0.63
bal07x.dat	1	G/MDB	75	13	684.1	71.1	0.19	0	0	0	0	0	0
bal07x.dat	2	G/MDB	78	3	774.6	64.8	0.21	0.21	0	0	0	0	0
bal07x.dat	3	G/MDB	75	15	897.1	73.6	0.19	0.29	0.26	0	0	0	0
bal07x.dat	4	G/MDB	75	15	992.9	73.7	0.35	0.19	0.29	0.26	0	0	0
bal07x.dat	5	G/MDB	75	17	1023.6	74.8	0.19	0.29	0.26	0.37	0.31	0	0
bal07x.dat	6	G/MDB	75	17	1066.4	74.6	0.35	0.19	0.29	0.26	0.37	0.31	0
bal07x.dat	7	G/MDB	75	17	1152.3	74.3	0.46	0.35	0.19	0.29	0.26	0.37	0.31



bal10x.dat	1	DB/MHR	86	1	77.5	14.6							
bal10x.dat	2	DB/MHR	86	2	77	13.8							
bal10x.dat	3	DB/MHR	86	3	75.3	13.8							
bal10x.dat	4	DB/MHR	86	4	75.6	14.3							
bal10x.dat	5	DB/MHR	86	5	74.5	13.4							
bal10x.dat	6	DB/MHR	90	13	72.8	14.2							
bal10x.dat	7	DB/MHR	90	14	72.5	13.8							
bal10x.dat	1	DB/MHR	76	28	36.2	2.5							
bal10x.dat	2	DB/MHR	76	28	36.8	2.4							
bal10x.dat	3	DB/MHR	62	27	38.2	2.5							
bal10x.dat	4	DB/MHR	62	27	39.7	2.6							
bal10x.dat	5	DB/MHR	76	30	41.7	3.5							
bal10x.dat	6	DB/MHR	76	31	43.8	4.1							
bal10x.dat	7	DB/MHR	76	28	44.5	4.4							
bal10x.dat	1	HR/MDB	90	13	15.9	73.1							
bal10x.dat	2	HR/MDB	90	13	15.6	72.4							
bal10x.dat	3	HR/MDB	90	13	15.2	72.4							
bal10x.dat	4	HR/MDB	90	13	14.7	72.5							
bal10x.dat	5	HR/MDB	90	13	14.5	73.1							
bal10x.dat	6	HR/MDB	90	13	14.2	72.8							
bal10x.dat	7	HR/MDB	90	14	13.8	72.5							
bal10x.dat	1	HR/MDB	65	29	1.6	36.3							
bal10x.dat	2	HR/MDB	69	24	1.9	39.5							
bal10x.dat	3	HR/MDB	69	25	2.3	40.9							
bal10x.dat	4	HR/MDB	74	22	2.5	41.7							
bal10x.dat	5	HR/MDB	62	28	2.9	42.9							
bal10x.dat	6	HR/MDB	65	30	3	44							
bal10x.dat	7	HR/MDB	65	31	3	45.6							
bal10x.dat	1	G/MDB	87	2	1702	58.7	0.74	0	0	0	0	0	0
bal10x.dat	2	G/MDB	74	5	1658.9	51.7	0.74	0.74	0	0	0	0	0
bal10x.dat	3	G/MDB	65	4	1635.3	55.7	0.72	0.69	0.74	0	0	0	0
bal10x.dat	4	G/MDB	65	5	1614.4	52.9	0.72	0.69	0.74	0.69	0	0	0
bal10x.dat	5	G/MDB	65	6	1585.3	52.2	0.72	0.69	0.74	0.69	0.66	0	0
bal10x.dat	6	G/MDB	63	7	1509.5	59.6	0.72	0.54	0.66	0.72	0.7	0.7	0
bal10x.dat	7	G/MDB	63	7	1511	59.4	0.65	0.72	0.54	0.66	0.72	0.7	0.7
bal10x.dat	1	G/MDB	83	23	303.1	55.7	0.16	0	0	0	0	0	0
bal10x.dat	2	G/MDB	62	31	343.9	47.3	0.2	0.2	0	0	0	0	0
bal10x.dat	3	G/MDB	89	19	399.4	58.2	0.21	0.19	0.21	0	0	0	0
bal10x.dat	4	G/MDB	89	20	447.6	56.1	0.21	0.19	0.21	0.31	0	0	0
bal10x.dat	5	G/MDB	85	24	557.6	58.6	0.33	0.21	0.3	0.39	0.25	0	0
bal10x.dat	6	G/MDB	83	25	545.1	52.5	0.2	0.4	0.47	0.16	0.3	0.21	0
bal10x.dat	7	G/MDB	83	25	535	52.8	0.24	0.2	0.4	0.47	0.16	0.3	0.21



cha01x.dat	1	DB/MHR	74	27	69.7	11.3							
cha01x.dat	2	DB/MHR	74	28	69.2	11.6							
cha01x.dat	3	DB/MHR	74	28	68.4	11.7							
cha01x.dat	4	DB/MHR	74	28	68.3	11.5							
cha01x.dat	5	DB/MHR	74	28	67.9	11.4							
cha01x.dat	6	DB/MHR	74	29	67.5	11.5							
cha01x.dat	7	DB/MHR	74	30	67.1	11.4							
cha01x.dat	1	DB/MHR	85	21	16.2	0.6							
cha01x.dat	2	DB/MHR	85	22	21.6	0.9							
cha01x.dat	3	DB/MHR	70	10	22.7	0.9							
cha01x.dat	4	DB/MHR	70	11	24.8	1.2							
cha01x.dat	5	DB/MHR	70	11	27.3	1.6							
cha01x.dat	6	DB/MHR	77	22	28.4	1.4							
cha01x.dat	7	DB/MHR	77	23	28.7	1.4							
cha01x.dat	1	HR/MDB	72	13	13	67.3							
cha01x.dat	2	HR/MDB	72	13	12.6	65.2							
cha01x.dat	3	HR/MDB	72	13	12.6	65.2							
cha01x.dat	4	HR/MDB	72	13	12.4	65.6							
cha01x.dat	5	HR/MDB	72	14	12.1	64.7							
cha01x.dat	6	HR/MDB	74	30	11.5	67.2							
cha01x.dat	7	HR/MDB	74	30	11.4	67.1							
cha01x.dat	1	HR/MDB	85	21	0.6	16.2							
cha01x.dat	2	HR/MDB	82	11	0.8	25.4							
cha01x.dat	3	HR/MDB	70	10	0.9	22.7							
cha01x.dat	4	HR/MDB	77	20	1.2	26.2							
cha01x.dat	5	HR/MDB	77	21	1.3	27.5							
cha01x.dat	6	HR/MDB	77	22	1.4	28.4							
cha01x.dat	7	HR/MDB	77	23	1.4	28.7							
cha01x.dat	1	G/MDB	66	30	1476	19.5	0.79	0	0	0	0	0	0
cha01x.dat	2	G/MDB	66	31	1469.8	24.3	0.79	0.77	0	0	0	0	0
cha01x.dat	3	G/MDB	78	30	1356.9	32.9	0.71	0.74	0.74	0	0	0	0
cha01x.dat	4	G/MDB	88	29	1341.6	36.8	0.73	0.73	0.74	0.72	0	0	0
cha01x.dat	5	G/MDB	88	30	1299	39.7	0.73	0.73	0.74	0.72	0.6	0	0
cha01x.dat	6	G/MDB	82	29	1255	40.6	0.7	0.7	0.7	0.75	0.59	0.68	0
cha01x.dat	7	G/MDB	67	31	1187.8	51.8	0.55	0.63	0.57	0.76	0.67	0.65	0.66
cha01x.dat	1	G/MDB	71	6	281.8	52.2	0.17	0	0	0	0	0	0
cha01x.dat	2	G/MDB	83	2	316.7	47.4	0.19	0.2	0	0	0	0	0
cha01x.dat	3	G/MDB	64	9	359.2	59.4	0.22	0.24	0.2	0	0	0	0
cha01x.dat	4	G/MDB	73	4	414.4	56.9	0.3	0.23	0.2	0.3	0	0	0
cha01x.dat	5	G/MDB	84	14	434.5	43.4	0.21	0.19	0.35	0.25	0.29	0	0
cha01x.dat	6	G/MDB	84	15	453.5	43.1	0.21	0.19	0.35	0.25	0.29	0.32	0
cha01x.dat	7	G/MDB	84	16	458.6	43	0.21	0.19	0.35	0.25	0.29	0.32	0.29



cha03x.dat	1	DB/MHR	74	10	74.8	9							
cha03x.dat	2	DB/MHR	74	10	73.2	9.3							
cha03x.dat	3	DB/MHR	85	31	72.6	10.1							
cha03x.dat	4	DB/MHR	85	31	71.7	9.6							
cha03x.dat	5	DB/MHR	90	17	71.2	12							
cha03x.dat	6	DB/MHR	90	17	71	11.8							
cha03x.dat	7	DB/MHR	90	17	70.5	11.5							
cha03x.dat	1	DB/MHR	80	2	23	2.1							
cha03x.dat	2	DB/MHR	80	3	25.8	1.8							
cha03x.dat	3	DB/MHR	80	3	29.7	2.4							
cha03x.dat	4	DB/MHR	80	4	32.6	2.5							
cha03x.dat	5	DB/MHR	80	5	36.6	3.5							
cha03x.dat	6	DB/MHR	80	6	39.5	4.1							
cha03x.dat	7	DB/MHR	62	8	40.9	3.3							
cha03x.dat	1	HR/MDB	89	30	13.8	71.3							
cha03x.dat	2	HR/MDB	89	6	13.2	69.1							
cha03x.dat	3	HR/MDB	90	17	13	72.2							
cha03x.dat	4	HR/MDB	90	17	12.5	71.4							
cha03x.dat	5	HR/MDB	87	30	12.3	67.4							
cha03x.dat	6	HR/MDB	73	16	12.2	69.8							
cha03x.dat	7	HR/MDB	73	16	12	68.4							
cha03x.dat	1	HR/MDB	67	18	1.5	39.6							
cha03x.dat	2	HR/MDB	80	3	1.8	25.8							
cha03x.dat	3	HR/MDB	69	13	2	41.4							
cha03x.dat	4	HR/MDB	69	14	2.1	42.4							
cha03x.dat	5	HR/MDB	69	14	2.3	42.7							
cha03x.dat	6	HR/MDB	68	6	2.4	46.9							
cha03x.dat	7	HR/MDB	68	7	2.6	46.8							
cha03x.dat	1	G/MDB	74	31	2291.6	66.6	0.78	0	0	0	0	0	0
cha03x.dat	2	G/MDB	66	31	2220.1	59.7	0.74	0.76	0	0	0	0	0
cha03x.dat	3	G/MDB	78	31	2177.5	60.1	0.75	0.75	0.73	0	0	0	0
cha03x.dat	4	G/MDB	66	31	2180.6	53.6	0.76	0.71	0.74	0.76	0	0	0
cha03x.dat	5	G/MDB	66	31	2184.5	53.5	0.76	0.76	0.71	0.74	0.76	0	0
cha03x.dat	6	G/MDB	66	31	2017.5	53.3	0.41	0.76	0.76	0.71	0.74	0.76	0
cha03x.dat	7	G/MDB	66	31	2049.2	52.6	0.79	0.41	0.76	0.76	0.71	0.74	0.76
cha03x.dat	1	G/MDB	74	25	478.7	44.8	0.17	0	0	0	0	0	0
cha03x.dat	2	G/MDB	62	2	526.5	43.9	0.23	0.2	0	0	0	0	0
cha03x.dat	3	G/MDB	73	10	620.6	59.4	0.21	0.25	0.27	0	0	0	0
cha03x.dat	4	G/MDB	73	9	640.1	59.9	0.23	0.32	0.21	0.25	0	0	0
cha03x.dat	5	G/MDB	73	10	649.3	59.9	0.23	0.32	0.21	0.25	0.27	0	0
cha03x.dat	6	G/MDB	73	11	704.2	60.7	0.23	0.32	0.21	0.25	0.27	0.38	0
cha03x.dat	7	G/MDB	73	11	783.5	61.7	0.51	0.23	0.32	0.21	0.25	0.27	0.38



cha07x.dat	1	DB/MHR	86	19	89.5	19.3							
cha07x.dat	2	DB/MHR	86	20	89.5	19							
cha07x.dat	3	DB/MHR	86	20	88.9	19.2							
cha07x.dat	4	DB/MHR	86	12	88.1	16.9							
cha07x.dat	5	DB/MHR	86	13	88	17							
cha07x.dat	6	DB/MHR	86	13	87.8	17.1							
cha07x.dat	7	DB/MHR	86	14	87.2	16.9							
cha07x.dat	1	DB/MHR	72	6	68.5	13.3							
cha07x.dat	2	DB/MHR	72	7	70.1	12.7							
cha07x.dat	3	DB/MHR	72	8	70.7	12.2							
cha07x.dat	4	DB/MHR	72	9	71.2	12							
cha07x.dat	5	DB/MHR	72	10	71.4	12.4							
cha07x.dat	6	DB/MHR	72	11	71.7	12.9							
cha07x.dat	7	DB/MHR	72	12	72.2	13.4							
cha07x.dat	1	HR/MDB	86	21	21.3	85.2							
cha07x.dat	2	HR/MDB	81	28	20.9	85.3							
cha07x.dat	3	HR/MDB	81	29	20.8	85.2							
cha07x.dat	4	HR/MDB	81	29	20.6	84.3							
cha07x.dat	5	HR/MDB	81	29	20.5	83.6							
cha07x.dat	6	HR/MDB	81	29	20.6	83.3							
cha07x.dat	7	HR/MDB	81	29	20.4	83.1							
cha07x.dat	1	HR/MDB	88	2	10.4	74.6							
cha07x.dat	2	HR/MDB	72	9	11.2	72.3							
cha07x.dat	3	HR/MDB	72	9	11.5	72.1							
cha07x.dat	4	HR/MDB	72	9	12	71.2							
cha07x.dat	5	HR/MDB	88	6	12.4	74.9							
cha07x.dat	6	HR/MDB	88	7	12.2	75.1							
cha07x.dat	7	HR/MDB	88	7	12.3	75.2							
cha07x.dat	1	G/MDB	87	20	2596.2	78.3	0.73	0	0	0	0	0	0
cha07x.dat	2	G/MDB	87	20	2571.7	77.3	0.71	0.73	0	0	0	0	0
cha07x.dat	3	G/MDB	87	20	2554.7	77.2	0.71	0.71	0.73	0	0	0	0
cha07x.dat	4	G/MDB	87	21	2545.9	78.1	0.71	0.71	0.73	0.71	0	0	0
cha07x.dat	5	G/MDB	87	21	2503.9	78.2	0.65	0.71	0.71	0.73	0.71	0	0
cha07x.dat	6	G/MDB	87	23	2451.8	80.4	0.71	0.71	0.73	0.71	0.61	0.67	0
cha07x.dat	7	G/MDB	87	23	2435.2	80.2	0.65	0.71	0.71	0.73	0.71	0.61	0.67
cha07x.dat	1	G/MDB	64	17	623.5	73.2	0.17	0	0	0	0	0	0
cha07x.dat	2	G/MDB	64	18	785.4	75.3	0.17	0.27	0	0	0	0	0
cha07x.dat	3	G/MDB	64	22	895.6	75	0.25	0.21	0.29	0	0	0	0
cha07x.dat	4	G/MDB	64	20	941.3	76.2	0.17	0.27	0.36	0.25	0	0	0
cha07x.dat	5	G/MDB	64	21	905.2	75.7	0.17	0.27	0.36	0.25	0.21	0	0
cha07x.dat	6	G/MDB	64	22	925.6	75.8	0.17	0.27	0.36	0.25	0.21	0.29	0
cha07x.dat	7	G/MDB	64	23	984.9	76.1	0.17	0.27	0.36	0.25	0.21	0.29	0.38



cha10x.dat	1	DB/MHR	86	5	82.3	15.2							
cha10x.dat	2	DB/MHR	86	5	82.2	16.2							
cha10x.dat	3	DB/MHR	86	5	82.2	16.9							
cha10x.dat	4	DB/MHR	86	5	82	17.1							
cha10x.dat	5	DB/MHR	86	5	81.7	17.1							
cha10x.dat	6	DB/MHR	86	6	80.5	16.1							
cha10x.dat	7	DB/MHR	86	7	78.6	15.4							
cha10x.dat	1	DB/MHR	76	28	42.3	2.8							
cha10x.dat	2	DB/MHR	76	29	43.5	3.2							
cha10x.dat	3	DB/MHR	76	29	46.3	3.7							
cha10x.dat	4	DB/MHR	62	28	47.9	3.9							
cha10x.dat	5	DB/MHR	62	28	48.6	3.9							
cha10x.dat	6	DB/MHR	62	29	50.1	4.5							
cha10x.dat	7	DB/MHR	62	30	51.7	5.1							
cha10x.dat	1	HR/MDB	90	10	18.6	77.6							
cha10x.dat	2	HR/MDB	64	4	18.2	77.8							
cha10x.dat	3	HR/MDB	64	4	18.2	77.2							
cha10x.dat	4	HR/MDB	64	4	18	77.4							
cha10x.dat	5	HR/MDB	86	5	17.1	81.7							
cha10x.dat	6	HR/MDB	90	12	16.7	76.9							
cha10x.dat	7	HR/MDB	90	13	16.5	76.5							
cha10x.dat	1	HR/MDB	76	28	2.8	42.3							
cha10x.dat	2	HR/MDB	62	27	3.2	45.3							
cha10x.dat	3	HR/MDB	62	27	3.5	47.1							
cha10x.dat	4	HR/MDB	62	27	3.7	48.1							
cha10x.dat	5	HR/MDB	62	28	3.9	48.6							
cha10x.dat	6	HR/MDB	62	29	4.5	50.1							
cha10x.dat	7	HR/MDB	68	31	4.9	52.7							
cha10x.dat	1	G/MDB	74	3	1930.8	50.2	0.76	0	0	0	0	0	0
cha10x.dat	2	G/MDB	74	4	1923.7	50.2	0.76	0.76	0	0	0	0	0
cha10x.dat	3	G/MDB	70	5	1905.3	66.3	0.74	0.76	0.77	0	0	0	0
cha10x.dat	4	G/MDB	74	4	1876.1	55.6	0.74	0.69	0.76	0.76	0	0	0
cha10x.dat	5	G/MDB	74	5	1863	56.2	0.74	0.69	0.76	0.76	0.73	0	0
cha10x.dat	6	G/MDB	87	6	1799.3	62.2	0.68	0.74	0.67	0.76	0.73	0.7	0
cha10x.dat	7	G/MDB	87	8	1799.2	61.3	0.74	0.67	0.76	0.73	0.7	0.71	0.75
cha10x.dat	1	G/MDB	63	25	350	69.3	0.16	0	0	0	0	0	0
cha10x.dat	2	G/MDB	71	21	440.2	70.4	0.22	0.18	0	0	0	0	0
cha10x.dat	3	G/MDB	71	22	459.2	71.1	0.22	0.18	0.23	0	0	0	0
cha10x.dat	4	G/MDB	71	22	499.3	68.9	0.28	0.22	0.18	0.23	0	0	0
cha10x.dat	5	G/MDB	85	31	560.8	65.3	0.27	0.27	0.31	0.25	0.27	0	0
cha10x.dat	6	G/MDB	65	22	645	66.9	0.32	0.28	0.28	0.27	0.32	0.28	0
cha10x.dat	7	G/MDB	70	31	717.6	65.2	0.39	0.33	0.44	0.35	0.32	0.22	0.36



chi01x.dat	1	DB/MHR	89	31	51.8	5.4							
chi01x.dat	2	DB/MHR	67	24	51.2	6.8							
chi01x.dat	3	DB/MHR	67	24	49.7	6.8							
chi01x.dat	4	DB/MHR	67	24	47.3	6							
chi01x.dat	5	DB/MHR	67	24	44.8	5.2							
chi01x.dat	6	DB/MHR	67	25	42.7	4.7							
chi01x.dat	7	DB/MHR	64	24	41.1	4.4							
chi01x.dat	1	DB/MHR	82	10	-17.1	0.2							
chi01x.dat	2	DB/MHR	82	10	-13.5	0.2							
chi01x.dat	3	DB/MHR	66	30	-8.9	0.2							
chi01x.dat	4	DB/MHR	66	30	-5.9	0.3							
chi01x.dat	5	DB/MHR	63	24	-3.7	0.4							
chi01x.dat	6	DB/MHR	63	25	-2.9	0.4							
chi01x.dat	7	DB/MHR	63	26	-2	0.5							
chi01x.dat	1	HR/MDB	67	24	7.5	51.4							
chi01x.dat	2	HR/MDB	65	8	7.1	47.8							
chi01x.dat	3	HR/MDB	67	24	6.8	49.7							
chi01x.dat	4	HR/MDB	67	24	6	47.3							
chi01x.dat	5	HR/MDB	67	25	5.3	44.2							
chi01x.dat	6	HR/MDB	67	26	4.8	41.5							
chi01x.dat	7	HR/MDB	65	8	4.6	38.6							
chi01x.dat	1	HR/MDB	66	29	0.2	-12.8							
chi01x.dat	2	HR/MDB	66	29	0.2	-10.4							
chi01x.dat	3	HR/MDB	66	30	0.2	-8.9							
chi01x.dat	4	HR/MDB	66	30	0.3	-5.9							
chi01x.dat	5	HR/MDB	84	21	0.4	-2.5							
chi01x.dat	6	HR/MDB	63	28	0.4	-2.5							
chi01x.dat	7	HR/MDB	63	29	0.4	-1							
chi01x.dat	1	G/MDB	78	31	1049.3	9.4	0.73	0	0	0	0	0	0
chi01x.dat	2	G/MDB	66	31	958	0.2	0.72	0.62	0	0	0	0	0
chi01x.dat	3	G/MDB	72	31	943.1	8.7	0.67	0.66	0.67	0	0	0	0
chi01x.dat	4	G/MDB	65	30	943.4	1	0.69	0.69	0.63	0.69	0	0	0
chi01x.dat	5	G/MDB	78	31	907.8	6.7	0.62	0.67	0.66	0.57	0.73	0	0
chi01x.dat	6	G/MDB	90	31	851.9	32.7	0.62	0.55	0.65	0.68	0.59	0.59	0
chi01x.dat	7	G/MDB	63	29	789.9	-1	0.7	0.72	0.37	0.47	0.72	0.63	0.48
chi01x.dat	1	G/MDB	90	9	206.7	38.1	0.18	0	0	0	0	0	0
chi01x.dat	2	G/MDB	90	10	274.2	35	0.18	0.29	0	0	0	0	0
chi01x.dat	3	G/MDB	89	7	291.2	35.4	0.28	0.28	0.2	0	0	0	0
chi01x.dat	4	G/MDB	89	8	302.3	29.6	0.28	0.28	0.2	0.29	0	0	0
chi01x.dat	5	G/MDB	63	9	347.6	32	0.29	0.35	0.34	0.28	0.24	0	0
chi01x.dat	6	G/MDB	63	10	348.6	32.4	0.29	0.35	0.34	0.28	0.24	0.3	0
chi01x.dat	7	G/MDB	63	10	353.1	32.1	0.34	0.29	0.35	0.34	0.28	0.24	0.3



chi03x.dat	1	DB/MHR	90	12	69.4	10.5							
chi03x.dat	2	DB/MHR	90	13	68.3	11.2							
chi03x.dat	3	DB/MHR	90	14	67.2	10.9							
chi03x.dat	4	DB/MHR	90	14	65.3	10.7							
chi03x.dat	5	DB/MHR	90	15	63.8	9.9							
chi03x.dat	6	DB/MHR	90	16	61.6	9.1							
chi03x.dat	7	DB/MHR	90	16	59.6	8.8							
chi03x.dat	1	DB/MHR	62	1	6.2	0.7							
chi03x.dat	2	DB/MHR	62	2	11.5	0.9							
chi03x.dat	3	DB/MHR	65	20	12.7	1							
chi03x.dat	4	DB/MHR	65	21	13.4	1							
chi03x.dat	5	DB/MHR	65	22	16.3	1.3							
chi03x.dat	6	DB/MHR	65	23	17.3	1.4							
chi03x.dat	7	DB/MHR	65	24	17.2	1.4							
chi03x.dat	1	HR/MDB	90	13	11.9	67.3							
chi03x.dat	2	HR/MDB	90	13	11.2	68.3							
chi03x.dat	3	HR/MDB	90	14	10.9	67.2							
chi03x.dat	4	HR/MDB	90	14	10.7	65.3							
chi03x.dat	5	HR/MDB	90	14	9.9	61.8							
chi03x.dat	6	HR/MDB	90	15	9.5	61.1							
chi03x.dat	7	HR/MDB	90	15	8.9	58.7							
chi03x.dat	1	HR/MDB	84	11	0.6	16.8							
chi03x.dat	2	HR/MDB	80	2	0.9	13.6							
chi03x.dat	3	HR/MDB	65	20	1	12.7							
chi03x.dat	4	HR/MDB	65	21	1	13.4							
chi03x.dat	5	HR/MDB	84	11	1.2	18.3							
chi03x.dat	6	HR/MDB	84	12	1.3	18.6							
chi03x.dat	7	HR/MDB	84	12	1.3	19							
chi03x.dat	1	G/MDB	88	30	1977.4	40	0.74	0	0	0	0	0	0
chi03x.dat	2	G/MDB	70	28	1894.7	28.4	0.71	0.74	0	0	0	0	0
chi03x.dat	3	G/MDB	68	30	1835.1	59.8	0.67	0.68	0.73	0	0	0	0
chi03x.dat	4	G/MDB	70	30	1786	29.3	0.71	0.74	0.64	0.62	0	0	0
chi03x.dat	5	G/MDB	86	31	1806.9	59.9	0.74	0.63	0.68	0.66	0.72	0	0
chi03x.dat	6	G/MDB	86	31	1724	58.1	0.51	0.74	0.63	0.68	0.66	0.72	0
chi03x.dat	7	G/MDB	86	31	1697.4	58.7	0.6	0.51	0.74	0.63	0.68	0.66	0.72
chi03x.dat	1	G/MDB	74	4	362.6	41.8	0.18	0	0	0	0	0	0
chi03x.dat	2	G/MDB	76	2	443.2	38.6	0.2	0.24	0	0	0	0	0
chi03x.dat	3	G/MDB	76	3	527.2	38.4	0.2	0.24	0.34	0	0	0	0
chi03x.dat	4	G/MDB	76	4	523.8	38.6	0.2	0.24	0.34	0.25	0	0	0
chi03x.dat	5	G/MDB	76	5	551.3	37.9	0.2	0.24	0.34	0.25	0.32	0	0
chi03x.dat	6	G/MDB	73	6	668.7	45.8	0.36	0.22	0.36	0.35	0.34	0.32	0
chi03x.dat	7	G/MDB	62	11	720.6	32.3	0.3	0.38	0.4	0.32	0.32	0.33	0.29



chi10x.dat	1	DB/MHR	71	1	79	12.8							
chi10x.dat	2	DB/MHR	71	2	78.3	12.3							
chi10x.dat	3	DB/MHR	71	3	74.8	12.3							
chi10x.dat	4	DB/MHR	68	16	72	11.8							
chi10x.dat	5	DB/MHR	68	17	71.1	11.4							
chi10x.dat	6	DB/MHR	62	15	69.7	11.3							
chi10x.dat	7	DB/MHR	73	13	68.7	11.7							
chi10x.dat	1	DB/MHR	81	23	29.9	2.2							
chi10x.dat	2	DB/MHR	62	26	30.5	1.9							
chi10x.dat	3	DB/MHR	62	26	31.8	2							
chi10x.dat	4	DB/MHR	62	26	33.7	2.3							
chi10x.dat	5	DB/MHR	80	29	35.6	2.8							
chi10x.dat	6	DB/MHR	88	30	36	2.6							
chi10x.dat	7	DB/MHR	88	30	35.9	2.7							
chi10x.dat	1	HR/MDB	73	9	13.4	71.4							
chi10x.dat	2	HR/MDB	73	10	13.1	72.3							
chi10x.dat	3	HR/MDB	73	10	12.9	70.3							
chi10x.dat	4	HR/MDB	73	11	12.6	71.2							
chi10x.dat	5	HR/MDB	73	12	12.4	70.5							
chi10x.dat	6	HR/MDB	73	12	12.1	69.5							
chi10x.dat	7	HR/MDB	73	13	11.7	68.7							
chi10x.dat	1	HR/MDB	88	29	1.7	32.2							
chi10x.dat	2	HR/MDB	62	26	1.9	30.5							
chi10x.dat	3	HR/MDB	62	26	2	31.8							
chi10x.dat	4	HR/MDB	88	31	2.3	35.3							
chi10x.dat	5	HR/MDB	88	31	2.7	37.5							
chi10x.dat	6	HR/MDB	88	30	2.6	36							
chi10x.dat	7	HR/MDB	88	31	2.7	36.6							
chi10x.dat	1	G/MDB	75	2	1609.1	45.5	0.74	0	0	0	0	0	0
chi10x.dat	2	G/MDB	75	3	1608.8	50	0.74	0.74	0	0	0	0	0
chi10x.dat	3	G/MDB	75	4	1574.5	52.8	0.74	0.74	0.7	0	0	0	0
chi10x.dat	4	G/MDB	75	5	1488.8	54.7	0.74	0.74	0.7	0.58	0	0	0
chi10x.dat	5	G/MDB	75	6	1481.2	55.5	0.74	0.74	0.7	0.58	0.69	0	0
chi10x.dat	6	G/MDB	75	7	1488.9	56.2	0.74	0.74	0.7	0.58	0.69	0.74	0
chi10x.dat	7	G/MDB	75	7	1417.4	55.3	0.45	0.74	0.74	0.7	0.58	0.69	0.74
chi10x.dat	1	G/MDB	73	31	286.6	46.6	0.18	0	0	0	0	0	0
chi10x.dat	2	G/MDB	86	25	345.7	54.2	0.2	0.2	0	0	0	0	0
chi10x.dat	3	G/MDB	90	10	417.3	46.6	0.21	0.2	0.21	0	0	0	0
chi10x.dat	4	G/MDB	90	10	420.6	48.2	0.21	0.21	0.2	0.21	0	0	0
chi10x.dat	5	G/MDB	83	23	431.2	51.7	0.23	0.17	0.33	0.23	0.26	0	0
chi10x.dat	6	G/MDB	83	24	434.3	51.3	0.23	0.17	0.33	0.23	0.26	0.26	0
chi10x.dat	7	G/MDB	83	25	523.5	50.7	0.23	0.17	0.33	0.23	0.26	0.26	0.63



hou01x.dat	1	DB/MHR	75	28	73.6	14.2							
hou01x.dat	2	DB/MHR	75	29	73.2	14.1							
hou01x.dat	3	DB/MHR	75	29	72.8	13.6							
hou01x.dat	4	DB/MHR	75	31	72.6	14.3							
hou01x.dat	5	DB/MHR	75	31	72.5	14							
hou01x.dat	6	DB/MHR	75	31	71.3	13.1							
hou01x.dat	7	DB/MHR	75	31	69.4	12.2							
hou01x.dat	1	DB/MHR	62	10	21.4	0.9							
hou01x.dat	2	DB/MHR	62	11	22.6	1							
hou01x.dat	3	DB/MHR	62	12	24.7	1.2							
hou01x.dat	4	DB/MHR	62	12	28.3	2							
hou01x.dat	5	DB/MHR	78	21	29.3	2.9							
hou01x.dat	6	DB/MHR	78	22	29.9	3.1							
hou01x.dat	7	DB/MHR	78	23	31.3	3.4							
hou01x.dat	1	HR/MDB	75	31	15	72.9							
hou01x.dat	2	HR/MDB	90	18	14.6	70.8							
hou01x.dat	3	HR/MDB	75	31	14.3	72.3							
hou01x.dat	4	HR/MDB	75	31	14.3	72.6							
hou01x.dat	5	HR/MDB	75	31	14	72.5							
hou01x.dat	6	HR/MDB	75	31	13.1	71.3							
hou01x.dat	7	HR/MDB	75	31	12.2	69.4							
hou01x.dat	1	HR/MDB	62	10	0.9	21.4							
hou01x.dat	2	HR/MDB	62	11	1	22.6							
hou01x.dat	3	HR/MDB	62	12	1.2	24.7							
hou01x.dat	4	HR/MDB	63	15	1.7	32.9							
hou01x.dat	5	HR/MDB	63	16	2	35.2							
hou01x.dat	6	HR/MDB	88	26	2.6	45							
hou01x.dat	7	HR/MDB	88	27	2.7	45.6							
hou01x.dat	1	G/MDB	61	30	1497.8	40.4	0.74	0	0	0	0	0	0
hou01x.dat	2	G/MDB	88	27	1466.4	47.6	0.74	0.74	0	0	0	0	0
hou01x.dat	3	G/MDB	76	29	1457.7	43.6	0.74	0.72	0.73	0	0	0	0
hou01x.dat	4	G/MDB	76	30	1451.7	46.1	0.74	0.72	0.73	0.71	0	0	0
hou01x.dat	5	G/MDB	65	30	1403.5	53.2	0.72	0.7	0.7	0.72	0.67	0	0
hou01x.dat	6	G/MDB	65	31	1385.1	52.2	0.72	0.7	0.7	0.72	0.67	0.63	0
hou01x.dat	7	G/MDB	88	27	1373.9	45.6	0.73	0.73	0.59	0.67	0.73	0.74	0.74
hou01x.dat	1	G/MDB	73	1	337.3	45.3	0.19	0	0	0	0	0	0
hou01x.dat	2	G/MDB	73	6	367.2	51	0.22	0.19	0	0	0	0	0
hou01x.dat	3	G/MDB	73	7	383.5	47.1	0.22	0.19	0.23	0	0	0	0
hou01x.dat	4	G/MDB	90	6	431.2	54.6	0.2	0.33	0.23	0.21	0	0	0
hou01x.dat	5	G/MDB	73	9	458.1	41.8	0.22	0.19	0.23	0.33	0.3	0	0
hou01x.dat	6	G/MDB	90	6	461.2	52.3	0.26	0.33	0.2	0.33	0.23	0.21	0
hou01x.dat	7	G/MDB	73	10	486.6	41.8	0.34	0.22	0.19	0.23	0.33	0.3	0.28



hou03x.dat	1	DB/MHR	82	19	76.9	14.5							
hou03x.dat	2	DB/MHR	82	20	76.8	14.5							
hou03x.dat	3	DB/MHR	82	20	76.4	14.7							
hou03x.dat	4	DB/MHR	82	20	76.1	14.8							
hou03x.dat	5	DB/MHR	82	20	75.9	14.8							
hou03x.dat	6	DB/MHR	82	20	75.5	14.9							
hou03x.dat	7	DB/MHR	82	20	75.2	14.9							
hou03x.dat	1	DB/MHR	89	5	31.2	2.2							
hou03x.dat	2	DB/MHR	89	6	33.3	2.2							
hou03x.dat	3	DB/MHR	89	7	35.4	2.5							
hou03x.dat	4	DB/MHR	89	8	37.3	2.8							
hou03x.dat	5	DB/MHR	89	9	40	3.1							
hou03x.dat	6	DB/MHR	89	9	42.1	4.2							
hou03x.dat	7	DB/MHR	89	10	44.3	4.4							
hou03x.dat	1	HR/MDB	61	29	16.4	74.9							
hou03x.dat	2	HR/MDB	61	29	16.2	74.4							
hou03x.dat	3	HR/MDB	61	29	16.2	74.6							
hou03x.dat	4	HR/MDB	61	29	15.9	73.9							
hou03x.dat	5	HR/MDB	61	7	15.5	72.2							
hou03x.dat	6	HR/MDB	82	18	15	74.4							
hou03x.dat	7	HR/MDB	82	19	14.9	74.7							
hou03x.dat	1	HR/MDB	66	5	1.6	50.3							
hou03x.dat	2	HR/MDB	66	6	1.8	49.4							
hou03x.dat	3	HR/MDB	66	6	1.9	51.6							
hou03x.dat	4	HR/MDB	66	7	2.3	51.2							
hou03x.dat	5	HR/MDB	65	7	2.7	47							
hou03x.dat	6	HR/MDB	65	7	2.8	46.5							
hou03x.dat	7	HR/MDB	65	8	3	47.3							
hou03x.dat	1	G/MDB	87	31	2324.2	49.6	0.77	0	0	0	0	0	0
hou03x.dat	2	G/MDB	74	30	2236	71.4	0.74	0.75	0	0	0	0	0
hou03x.dat	3	G/MDB	74	31	2195.8	72.7	0.74	0.75	0.7	0	0	0	0
hou03x.dat	4	G/MDB	79	26	2082.7	57.6	0.68	0.72	0.73	0.72	0	0	0
hou03x.dat	5	G/MDB	61	24	2056.2	62.2	0.75	0.7	0.71	0.73	0.67	0	0
hou03x.dat	6	G/MDB	69	29	1938.1	58.9	0.74	0.69	0.65	0.72	0.61	0.53	0
hou03x.dat	7	G/MDB	69	30	1888.4	60	0.74	0.69	0.65	0.72	0.61	0.53	0.53
hou03x.dat	1	G/MDB	79	2	505.3	63.3	0.2	0	0	0	0	0	0
hou03x.dat	2	G/MDB	80	27	650.8	59.1	0.24	0.2	0	0	0	0	0
hou03x.dat	3	G/MDB	85	16	679.5	57.5	0.24	0.24	0.26	0	0	0	0
hou03x.dat	4	G/MDB	76	7	777.6	61	0.32	0.31	0.3	0.27	0	0	0
hou03x.dat	5	G/MDB	76	8	796.1	61.3	0.32	0.31	0.3	0.27	0.33	0	0
hou03x.dat	6	G/MDB	76	8	812	63.1	0.35	0.32	0.31	0.3	0.27	0.33	0
hou03x.dat	7	G/MDB	74	15	856.5	68	0.29	0.33	0.39	0.35	0.31	0.29	0.25



hou07x.dat	1	DB/MHR	80	17	90.4	16.2							
hou07x.dat	2	DB/MHR	80	17	90	16.1							
hou07x.dat	3	DB/MHR	80	17	90.1	16.6							
hou07x.dat	4	DB/MHR	80	18	89.8	16.6							
hou07x.dat	5	DB/MHR	80	18	89.6	16.8							
hou07x.dat	6	DB/MHR	80	18	89.3	16.9							
hou07x.dat	7	DB/MHR	80	18	89.2	16.9							
hou07x.dat	1	DB/MHR	85	4	71.4	15.1							
hou07x.dat	2	DB/MHR	85	4	72.7	15.5							
hou07x.dat	3	DB/MHR	85	5	73.8	15.5							
hou07x.dat	4	DB/MHR	85	5	75.3	15.8							
hou07x.dat	5	DB/MHR	76	9	75.9	15.8							
hou07x.dat	6	DB/MHR	76	10	76	16							
hou07x.dat	7	DB/MHR	72	10	76.4	15.5							
hou07x.dat	1	HR/MDB	79	14	20.2	82.7							
hou07x.dat	2	HR/MDB	79	15	20.1	83.5							
hou07x.dat	3	HR/MDB	79	16	19.8	83.8							
hou07x.dat	4	HR/MDB	79	17	19.7	82.6							
hou07x.dat	5	HR/MDB	79	17	19.5	82							
hou07x.dat	6	HR/MDB	79	29	19.4	80.4							
hou07x.dat	7	HR/MDB	79	28	19.4	80.2							
hou07x.dat	1	HR/MDB	90	14	9.7	75.1							
hou07x.dat	2	HR/MDB	90	14	10.3	76.7							
hou07x.dat	3	HR/MDB	90	15	11.2	77							
hou07x.dat	4	HR/MDB	67	17	11.9	76.6							
hou07x.dat	5	HR/MDB	67	18	12.8	76.9							
hou07x.dat	6	HR/MDB	67	19	13.5	77.1							
hou07x.dat	7	HR/MDB	84	31	13.8	79.4							
hou07x.dat	1	G/MDB	68	5	2593.1	79.8	0.72	0	0	0	0	0	0
hou07x.dat	2	G/MDB	88	24	2538.1	84.3	0.72	0.72	0	0	0	0	0
hou07x.dat	3	G/MDB	80	18	2488.6	89.7	0.7	0.72	0.68	0	0	0	0
hou07x.dat	4	G/MDB	80	17	2453.7	89.7	0.68	0.65	0.7	0.72	0	0	0
hou07x.dat	5	G/MDB	80	18	2444.1	89.6	0.68	0.65	0.7	0.72	0.68	0	0
hou07x.dat	6	G/MDB	80	18	2425	89.3	0.65	0.68	0.65	0.7	0.72	0.68	0
hou07x.dat	7	G/MDB	80	18	2404.8	89.2	0.64	0.65	0.68	0.65	0.7	0.72	0.68
hou07x.dat	1	G/MDB	79	25	669.5	77.2	0.19	0	0	0	0	0	0
hou07x.dat	2	G/MDB	61	10	782.8	77	0.23	0.21	0	0	0	0	0
hou07x.dat	3	G/MDB	83	15	816	74.8	0.2	0.24	0.24	0	0	0	0
hou07x.dat	4	G/MDB	83	15	869.5	75.4	0.29	0.2	0.24	0.24	0	0	0
hou07x.dat	5	G/MDB	83	16	998.2	76	0.29	0.2	0.24	0.24	0.42	0	0
hou07x.dat	6	G/MDB	76	12	1089.1	77.4	0.41	0.3	0.2	0.28	0.32	0.3	0
hou07x.dat	7	G/MDB	76	14	1094.8	77.8	0.3	0.2	0.28	0.32	0.3	0.42	0.31



hou10x.dat	1	DB/MHR	86	1	84.2	17.8							
hou10x.dat	2	DB/MHR	86	2	84.2	17.7							
hou10x.dat	3	DB/MHR	86	3	84.1	17.7							
hou10x.dat	4	DB/MHR	86	4	83.9	17.8							
hou10x.dat	5	DB/MHR	86	5	82.7	17.7							
hou10x.dat	6	DB/MHR	62	12	81.5	18.3							
hou10x.dat	7	DB/MHR	62	13	81.1	17.9							
hou10x.dat	1	DB/MHR	76	20	46.8	4.4							
hou10x.dat	2	DB/MHR	76	21	48	4.7							
hou10x.dat	3	DB/MHR	76	21	49.6	5.6							
hou10x.dat	4	DB/MHR	80	31	51.1	5							
hou10x.dat	5	DB/MHR	76	31	51.7	6.3							
hou10x.dat	6	DB/MHR	76	31	52.4	6.5							
hou10x.dat	7	DB/MHR	76	31	53.3	6.9							
hou10x.dat	1	HR/MDB	62	8	19.8	83.5							
hou10x.dat	2	HR/MDB	62	8	19.7	83.1							
hou10x.dat	3	HR/MDB	62	9	19.4	82.7							
hou10x.dat	4	HR/MDB	62	9	19.2	81.6							
hou10x.dat	5	HR/MDB	62	10	18.9	81.6							
hou10x.dat	6	HR/MDB	62	11	18.6	81.3							
hou10x.dat	7	HR/MDB	62	12	18.3	81							
hou10x.dat	1	HR/MDB	89	19	2.9	47.6							
hou10x.dat	2	HR/MDB	89	20	3.3	50.5							
hou10x.dat	3	HR/MDB	89	20	4.2	52.1							
hou10x.dat	4	HR/MDB	80	31	5	51.1							
hou10x.dat	5	HR/MDB	65	26	5.5	61.5							
hou10x.dat	6	HR/MDB	65	27	5.7	61.5							
hou10x.dat	7	HR/MDB	65	27	5.8	62.3							
hou10x.dat	1	G/MDB	79	4	1965.4	67.2	0.75	0	0	0	0	0	0
hou10x.dat	2	G/MDB	79	2	1941.1	75	0.73	0.73	0	0	0	0	0
hou10x.dat	3	G/MDB	87	7	1920.6	66.7	0.73	0.74	0.76	0	0	0	0
hou10x.dat	4	G/MDB	87	7	1925.8	65.3	0.74	0.73	0.74	0.76	0	0	0
hou10x.dat	5	G/MDB	87	8	1902.8	66.1	0.74	0.73	0.74	0.76	0.71	0	0
hou10x.dat	6	G/MDB	87	7	1889	66.2	0.69	0.68	0.74	0.73	0.74	0.76	0
hou10x.dat	7	G/MDB	87	8	1877.8	66.6	0.69	0.68	0.74	0.73	0.74	0.76	0.71
hou10x.dat	1	G/MDB	75	25	394.3	60.7	0.17	0	0	0	0	0	0
hou10x.dat	2	G/MDB	73	12	509.1	73.6	0.2	0.21	0	0	0	0	0
hou10x.dat	3	G/MDB	73	13	544.6	73.1	0.2	0.21	0.25	0	0	0	0
hou10x.dat	4	G/MDB	84	25	572.5	66.6	0.28	0.23	0.3	0.2	0	0	0
hou10x.dat	5	G/MDB	84	26	599.3	68.2	0.28	0.23	0.3	0.2	0.32	0	0
hou10x.dat	6	G/MDB	73	16	599.2	72.6	0.2	0.21	0.25	0.28	0.3	0.22	0
hou10x.dat	7	G/MDB	84	27	634.5	70	0.33	0.28	0.23	0.3	0.2	0.32	0.31



kan01x.dat	1	DB/MHR	67	23	60	8							
kan01x.dat	2	DB/MHR	67	23	59.4	7.4							
kan01x.dat	3	DB/MHR	67	24	57.8	7.2							
kan01x.dat	4	DB/MHR	67	24	56.3	7							
kan01x.dat	5	DB/MHR	67	24	54.1	6.1							
kan01x.dat	6	DB/MHR	67	24	50.4	5.4							
kan01x.dat	7	DB/MHR	67	25	47.6	5							
kan01x.dat	1	DB/MHR	82	10	-11.1	0.2							
kan01x.dat	2	DB/MHR	77	10	-4.2	0.3							
kan01x.dat	3	DB/MHR	77	11	-2	0.4							
kan01x.dat	4	DB/MHR	77	11	1.1	0.6							
kan01x.dat	5	DB/MHR	82	13	2.8	0.5							
kan01x.dat	6	DB/MHR	74	12	4.2	0.7							
kan01x.dat	7	DB/MHR	79	7	5	0.6							
kan01x.dat	1	HR/MDB	90	16	9.3	59.1							
kan01x.dat	2	HR/MDB	90	16	7.6	53.9							
kan01x.dat	3	HR/MDB	67	24	7.2	57.8							
kan01x.dat	4	HR/MDB	67	24	7	56.3							
kan01x.dat	5	HR/MDB	68	31	6.2	45.2							
kan01x.dat	6	HR/MDB	68	31	6.1	45.9							
kan01x.dat	7	HR/MDB	68	31	5.7	45.2							
kan01x.dat	1	HR/MDB	82	10	0.2	-11.1							
kan01x.dat	2	HR/MDB	82	11	0.3	-3.2							
kan01x.dat	3	HR/MDB	82	11	0.4	0.2							
kan01x.dat	4	HR/MDB	82	13	0.5	1.8							
kan01x.dat	5	HR/MDB	82	13	0.5	2.8							
kan01x.dat	6	HR/MDB	82	14	0.6	4.7							
kan01x.dat	7	HR/MDB	79	7	0.6	5							
kan01x.dat	1	G/MDB	77	29	1141.8	7.7	0.75	0	0	0	0	0	0
kan01x.dat	2	G/MDB	77	30	1137.6	7.8	0.75	0.73	0	0	0	0	0
kan01x.dat	3	G/MDB	77	30	1118.4	4.8	0.71	0.75	0.73	0	0	0	0
kan01x.dat	4	G/MDB	77	30	1067.4	10.6	0.61	0.71	0.75	0.73	0	0	0
kan01x.dat	5	G/MDB	77	31	1033.9	10.9	0.61	0.71	0.75	0.73	0.58	0	0
kan01x.dat	6	G/MDB	61	31	1033	23.9	0.72	0.69	0.73	0.68	0.57	0.69	0
kan01x.dat	7	G/MDB	77	30	1018.8	17.2	0.66	0.69	0.59	0.61	0.71	0.75	0.73
kan01x.dat	1	G/MDB	74	26	275.8	40.5	0.19	0	0	0	0	0	0
kan01x.dat	2	G/MDB	75	31	332.1	29.3	0.19	0.24	0	0	0	0	0
kan01x.dat	3	G/MDB	82	3	370.9	23.1	0.31	0.23	0.35	0	0	0	0
kan01x.dat	4	G/MDB	78	7	405	35.2	0.36	0.32	0.32	0.27	0	0	0
kan01x.dat	5	G/MDB	69	18	437.1	37.4	0.3	0.31	0.33	0.3	0.36	0	0
kan01x.dat	6	G/MDB	63	7	453.2	32.7	0.32	0.33	0.36	0.36	0.36	0.4	0
kan01x.dat	7	G/MDB	83	25	458	29.1	0.28	0.43	0.38	0.28	0.31	0.3	0.26



kan03x.dat	1	DB/MHR	67	30	73	8.5							
kan03x.dat	2	DB/MHR	86	30	71	7.1							
kan03x.dat	3	DB/MHR	86	31	70.5	7.4							
kan03x.dat	4	DB/MHR	86	31	70	7.3							
kan03x.dat	5	DB/MHR	86	31	66.9	6.5							
kan03x.dat	6	DB/MHR	68	30	64.7	7.9							
kan03x.dat	7	DB/MHR	86	31	64.5	6.1							
kan03x.dat	1	DB/MHR	78	4	1.4	0.5							
kan03x.dat	2	DB/MHR	78	4	5.7	0.7							
kan03x.dat	3	DB/MHR	78	5	11.9	1							
kan03x.dat	4	DB/MHR	78	4	15.1	1.4							
kan03x.dat	5	DB/MHR	78	5	16.9	1.4							
kan03x.dat	6	DB/MHR	78	6	19.7	1.6							
kan03x.dat	7	DB/MHR	78	7	21.2	1.8							
kan03x.dat	1	HR/MDB	90	13	12	65.9							
kan03x.dat	2	HR/MDB	90	11	11.1	64.3							
kan03x.dat	3	HR/MDB	90	13	10.6	64.6							
kan03x.dat	4	HR/MDB	90	13	10.9	65.3							
kan03x.dat	5	HR/MDB	90	13	10.5	63.4							
kan03x.dat	6	HR/MDB	90	14	10.1	61.4							
kan03x.dat	7	HR/MDB	90	14	9.6	59.7							
kan03x.dat	1	HR/MDB	78	4	0.5	1.4							
kan03x.dat	2	HR/MDB	78	4	0.7	5.7							
kan03x.dat	3	HR/MDB	78	5	1	11.9							
kan03x.dat	4	HR/MDB	88	16	1.3	26.4							
kan03x.dat	5	HR/MDB	88	16	1.4	27.1							
kan03x.dat	6	HR/MDB	80	6	1.6	23.9							
kan03x.dat	7	HR/MDB	65	24	1.7	26.5							
kan03x.dat	1	G/MDB	82	31	2091.2	53.1	0.75	0	0	0	0	0	0
kan03x.dat	2	G/MDB	82	31	2049.4	55.8	0.73	0.75	0	0	0	0	0
kan03x.dat	3	G/MDB	86	30	1979.1	70.2	0.72	0.73	0.72	0	0	0	0
kan03x.dat	4	G/MDB	86	31	1955.3	70	0.72	0.73	0.72	0.68	0	0	0
kan03x.dat	5	G/MDB	86	30	1939	63.6	0.71	0.69	0.72	0.73	0.72	0	0
kan03x.dat	6	G/MDB	86	31	1929.7	64.6	0.71	0.69	0.72	0.73	0.72	0.68	0
kan03x.dat	7	G/MDB	86	30	1863.1	63.2	0.72	0.55	0.71	0.69	0.72	0.73	0.72
kan03x.dat	1	G/MDB	73	4	432.4	46.4	0.2	0	0	0	0	0	0
kan03x.dat	2	G/MDB	81	4	468.5	38.9	0.22	0.21	0	0	0	0	0
kan03x.dat	3	G/MDB	73	6	557.5	47.7	0.2	0.35	0.21	0	0	0	0
kan03x.dat	4	G/MDB	73	4	573.3	48	0.26	0.31	0.3	0.2	0	0	0
kan03x.dat	5	G/MDB	73	6	596.1	48.4	0.31	0.3	0.2	0.35	0.21	0	0
kan03x.dat	6	G/MDB	73	6	588.9	48.1	0.26	0.31	0.3	0.2	0.35	0.21	0
kan03x.dat	7	G/MDB	73	7	717.3	48.4	0.26	0.31	0.3	0.2	0.35	0.21	0.66



kan07x.dat	1	DB/MHR	80	14	94	12.2							
kan07x.dat	2	DB/MHR	80	15	93.9	12.3							
kan07x.dat	3	DB/MHR	80	15	92.6	12.9							
kan07x.dat	4	DB/MHR	80	15	91.3	13.3							
kan07x.dat	5	DB/MHR	80	15	91.1	13.4							
kan07x.dat	6	DB/MHR	80	15	91.1	13.9							
kan07x.dat	7	DB/MHR	80	15	91.1	14.1							
kan07x.dat	1	DB/MHR	71	29	61.9	9.5							
kan07x.dat	2	DB/MHR	79	6	62.1	11.2							
kan07x.dat	3	DB/MHR	90	14	63.5	10.1							
kan07x.dat	4	DB/MHR	79	8	65	12.3							
kan07x.dat	5	DB/MHR	90	15	66.6	11							
kan07x.dat	6	DB/MHR	90	15	68.5	12							
kan07x.dat	7	DB/MHR	90	16	69.9	12							
kan07x.dat	1	HR/MDB	87	6	19.6	82.1							
kan07x.dat	2	HR/MDB	79	14	19.2	83.3							
kan07x.dat	3	HR/MDB	81	19	18.9	78.1							
kan07x.dat	4	HR/MDB	81	19	18.7	78.9							
kan07x.dat	5	HR/MDB	81	19	18.8	79.8							
kan07x.dat	6	HR/MDB	81	19	18.7	80.9							
kan07x.dat	7	HR/MDB	81	19	18.6	81.5							
kan07x.dat	1	HR/MDB	72	5	6.5	65.5							
kan07x.dat	2	HR/MDB	72	6	6.9	68.4							
kan07x.dat	3	HR/MDB	72	6	7.2	67.9							
kan07x.dat	4	HR/MDB	72	6	7.8	68.1							
kan07x.dat	5	HR/MDB	72	7	8.3	68.9							
kan07x.dat	6	HR/MDB	71	31	8.8	68.7							
kan07x.dat	7	HR/MDB	71	31	9.5	70							
kan07x.dat	1	G/MDB	61	4	2692.6	80	0.74	0	0	0	0	0	0
kan07x.dat	2	G/MDB	90	4	2665.5	88.2	0.73	0.73	0	0	0	0	0
kan07x.dat	3	G/MDB	73	13	2617.8	79.8	0.73	0.73	0.71	0	0	0	0
kan07x.dat	4	G/MDB	89	9	2618.4	84	0.73	0.7	0.72	0.73	0	0	0
kan07x.dat	5	G/MDB	89	9	2615	83.6	0.71	0.73	0.7	0.72	0.73	0	0
kan07x.dat	6	G/MDB	89	8	2595.4	82.3	0.73	0.68	0.71	0.73	0.7	0.72	0
kan07x.dat	7	G/MDB	89	9	2602.3	82.6	0.73	0.68	0.71	0.73	0.7	0.72	0.73
kan07x.dat	1	G/MDB	90	21	733.9	69	0.21	0	0	0	0	0	0
kan07x.dat	2	G/MDB	79	6	947.8	62.1	0.31	0.21	0	0	0	0	0
kan07x.dat	3	G/MDB	79	7	1045.4	63.9	0.31	0.21	0.34	0	0	0	0
kan07x.dat	4	G/MDB	79	8	1104.1	65	0.31	0.21	0.34	0.35	0	0	0
kan07x.dat	5	G/MDB	66	26	1258.6	80.1	0.3	0.37	0.45	0.38	0.29	0	0
kan07x.dat	6	G/MDB	66	26	1281.5	79.3	0.39	0.3	0.37	0.45	0.38	0.29	0
kan07x.dat	7	G/MDB	66	27	1320.4	80	0.39	0.3	0.37	0.45	0.38	0.29	0.44



kan10x.dat	1	DB/MHR	67	4	79.7	14.8							
kan10x.dat	2	DB/MHR	63	6	79.4	6							
kan10x.dat	3	DB/MHR	63	7	78	6.5							
kan10x.dat	4	DB/MHR	63	7	77.3	6.2							
kan10x.dat	5	DB/MHR	63	8	76.5	6.4							
kan10x.dat	6	DB/MHR	63	10	76.7	6.7							
kan10x.dat	7	DB/MHR	63	10	76.5	6.5							
kan10x.dat	1	DB/MHR	81	23	33.7	1.7							
kan10x.dat	2	DB/MHR	80	29	34.8	2.8							
kan10x.dat	3	DB/MHR	80	29	36.5	3.5							
kan10x.dat	4	DB/MHR	80	29	37.1	3.4							
kan10x.dat	5	DB/MHR	80	29	37.4	3.3							
kan10x.dat	6	DB/MHR	80	29	37.9	3.4							
kan10x.dat	7	DB/MHR	80	30	38.9	3.4							
kan10x.dat	1	HR/MDB	62	12	16.1	76.1							
kan10x.dat	2	HR/MDB	62	12	16	77							
kan10x.dat	3	HR/MDB	62	13	15.9	76.4							
kan10x.dat	4	HR/MDB	62	13	15.7	76.1							
kan10x.dat	5	HR/MDB	62	14	15.5	76							
kan10x.dat	6	HR/MDB	62	15	15.3	75.7							
kan10x.dat	7	HR/MDB	62	15	14.5	75							
kan10x.dat	1	HR/MDB	81	23	1.7	33.7							
kan10x.dat	2	HR/MDB	81	24	2.2	38							
kan10x.dat	3	HR/MDB	88	30	2.4	39.9							
kan10x.dat	4	HR/MDB	88	31	2.8	42.3							
kan10x.dat	5	HR/MDB	64	22	3.1	54.1							
kan10x.dat	6	HR/MDB	64	23	3.2	53.5							
kan10x.dat	7	HR/MDB	76	21	3.1	41.1							
kan10x.dat	1	G/MDB	81	2	1725.1	50.6	0.75	0	0	0	0	0	0
kan10x.dat	2	G/MDB	87	4	1708	54.8	0.75	0.76	0	0	0	0	0
kan10x.dat	3	G/MDB	70	4	1667.9	65.7	0.73	0.76	0.72	0	0	0	0
kan10x.dat	4	G/MDB	87	4	1630.6	56.7	0.72	0.62	0.75	0.76	0	0	0
kan10x.dat	5	G/MDB	63	5	1610.7	74.6	0.69	0.74	0.73	0.68	0.71	0	0
kan10x.dat	6	G/MDB	63	6	1602.1	75.4	0.69	0.74	0.73	0.68	0.71	0.71	0
kan10x.dat	7	G/MDB	63	7	1599.1	75.4	0.69	0.74	0.73	0.68	0.71	0.71	0.72
kan10x.dat	1	G/MDB	82	28	336.3	53.5	0.19	0	0	0	0	0	0
kan10x.dat	2	G/MDB	89	28	402.9	59.2	0.23	0.23	0	0	0	0	0
kan10x.dat	3	G/MDB	89	29	447.5	59.6	0.23	0.23	0.31	0	0	0	0
kan10x.dat	4	G/MDB	89	30	480.2	55.4	0.23	0.23	0.31	0.34	0	0	0
kan10x.dat	5	G/MDB	86	26	523.3	55.5	0.19	0.34	0.27	0.27	0.37	0	0
kan10x.dat	6	G/MDB	86	26	587.3	56.4	0.48	0.19	0.34	0.27	0.27	0.37	0
kan10x.dat	7	G/MDB	83	23	609.1	51.2	0.32	0.36	0.34	0.33	0.22	0.28	0.38



los01x.dat	1	DB/MHR	86	11	70.5	4							
los01x.dat	2	DB/MHR	76	17	68.9	4.9							
los01x.dat	3	DB/MHR	76	17	68.2	4.4							
los01x.dat	4	DB/MHR	86	13	67.1	4.4							
los01x.dat	5	DB/MHR	83	14	66.7	3.9							
los01x.dat	6	DB/MHR	83	15	66.4	4.1							
los01x.dat	7	DB/MHR	83	15	66	4.3							
los01x.dat	1	DB/MHR	71	4	44.8	1.7							
los01x.dat	2	DB/MHR	62	22	45.3	5.1							
los01x.dat	3	DB/MHR	79	30	46.1	3.6							
los01x.dat	4	DB/MHR	71	7	46.5	2							
los01x.dat	5	DB/MHR	71	7	46.9	1.8							
los01x.dat	6	DB/MHR	71	8	47.2	2.2							
los01x.dat	7	DB/MHR	71	9	47.5	2.6							
los01x.dat	1	HR/MDB	80	13	10.9	61.5							
los01x.dat	2	HR/MDB	80	13	10.8	62.7							
los01x.dat	3	HR/MDB	80	14	10.8	62.1							
los01x.dat	4	HR/MDB	80	14	10.5	61.9							
los01x.dat	5	HR/MDB	80	15	10.3	61.4							
los01x.dat	6	HR/MDB	80	16	10.1	60.9							
los01x.dat	7	HR/MDB	80	16	10	60.8							
los01x.dat	1	HR/MDB	63	12	0.8	48.6							
los01x.dat	2	HR/MDB	63	13	1.1	46.9							
los01x.dat	3	HR/MDB	71	5	1.6	46.4							
los01x.dat	4	HR/MDB	71	6	1.6	46.8							
los01x.dat	5	HR/MDB	71	7	1.8	46.9							
los01x.dat	6	HR/MDB	71	8	2.2	47.2							
los01x.dat	7	HR/MDB	71	8	2.5	48							
los01x.dat	1	G/MDB	81	31	1321.3	55	0.72	0	0	0	0	0	0
los01x.dat	2	G/MDB	62	31	1308.4	62.6	0.71	0.71	0	0	0	0	0
los01x.dat	3	G/MDB	62	31	1285.2	63.4	0.68	0.71	0.71	0	0	0	0
los01x.dat	4	G/MDB	62	31	1282.7	63.6	0.71	0.68	0.71	0.71	0	0	0
los01x.dat	5	G/MDB	62	31	1239.5	62.2	0.6	0.71	0.68	0.71	0.71	0	0
los01x.dat	6	G/MDB	62	31	1224	60.6	0.65	0.6	0.71	0.68	0.71	0.71	0
los01x.dat	7	G/MDB	62	31	1175.1	59.4	0.5	0.65	0.6	0.71	0.68	0.71	0.71
los01x.dat	1	G/MDB	80	28	230.1	56.9	0.13	0	0	0	0	0	0
los01x.dat	2	G/MDB	80	29	264.5	56.7	0.13	0.16	0	0	0	0	0
los01x.dat	3	G/MDB	80	29	301.3	57	0.21	0.13	0.16	0	0	0	0
los01x.dat	4	G/MDB	80	29	374.8	57	0.34	0.21	0.13	0.16	0	0	0
los01x.dat	5	G/MDB	80	13	396.7	61.5	0.19	0.27	0.35	0.19	0.22	0	0
los01x.dat	6	G/MDB	80	14	394	61.4	0.19	0.27	0.35	0.19	0.22	0.23	0
los01x.dat	7	G/MDB	80	14	421.1	61.3	0.37	0.19	0.27	0.35	0.19	0.22	0.23



los03x.dat	1	DB/MHR	88	25	77	5.4							
los03x.dat	2	DB/MHR	88	26	76.9	5.4							
los03x.dat	3	DB/MHR	88	26	74.8	5.9							
los03x.dat	4	DB/MHR	88	27	72.4	6.7							
los03x.dat	5	DB/MHR	88	28	70.6	7.1							
los03x.dat	6	DB/MHR	88	29	69.8	6.7							
los03x.dat	7	DB/MHR	88	30	68.5	6.9							
los03x.dat	1	DB/MHR	64	23	48.5	5.8							
los03x.dat	2	DB/MHR	66	3	48.9	3.5							
los03x.dat	3	DB/MHR	76	4	49.4	4.4							
los03x.dat	4	DB/MHR	76	5	50.5	4.6							
los03x.dat	5	DB/MHR	69	13	51.2	5.3							
los03x.dat	6	DB/MHR	69	13	51.4	5.3							
los03x.dat	7	DB/MHR	69	13	51.7	5.1							
los03x.dat	1	HR/MDB	78	1	10.5	59.7							
los03x.dat	2	HR/MDB	78	20	10.3	62.6							
los03x.dat	3	HR/MDB	78	21	10.2	62.5							
los03x.dat	4	HR/MDB	78	22	10.2	62							
los03x.dat	5	HR/MDB	78	23	10	61.7							
los03x.dat	6	HR/MDB	78	24	9.9	61.6							
los03x.dat	7	HR/MDB	78	25	9.8	62.4							
los03x.dat	1	HR/MDB	64	16	1.4	70.3							
los03x.dat	2	HR/MDB	64	17	2.2	71							
los03x.dat	3	HR/MDB	88	12	2.5	58.6							
los03x.dat	4	HR/MDB	88	13	2.7	58.8							
los03x.dat	5	HR/MDB	88	14	3.1	58.9							
los03x.dat	6	HR/MDB	88	14	3.8	58.8							
los03x.dat	7	HR/MDB	71	7	3.8	54.8							
los03x.dat	1	G/MDB	88	29	2194.3	65.7	0.76	0	0	0	0	0	0
los03x.dat	2	G/MDB	75	30	2144.8	56	0.73	0.75	0	0	0	0	0
los03x.dat	3	G/MDB	75	30	2113.1	55.3	0.71	0.73	0.75	0	0	0	0
los03x.dat	4	G/MDB	75	30	2108.4	55.1	0.73	0.71	0.73	0.75	0	0	0
los03x.dat	5	G/MDB	75	30	2081.5	55	0.7	0.73	0.71	0.73	0.75	0	0
los03x.dat	6	G/MDB	80	31	2063.4	58.5	0.74	0.66	0.73	0.73	0.7	0.72	0
los03x.dat	7	G/MDB	88	30	2023.1	68.5	0.71	0.75	0.71	0.66	0.73	0.76	0.64
los03x.dat	1	G/MDB	80	2	395.9	56.3	0.17	0	0	0	0	0	0
los03x.dat	2	G/MDB	80	2	562	57.9	0.31	0.17	0	0	0	0	0
los03x.dat	3	G/MDB	83	3	655.1	56.8	0.23	0.26	0.34	0	0	0	0
los03x.dat	4	G/MDB	78	4	711	59.1	0.24	0.29	0.31	0.35	0	0	0
los03x.dat	5	G/MDB	86	10	749.5	57	0.32	0.33	0.24	0.37	0.24	0	0
los03x.dat	6	G/MDB	86	10	785.6	57.2	0.4	0.32	0.33	0.24	0.37	0.24	0
los03x.dat	7	G/MDB	86	10	810.3	57.2	0.4	0.4	0.32	0.33	0.24	0.37	0.24



los07x.dat	1	DB/MHR	85	1	79	8.7							
los07x.dat	2	DB/MHR	85	2	78.7	8.8							
los07x.dat	3	DB/MHR	85	3	77.6	9.2							
los07x.dat	4	DB/MHR	85	4	76.4	9.7							
los07x.dat	5	DB/MHR	90	15	75.2	13							
los07x.dat	6	DB/MHR	90	16	74.6	12.9							
los07x.dat	7	DB/MHR	90	17	74.1	12.8							
los07x.dat	1	DB/MHR	65	2	60.9	9.3							
los07x.dat	2	DB/MHR	65	3	61.2	9.2							
los07x.dat	3	DB/MHR	65	3	61.6	9.2							
los07x.dat	4	DB/MHR	65	5	61.6	9.2							
los07x.dat	5	DB/MHR	65	5	61.8	9.2							
los07x.dat	6	DB/MHR	65	7	61.9	9.3							
los07x.dat	7	DB/MHR	65	7	61.9	9.3							
los07x.dat	1	HR/MDB	89	21	14.2	71.4							
los07x.dat	2	HR/MDB	89	21	13.9	71.4							
los07x.dat	3	HR/MDB	89	22	13.7	71.2							
los07x.dat	4	HR/MDB	89	22	13.4	70.6							
los07x.dat	5	HR/MDB	89	23	13.2	69.9							
los07x.dat	6	HR/MDB	90	18	13.1	73.2							
los07x.dat	7	HR/MDB	74	31	13	71.2							
los07x.dat	1	HR/MDB	64	4	8.3	62.7							
los07x.dat	2	HR/MDB	64	4	8.6	63.3							
los07x.dat	3	HR/MDB	64	5	8.7	63.3							
los07x.dat	4	HR/MDB	64	5	8.8	64							
los07x.dat	5	HR/MDB	64	5	8.9	63.9							
los07x.dat	6	HR/MDB	64	6	8.9	63.6							
los07x.dat	7	HR/MDB	64	7	9	63.4							
los07x.dat	1	G/MDB	78	2	2711.6	65.4	0.74	0	0	0	0	0	0
los07x.dat	2	G/MDB	80	6	2687.1	68.4	0.73	0.75	0	0	0	0	0
los07x.dat	3	G/MDB	80	6	2667.1	68.1	0.72	0.73	0.75	0	0	0	0
los07x.dat	4	G/MDB	78	4	2643.7	65.7	0.72	0.74	0.71	0.72	0	0	0
los07x.dat	5	G/MDB	80	12	2633.1	67.9	0.73	0.74	0.73	0.7	0.74	0	0
los07x.dat	6	G/MDB	80	10	2619.6	68.1	0.73	0.75	0.65	0.73	0.74	0.73	0
los07x.dat	7	G/MDB	80	10	2620.7	68	0.72	0.73	0.75	0.65	0.73	0.74	0.73
los07x.dat	1	G/MDB	87	16	1029	64.4	0.29	0	0	0	0	0	0
los07x.dat	2	G/MDB	87	16	1162.3	64.7	0.36	0.29	0	0	0	0	0
los07x.dat	3	G/MDB	87	17	1298.6	64.5	0.36	0.29	0.44	0	0	0	0
los07x.dat	4	G/MDB	73	9	1436.4	65.9	0.4	0.33	0.49	0.37	0	0	0
los07x.dat	5	G/MDB	62	18	1529.3	64.4	0.49	0.38	0.38	0.4	0.49	0	0
los07x.dat	6	G/MDB	73	11	1562.7	66.1	0.4	0.33	0.49	0.37	0.57	0.43	0
los07x.dat	7	G/MDB	73	12	1602	66.3	0.4	0.33	0.49	0.37	0.57	0.43	0.51



los10x.dat	1	DB/MHR	61	15	87.6	7.8							
los10x.dat	2	DB/MHR	61	15	85.7	7.1							
los10x.dat	3	DB/MHR	61	15	81.5	7.3							
los10x.dat	4	DB/MHR	65	24	80.1	4.9							
los10x.dat	5	DB/MHR	65	25	78.5	5.2							
los10x.dat	6	DB/MHR	65	25	77.3	5.6							
los10x.dat	7	DB/MHR	65	26	76.2	5.8							
los10x.dat	1	DB/MHR	71	29	52.7	2.1							
los10x.dat	2	DB/MHR	71	30	53.4	2.8							
los10x.dat	3	DB/MHR	71	31	53.8	3.8							
los10x.dat	4	DB/MHR	71	31	54.7	3.8							
los10x.dat	5	DB/MHR	71	31	55.5	4.7							
los10x.dat	6	DB/MHR	71	31	56.2	5.2							
los10x.dat	7	DB/MHR	71	31	56.2	5.4							
los10x.dat	1	HR/MDB	76	7	13.7	70.4							
los10x.dat	2	HR/MDB	76	7	13.5	69.8							
los10x.dat	3	HR/MDB	76	7	13.4	69.6							
los10x.dat	4	HR/MDB	76	7	13.2	69.4							
los10x.dat	5	HR/MDB	76	7	12.9	69.1							
los10x.dat	6	HR/MDB	76	7	12.7	68.9							
los10x.dat	7	HR/MDB	76	7	12.7	68.9							
los10x.dat	1	HR/MDB	70	28	2	66.9							
los10x.dat	2	HR/MDB	70	28	2.6	65.9							
los10x.dat	3	HR/MDB	70	29	3	65.9							
los10x.dat	4	HR/MDB	80	31	3.6	69.5							
los10x.dat	5	HR/MDB	80	31	4.5	67.8							
los10x.dat	6	HR/MDB	66	19	5.1	70.2							
los10x.dat	7	HR/MDB	70	31	5.4	62.9							
los10x.dat	1	G/MDB	71	1	1906.4	63.9	0.75	0	0	0	0	0	0
los10x.dat	2	G/MDB	71	2	1880.8	64.6	0.75	0.74	0	0	0	0	0
los10x.dat	3	G/MDB	71	3	1837.8	65.2	0.75	0.74	0.7	0	0	0	0
los10x.dat	4	G/MDB	71	4	1845.7	67	0.75	0.74	0.7	0.76	0	0	0
los10x.dat	5	G/MDB	71	5	1809.8	69.6	0.75	0.74	0.7	0.76	0.68	0	0
los10x.dat	6	G/MDB	71	6	1812.7	71.6	0.75	0.74	0.7	0.76	0.68	0.75	0
los10x.dat	7	G/MDB	71	7	1799.2	72.3	0.75	0.74	0.7	0.76	0.68	0.75	0.71
los10x.dat	1	G/MDB	87	31	347.7	61.7	0.18	0	0	0	0	0	0
los10x.dat	2	G/MDB	80	6	622	64.2	0.24	0.27	0	0	0	0	0
los10x.dat	3	G/MDB	89	22	684.9	66	0.29	0.36	0.3	0	0	0	0
los10x.dat	4	G/MDB	79	19	713.8	65.7	0.27	0.42	0.32	0.28	0	0	0
los10x.dat	5	G/MDB	79	20	813.5	65.5	0.27	0.42	0.32	0.28	0.56	0	0
los10x.dat	6	G/MDB	80	10	847.4	64.6	0.24	0.27	0.46	0.33	0.47	0.35	0
los10x.dat	7	G/MDB	80	11	878.3	64.6	0.24	0.27	0.46	0.33	0.47	0.35	0.46



mad01x.dat	1	DB/MHR	73	18	47.5	6.3							
mad01x.dat	2	DB/MHR	73	18	47.1	6							
mad01x.dat	3	DB/MHR	73	18	44.8	5.3							
mad01x.dat	4	DB/MHR	73	18	41.8	4.8							
mad01x.dat	5	DB/MHR	73	18	39.1	4.4							
mad01x.dat	6	DB/MHR	64	24	38	3.7							
mad01x.dat	7	DB/MHR	64	24	37.4	3.5							
mad01x.dat	1	DB/MHR	72	15	-18.5	0.2							
mad01x.dat	2	DB/MHR	66	29	-14.1	0.2							
mad01x.dat	3	DB/MHR	66	29	-11.1	0.2							
mad01x.dat	4	DB/MHR	63	23	-9.9	0.3							
mad01x.dat	5	DB/MHR	63	23	-9.2	0.3							
mad01x.dat	6	DB/MHR	63	24	-8.3	0.3							
mad01x.dat	7	DB/MHR	63	25	-7.8	0.3							
mad01x.dat	1	HR/MDB	73	18	6.3	47.5							
mad01x.dat	2	HR/MDB	73	18	6	47.1							
mad01x.dat	3	HR/MDB	73	18	5.3	44.8							
mad01x.dat	4	HR/MDB	73	18	4.8	41.8							
mad01x.dat	5	HR/MDB	73	18	4.4	39.1							
mad01x.dat	6	HR/MDB	73	19	4	37.2							
mad01x.dat	7	HR/MDB	73	22	3.9	36.2							
mad01x.dat	1	HR/MDB	72	15	0.2	-18.5							
mad01x.dat	2	HR/MDB	66	29	0.2	-14.1							
mad01x.dat	3	HR/MDB	66	29	0.2	-11.1							
mad01x.dat	4	HR/MDB	66	30	0.3	-9.5							
mad01x.dat	5	HR/MDB	63	24	0.3	-8.7							
mad01x.dat	6	HR/MDB	63	24	0.3	-8.3							
mad01x.dat	7	HR/MDB	63	25	0.3	-7.8							
mad01x.dat	1	G/MDB	71	30	1005.8	-3.8	0.75	0	0	0	0	0	0
mad01x.dat	2	G/MDB	77	31	982.5	5.1	0.73	0.72	0	0	0	0	0
mad01x.dat	3	G/MDB	72	30	966.5	-0.3	0.74	0.7	0.74	0	0	0	0
mad01x.dat	4	G/MDB	72	31	941.6	3.5	0.74	0.7	0.74	0.64	0	0	0
mad01x.dat	5	G/MDB	66	31	889.1	-6.6	0.66	0.63	0.71	0.7	0.65	0	0
mad01x.dat	6	G/MDB	66	31	870.6	-3.9	0.61	0.66	0.63	0.71	0.7	0.65	0
mad01x.dat	7	G/MDB	66	31	851.6	-2.9	0.58	0.61	0.66	0.63	0.71	0.7	0.65
mad01x.dat	1	G/MDB	80	16	159.1	39.8	0.14	0	0	0	0	0	0
mad01x.dat	2	G/MDB	80	17	163.7	36.9	0.14	0.14	0	0	0	0	0
mad01x.dat	3	G/MDB	80	17	180.2	36.3	0.19	0.14	0.14	0	0	0	0
mad01x.dat	4	G/MDB	80	18	217.2	34	0.19	0.14	0.14	0.28	0	0	0
mad01x.dat	5	G/MDB	83	7	228.8	25.2	0.22	0.21	0.29	0.16	0.18	0	0
mad01x.dat	6	G/MDB	83	8	232.5	25.1	0.22	0.21	0.29	0.16	0.18	0.23	0
mad01x.dat	7	G/MDB	83	10	256.6	28.5	0.21	0.29	0.16	0.18	0.23	0.41	0.17



mad03x.dat	1	DB/MHR	86	29	66.2	7.5							
mad03x.dat	2	DB/MHR	86	30	62.6	6.4							
mad03x.dat	3	DB/MHR	86	31	62.7	6.2							
mad03x.dat	4	DB/MHR	86	31	61.6	6.1							
mad03x.dat	5	DB/MHR	90	15	56.9	8.5							
mad03x.dat	6	DB/MHR	90	16	55.1	7.8							
mad03x.dat	7	DB/MHR	86	31	55.1	5.2							
mad03x.dat	1	DB/MHR	62	1	-10.7	0.2							
mad03x.dat	2	DB/MHR	62	2	-2.1	0.5							
mad03x.dat	3	DB/MHR	62	3	5.2	0.9							
mad03x.dat	4	DB/MHR	65	21	9.4	0.9							
mad03x.dat	5	DB/MHR	62	5	11.6	1.2							
mad03x.dat	6	DB/MHR	65	24	12.5	1							
mad03x.dat	7	DB/MHR	65	24	12.4	1.1							
mad03x.dat	1	HR/MDB	90	14	10.7	62							
mad03x.dat	2	HR/MDB	90	14	10.2	60.9							
mad03x.dat	3	HR/MDB	90	14	9.5	61.2							
mad03x.dat	4	HR/MDB	90	14	9	58							
mad03x.dat	5	HR/MDB	90	15	8.5	56.9							
mad03x.dat	6	HR/MDB	90	15	8	54.1							
mad03x.dat	7	HR/MDB	90	15	7.5	51.9							
mad03x.dat	1	HR/MDB	62	1	0.2	-10.7							
mad03x.dat	2	HR/MDB	62	2	0.5	-2.1							
mad03x.dat	3	HR/MDB	65	21	0.8	8.5							
mad03x.dat	4	HR/MDB	65	21	0.9	9.4							
mad03x.dat	5	HR/MDB	78	5	1	12.6							
mad03x.dat	6	HR/MDB	84	11	1	13.7							
mad03x.dat	7	HR/MDB	65	24	1.1	12.4							
mad03x.dat	1	G/MDB	72	30	2157.8	28.5	0.82	0	0	0	0	0	0
mad03x.dat	2	G/MDB	69	30	2007.9	11	0.77	0.77	0	0	0	0	0
mad03x.dat	3	G/MDB	90	27	1935.6	33.4	0.8	0.73	0.77	0	0	0	0
mad03x.dat	4	G/MDB	90	27	1908.2	31.9	0.74	0.8	0.73	0.77	0	0	0
mad03x.dat	5	G/MDB	90	27	1873.5	30.4	0.71	0.74	0.8	0.73	0.77	0	0
mad03x.dat	6	G/MDB	90	28	1817.6	32.5	0.71	0.74	0.8	0.73	0.77	0.6	0
mad03x.dat	7	G/MDB	71	26	1767.1	23.9	0.8	0.64	0.6	0.77	0.79	0.7	0.74
mad03x.dat	1	G/MDB	73	1	361.1	37.9	0.19	0	0	0	0	0	0
mad03x.dat	2	G/MDB	73	6	407.2	39.6	0.19	0.21	0	0	0	0	0
mad03x.dat	3	G/MDB	79	4	447.2	34.9	0.21	0.21	0.25	0	0	0	0
mad03x.dat	4	G/MDB	90	11	498	40.3	0.2	0.26	0.28	0.2	0	0	0
mad03x.dat	5	G/MDB	76	5	540.5	30	0.24	0.23	0.35	0.24	0.3	0	0
mad03x.dat	6	G/MDB	73	6	594.4	39.2	0.19	0.29	0.33	0.58	0.19	0.21	0
mad03x.dat	7	G/MDB	79	8	591.8	33.2	0.21	0.21	0.25	0.37	0.53	0.25	0.22



mad07x.dat	1	DB/MHR	76	10	88.7	13.2							
mad07x.dat	2	DB/MHR	76	11	86.5	12							
mad07x.dat	3	DB/MHR	76	11	85.4	11.9							
mad07x.dat	4	DB/MHR	76	11	82.8	11.3							
mad07x.dat	5	DB/MHR	88	9	81.5	12.2							
mad07x.dat	6	DB/MHR	88	9	80.7	11.7							
mad07x.dat	7	DB/MHR	87	23	80.2	15.8							
mad07x.dat	1	DB/MHR	67	4	53.7	6.6							
mad07x.dat	2	DB/MHR	67	5	55.1	6.6							
mad07x.dat	3	DB/MHR	67	5	55.6	6.7							
mad07x.dat	4	DB/MHR	67	5	56.6	7							
mad07x.dat	5	DB/MHR	67	6	57.3	7.2							
mad07x.dat	6	DB/MHR	67	7	58.9	7.6							
mad07x.dat	7	DB/MHR	67	7	60.1	8.1							
mad07x.dat	1	HR/MDB	86	18	18.7	84.5							
mad07x.dat	2	HR/MDB	86	18	18.4	84.3							
mad07x.dat	3	HR/MDB	86	18	18.3	83							
mad07x.dat	4	HR/MDB	86	19	18.1	82.1							
mad07x.dat	5	HR/MDB	86	19	17.4	80							
mad07x.dat	6	HR/MDB	86	19	16.6	78.1							
mad07x.dat	7	HR/MDB	83	22	16.3	79.5							
mad07x.dat	1	HR/MDB	72	4	6	55							
mad07x.dat	2	HR/MDB	72	5	6.2	58.1							
mad07x.dat	3	HR/MDB	72	5	6.6	58.1							
mad07x.dat	4	HR/MDB	72	6	6.8	59.5							
mad07x.dat	5	HR/MDB	72	7	7.1	59.8							
mad07x.dat	6	HR/MDB	72	8	7.4	60.7							
mad07x.dat	7	HR/MDB	72	8	7.8	61.8							
mad07x.dat	1	G/MDB	68	10	2726.8	58.9	0.75	0	0	0	0	0	0
mad07x.dat	2	G/MDB	68	10	2696.9	64.2	0.73	0.75	0	0	0	0	0
mad07x.dat	3	G/MDB	68	11	2669.5	64.5	0.73	0.75	0.72	0	0	0	0
mad07x.dat	4	G/MDB	68	11	2594.6	66.9	0.65	0.73	0.75	0.72	0	0	0
mad07x.dat	5	G/MDB	88	5	2536.6	72	0.66	0.71	0.68	0.72	0.69	0	0
mad07x.dat	6	G/MDB	76	6	2520.8	70.4	0.72	0.64	0.7	0.69	0.69	0.68	0
mad07x.dat	7	G/MDB	88	7	2493.2	75.3	0.66	0.71	0.68	0.72	0.69	0.6	0.7
mad07x.dat	1	G/MDB	89	19	521.8	64.3	0.15	0	0	0	0	0	0
mad07x.dat	2	G/MDB	89	30	767.9	65.9	0.26	0.19	0	0	0	0	0
mad07x.dat	3	G/MDB	89	21	984.2	65.2	0.15	0.48	0.21	0	0	0	0
mad07x.dat	4	G/MDB	89	21	1032.5	66.4	0.33	0.15	0.48	0.21	0	0	0
mad07x.dat	5	G/MDB	89	22	1143.7	67.1	0.33	0.15	0.48	0.21	0.45	0	0
mad07x.dat	6	G/MDB	89	22	1265.4	68.2	0.52	0.33	0.15	0.48	0.21	0.45	0
mad07x.dat	7	G/MDB	89	25	1343.4	70.3	0.15	0.48	0.21	0.45	0.59	0.47	0.33



mad10x.dat	1	DB/MHR	71	1	74.2	11.3							
mad10x.dat	2	DB/MHR	71	2	73.4	11.6							
mad10x.dat	3	DB/MHR	68	16	70.9	12.3							
mad10x.dat	4	DB/MHR	68	16	69.4	12							
mad10x.dat	5	DB/MHR	68	17	68	11.4							
mad10x.dat	6	DB/MHR	68	17	66.4	10.8							
mad10x.dat	7	DB/MHR	68	17	64.3	10							
mad10x.dat	1	DB/MHR	62	25	26.9	2							
mad10x.dat	2	DB/MHR	88	30	27.5	1.5							
mad10x.dat	3	DB/MHR	80	28	29.5	2.3							
mad10x.dat	4	DB/MHR	80	29	29.8	2.2							
mad10x.dat	5	DB/MHR	80	29	30.5	2.4							
mad10x.dat	6	DB/MHR	80	30	32.1	2.6							
mad10x.dat	7	DB/MHR	80	30	33.6	2.9							
mad10x.dat	1	HR/MDB	62	11	14.1	70.2							
mad10x.dat	2	HR/MDB	62	15	13.3	69.5							
mad10x.dat	3	HR/MDB	68	15	12.4	69.2							
mad10x.dat	4	HR/MDB	73	11	12	67.6							
mad10x.dat	5	HR/MDB	62	15	11.6	65.2							
mad10x.dat	6	HR/MDB	62	15	11.5	65.4							
mad10x.dat	7	HR/MDB	62	15	11.1	64.1							
mad10x.dat	1	HR/MDB	88	29	1.4	27.9							
mad10x.dat	2	HR/MDB	88	30	1.5	27.5							
mad10x.dat	3	HR/MDB	88	30	1.6	29.7							
mad10x.dat	4	HR/MDB	88	31	2	32.7							
mad10x.dat	5	HR/MDB	88	30	2.2	34.1							
mad10x.dat	6	HR/MDB	88	30	2.3	33.9							
mad10x.dat	7	HR/MDB	88	31	2.3	35							
mad10x.dat	1	G/MDB	75	2	1627.8	43.3	0.76	0	0	0	0	0	0
mad10x.dat	2	G/MDB	75	3	1594.2	49.9	0.76	0.74	0	0	0	0	0
mad10x.dat	3	G/MDB	75	4	1579.3	52.6	0.76	0.74	0.74	0	0	0	0
mad10x.dat	4	G/MDB	75	5	1492.5	53.8	0.76	0.74	0.74	0.6	0	0	0
mad10x.dat	5	G/MDB	75	6	1499.3	54.1	0.76	0.74	0.74	0.6	0.75	0	0
mad10x.dat	6	G/MDB	75	7	1500	54.7	0.76	0.74	0.74	0.6	0.75	0.75	0
mad10x.dat	7	G/MDB	75	7	1431.1	53	0.47	0.76	0.74	0.74	0.6	0.75	0.75
mad10x.dat	1	G/MDB	83	23	170.2	45.2	0.1	0	0	0	0	0	0
mad10x.dat	2	G/MDB	83	24	174.2	44.5	0.1	0.11	0	0	0	0	0
mad10x.dat	3	G/MDB	83	24	186.5	44.9	0.13	0.1	0.11	0	0	0	0
mad10x.dat	4	G/MDB	83	24	187	45.2	0.11	0.13	0.1	0.11	0	0	0
mad10x.dat	5	G/MDB	83	24	187.7	44.6	0.11	0.11	0.13	0.1	0.11	0	0
mad10x.dat	6	G/MDB	83	24	189.8	44.8	0.11	0.11	0.11	0.13	0.1	0.11	0
mad10x.dat	7	G/MDB	83	24	314.3	44.7	0.6	0.11	0.11	0.11	0.13	0.1	0.11



mia01x.dat	1	DB/MHR	67	3	78.1	16.3							
mia01x.dat	2	DB/MHR	71	6	77.9	17.4							
mia01x.dat	3	DB/MHR	71	6	77.7	17							
mia01x.dat	4	DB/MHR	71	7	77.5	16.8							
mia01x.dat	5	DB/MHR	71	8	77.1	16.6							
mia01x.dat	6	DB/MHR	71	9	76.8	16.5							
mia01x.dat	7	DB/MHR	71	9	76.5	16.1							
mia01x.dat	1	DB/MHR	85	22	40.6	2.6							
mia01x.dat	2	DB/MHR	85	22	42.9	2.8							
mia01x.dat	3	DB/MHR	70	10	43.8	2.8							
mia01x.dat	4	DB/MHR	70	11	46.6	3.6							
mia01x.dat	5	DB/MHR	77	22	47.8	4							
mia01x.dat	6	DB/MHR	77	22	48.5	4.3							
mia01x.dat	7	DB/MHR	77	23	49.6	4.5							
mia01x.dat	1	HR/MDB	71	6	17.8	77.8							
mia01x.dat	2	HR/MDB	71	6	17.4	77.9							
mia01x.dat	3	HR/MDB	71	7	17.1	77.5							
mia01x.dat	4	HR/MDB	71	7	16.8	77.5							
mia01x.dat	5	HR/MDB	71	8	16.6	77.1							
mia01x.dat	6	HR/MDB	71	9	16.5	76.8							
mia01x.dat	7	HR/MDB	71	10	16.2	76.3							
mia01x.dat	1	HR/MDB	85	22	2.6	40.6							
mia01x.dat	2	HR/MDB	70	10	2.7	43.2							
mia01x.dat	3	HR/MDB	70	10	2.8	43.8							
mia01x.dat	4	HR/MDB	70	11	3.6	46.6							
mia01x.dat	5	HR/MDB	77	22	4	47.8							
mia01x.dat	6	HR/MDB	77	22	4.3	48.5							
mia01x.dat	7	HR/MDB	77	23	4.5	49.6							
mia01x.dat	1	G/MDB	76	30	1652.8	56.3	0.74	0	0	0	0	0	0
mia01x.dat	2	G/MDB	79	30	1615.1	56	0.74	0.72	0	0	0	0	0
mia01x.dat	3	G/MDB	78	31	1596.8	54.1	0.7	0.73	0.71	0	0	0	0
mia01x.dat	4	G/MDB	78	31	1581.6	53.9	0.7	0.7	0.73	0.71	0	0	0
mia01x.dat	5	G/MDB	71	31	1537.1	63.8	0.7	0.72	0.73	0.69	0.64	0	0
mia01x.dat	6	G/MDB	87	31	1500.9	61.7	0.61	0.69	0.73	0.7	0.64	0.7	0
mia01x.dat	7	G/MDB	87	31	1467.3	63.2	0.58	0.61	0.69	0.73	0.7	0.64	0.7
mia01x.dat	1	G/MDB	80	27	177.2	69.9	0.08	0	0	0	0	0	0
mia01x.dat	2	G/MDB	61	12	394.5	69.4	0.17	0.22	0	0	0	0	0
mia01x.dat	3	G/MDB	61	11	438.4	68.5	0.18	0.3	0.17	0	0	0	0
mia01x.dat	4	G/MDB	61	12	440.8	69	0.18	0.3	0.17	0.22	0	0	0
mia01x.dat	5	G/MDB	61	12	502	69.2	0.37	0.18	0.3	0.17	0.22	0	0
mia01x.dat	6	G/MDB	61	13	553.3	69.7	0.37	0.18	0.3	0.17	0.22	0.39	0
mia01x.dat	7	G/MDB	61	13	642	69.4	0.58	0.37	0.18	0.3	0.17	0.22	0.39



mia03x.dat	1	DB/MHR	70	31	81.2	16.1							
mia03x.dat	2	DB/MHR	70	31	80.7	16.3							
mia03x.dat	3	DB/MHR	70	31	80.6	16.2							
mia03x.dat	4	DB/MHR	70	31	80.1	16.1							
mia03x.dat	5	DB/MHR	74	27	79.6	15.7							
mia03x.dat	6	DB/MHR	74	27	79.4	15.7							
mia03x.dat	7	DB/MHR	74	29	79.3	15.1							
mia03x.dat	1	DB/MHR	80	3	44.6	3.2							
mia03x.dat	2	DB/MHR	80	4	51.1	5							
mia03x.dat	3	DB/MHR	86	3	54.4	4.6							
mia03x.dat	4	DB/MHR	86	4	56.3	5.2							
mia03x.dat	5	DB/MHR	86	5	58.1	5.7							
mia03x.dat	6	DB/MHR	86	6	58.8	6							
mia03x.dat	7	DB/MHR	86	7	59.6	6.4							
mia03x.dat	1	HR/MDB	80	30	18.3	79.9							
mia03x.dat	2	HR/MDB	80	31	17.7	80.2							
mia03x.dat	3	HR/MDB	80	31	17.4	80.1							
mia03x.dat	4	HR/MDB	80	31	16.9	79.6							
mia03x.dat	5	HR/MDB	80	31	16.6	79.2							
mia03x.dat	6	HR/MDB	80	31	16.4	78.9							
mia03x.dat	7	HR/MDB	80	31	15.9	78.6							
mia03x.dat	1	HR/MDB	80	3	3.2	44.6							
mia03x.dat	2	HR/MDB	88	16	4	56.6							
mia03x.dat	3	HR/MDB	86	3	4.6	54.4							
mia03x.dat	4	HR/MDB	86	4	5.2	56.3							
mia03x.dat	5	HR/MDB	86	5	5.7	58.1							
mia03x.dat	6	HR/MDB	68	6	5.9	59.1							
mia03x.dat	7	HR/MDB	68	7	6.4	60.1							
mia03x.dat	1	G/MDB	64	30	2304.9	67.4	0.74	0	0	0	0	0	0
mia03x.dat	2	G/MDB	79	27	2252.6	62.7	0.74	0.73	0	0	0	0	0
mia03x.dat	3	G/MDB	63	19	2181.5	76.4	0.75	0.73	0.75	0	0	0	0
mia03x.dat	4	G/MDB	72	26	2135.3	70.8	0.74	0.71	0.65	0.71	0	0	0
mia03x.dat	5	G/MDB	72	27	2140.8	70.6	0.74	0.71	0.65	0.71	0.7	0	0
mia03x.dat	6	G/MDB	72	28	2130.7	71	0.74	0.71	0.65	0.71	0.7	0.68	0
mia03x.dat	7	G/MDB	72	29	2118.6	71.7	0.74	0.71	0.65	0.71	0.7	0.68	0.66
mia03x.dat	1	G/MDB	80	1	317.3	69.6	0.12	0	0	0	0	0	0
mia03x.dat	2	G/MDB	80	2	671.4	65.6	0.12	0.38	0	0	0	0	0
mia03x.dat	3	G/MDB	89	8	876.3	68.6	0.29	0.31	0.35	0	0	0	0
mia03x.dat	4	G/MDB	89	9	1016.9	65.1	0.29	0.31	0.35	0.51	0	0	0
mia03x.dat	5	G/MDB	87	6	1031.6	70.5	0.36	0.39	0.51	0.34	0.29	0	0
mia03x.dat	6	G/MDB	87	6	1028.6	71.6	0.38	0.36	0.39	0.51	0.34	0.29	0
mia03x.dat	7	G/MDB	87	7	1088.9	71.8	0.38	0.36	0.39	0.51	0.34	0.29	0.52



mia07x.dat	1	DB/MHR	83	24	87.2	18.6							
mia07x.dat	2	DB/MHR	83	25	87.1	18.5							
mia07x.dat	3	DB/MHR	83	26	87	18.4							
mia07x.dat	4	DB/MHR	83	26	86.6	18.4							
mia07x.dat	5	DB/MHR	83	26	86.6	18.3							
mia07x.dat	6	DB/MHR	83	26	86.2	18.4							
mia07x.dat	7	DB/MHR	83	26	86.1	18.4							
mia07x.dat	1	DB/MHR	72	19	74.4	16.6							
mia07x.dat	2	DB/MHR	65	21	76.2	16.5							
mia07x.dat	3	DB/MHR	65	22	76.3	16.5							
mia07x.dat	4	DB/MHR	65	22	76.6	16.6							
mia07x.dat	5	DB/MHR	65	22	76.7	16.7							
mia07x.dat	6	DB/MHR	65	22	77	16.6							
mia07x.dat	7	DB/MHR	65	22	77	16.5							
mia07x.dat	1	HR/MDB	80	26	20.3	84.4							
mia07x.dat	2	HR/MDB	80	26	20.1	83.9							
mia07x.dat	3	HR/MDB	80	15	20	83.2							
mia07x.dat	4	HR/MDB	80	15	19.8	83.8							
mia07x.dat	5	HR/MDB	80	16	19.6	83.1							
mia07x.dat	6	HR/MDB	80	17	19.4	82.2							
mia07x.dat	7	HR/MDB	80	18	19.2	81.9							
mia07x.dat	1	HR/MDB	81	1	13.7	82.9							
mia07x.dat	2	HR/MDB	74	15	15.2	81.4							
mia07x.dat	3	HR/MDB	67	19	15.6	83.1							
mia07x.dat	4	HR/MDB	67	19	15.7	82.4							
mia07x.dat	5	HR/MDB	67	20	15.8	82.3							
mia07x.dat	6	HR/MDB	67	20	16	81.8							
mia07x.dat	7	HR/MDB	67	30	16	82.7							
mia07x.dat	1	G/MDB	72	2	2485.9	83.3	0.7	0	0	0	0	0	0
mia07x.dat	2	G/MDB	72	29	2438.8	84	0.7	0.7	0	0	0	0	0
mia07x.dat	3	G/MDB	72	29	2442.1	84.1	0.7	0.7	0.7	0	0	0	0
mia07x.dat	4	G/MDB	72	30	2369.3	83.9	0.7	0.7	0.7	0.62	0	0	0
mia07x.dat	5	G/MDB	69	8	2356.9	85.2	0.68	0.63	0.69	0.66	0.66	0	0
mia07x.dat	6	G/MDB	69	9	2339.3	85.2	0.68	0.63	0.69	0.66	0.66	0.63	0
mia07x.dat	7	G/MDB	71	21	2321.1	83.6	0.68	0.61	0.64	0.7	0.66	0.65	0.67
mia07x.dat	1	G/MDB	85	23	198.8	74.5	0.06	0	0	0	0	0	0
mia07x.dat	2	G/MDB	85	23	512.4	76.2	0.24	0.06	0	0	0	0	0
mia07x.dat	3	G/MDB	85	24	872.9	78.3	0.24	0.06	0.45	0	0	0	0
mia07x.dat	4	G/MDB	85	14	1018.8	78.1	0.35	0.33	0.21	0.26	0	0	0
mia07x.dat	5	G/MDB	85	23	1028.2	77.3	0.27	0.36	0.54	0.24	0.06	0	0
mia07x.dat	6	G/MDB	85	23	1041.7	77.5	0.31	0.27	0.36	0.54	0.24	0.06	0
mia07x.dat	7	G/MDB	85	23	1112.5	77.8	0.44	0.31	0.27	0.36	0.54	0.24	0.06



mia10x.dat	1	DB/MHR	80	2	84.9	17.8							
mia10x.dat	2	DB/MHR	80	2	84.5	18.1							
mia10x.dat	3	DB/MHR	90	5	83.7	18.6							
mia10x.dat	4	DB/MHR	90	5	83.4	18.4							
mia10x.dat	5	DB/MHR	86	5	83.1	17.4							
mia10x.dat	6	DB/MHR	86	6	82.9	17.2							
mia10x.dat	7	DB/MHR	89	7	82.9	17.4							
mia10x.dat	1	DB/MHR	90	26	64	7.1							
mia10x.dat	2	DB/MHR	89	21	64.1	7.2							
mia10x.dat	3	DB/MHR	89	22	66	8.1							
mia10x.dat	4	DB/MHR	89	23	67.6	8.6							
mia10x.dat	5	DB/MHR	89	24	68.3	9.4							
mia10x.dat	6	DB/MHR	89	25	69.2	10.1							
mia10x.dat	7	DB/MHR	89	26	69.8	10.4							
mia10x.dat	1	HR/MDB	76	8	21.4	83.1							
mia10x.dat	2	HR/MDB	76	9	21.1	81.6							
mia10x.dat	3	HR/MDB	76	9	20.6	81.6							
mia10x.dat	4	HR/MDB	76	9	20.1	81.3							
mia10x.dat	5	HR/MDB	76	9	19.7	81							
mia10x.dat	6	HR/MDB	76	10	19.1	80.1							
mia10x.dat	7	HR/MDB	66	9	18.9	78.6							
mia10x.dat	1	HR/MDB	89	21	6.6	64.2							
mia10x.dat	2	HR/MDB	89	21	7.2	64.1							
mia10x.dat	3	HR/MDB	89	22	8.1	66							
mia10x.dat	4	HR/MDB	89	23	8.6	67.6							
mia10x.dat	5	HR/MDB	77	18	9.1	70.1							
mia10x.dat	6	HR/MDB	77	19	9.4	70.7							
mia10x.dat	7	HR/MDB	77	20	9.6	71.1							
mia10x.dat	1	G/MDB	69	4	1978.4	79.7	0.72	0	0	0	0	0	0
mia10x.dat	2	G/MDB	65	11	1943.5	79	0.72	0.74	0	0	0	0	0
mia10x.dat	3	G/MDB	72	8	1895.6	77.5	0.68	0.71	0.71	0	0	0	0
mia10x.dat	4	G/MDB	72	9	1856.7	77	0.68	0.71	0.71	0.65	0	0	0
mia10x.dat	5	G/MDB	72	10	1807	77.2	0.68	0.71	0.71	0.65	0.6	0	0
mia10x.dat	6	G/MDB	61	24	1768.5	71.9	0.69	0.73	0.74	0.72	0.7	0.68	0
mia10x.dat	7	G/MDB	86	8	1726.2	82.6	0.63	0.66	0.59	0.61	0.64	0.59	0.67
mia10x.dat	1	G/MDB	78	14	313.8	75.4	0.12	0	0	0	0	0	0
mia10x.dat	2	G/MDB	78	15	346	74.8	0.12	0.15	0	0	0	0	0
mia10x.dat	3	G/MDB	78	16	592.9	75.3	0.12	0.15	0.42	0	0	0	0
mia10x.dat	4	G/MDB	79	16	731.8	75.4	0.12	0.28	0.35	0.38	0	0	0
mia10x.dat	5	G/MDB	79	17	775.4	75.5	0.12	0.28	0.35	0.38	0.37	0	0
mia10x.dat	6	G/MDB	87	14	875.6	76.1	0.31	0.3	0.26	0.28	0.33	0.51	0
mia10x.dat	7	G/MDB	78	16	922.7	76.9	0.31	0.51	0.36	0.59	0.12	0.15	0.42



new01x.dat	1	DB/MHR	67	24	60.8	7.4							
new01x.dat	2	DB/MHR	67	24	57.9	6.6							
new01x.dat	3	DB/MHR	67	24	54.4	5.8							
new01x.dat	4	DB/MHR	67	26	51.6	5.9							
new01x.dat	5	DB/MHR	67	26	50.8	5.6							
new01x.dat	6	DB/MHR	67	27	49.2	5.4							
new01x.dat	7	DB/MHR	67	27	47.6	5							
new01x.dat	1	DB/MHR	85	21	3	0.5							
new01x.dat	2	DB/MHR	77	18	5.7	0.4							
new01x.dat	3	DB/MHR	68	10	9.3	0.6							
new01x.dat	4	DB/MHR	68	11	9.4	0.6							
new01x.dat	5	DB/MHR	68	12	10.2	0.6							
new01x.dat	6	DB/MHR	68	12	11.9	0.7							
new01x.dat	7	DB/MHR	68	13	13.6	0.8							
new01x.dat	1	HR/MDB	75	11	8.2	55.1							
new01x.dat	2	HR/MDB	79	2	7.5	51.2							
new01x.dat	3	HR/MDB	75	11	6.1	47							
new01x.dat	4	HR/MDB	67	26	5.9	51.6							
new01x.dat	5	HR/MDB	67	27	5.6	49.6							
new01x.dat	6	HR/MDB	67	27	5.4	49.2							
new01x.dat	7	HR/MDB	67	27	5	47.6							
new01x.dat	1	HR/MDB	82	17	0.4	3.9							
new01x.dat	2	HR/MDB	77	18	0.4	5.7							
new01x.dat	3	HR/MDB	82	12	0.5	10.9							
new01x.dat	4	HR/MDB	68	12	0.6	10.4							
new01x.dat	5	HR/MDB	68	12	0.6	10.2							
new01x.dat	6	HR/MDB	68	13	0.7	12.3							
new01x.dat	7	HR/MDB	68	13	0.8	13.6							
new01x.dat	1	G/MDB	63	31	1031.5	24.5	0.7	0	0	0	0	0	0
new01x.dat	2	G/MDB	81	31	986.8	23.3	0.68	0.66	0	0	0	0	0
new01x.dat	3	G/MDB	82	27	964	18.4	0.67	0.68	0.7	0	0	0	0
new01x.dat	4	G/MDB	82	27	952.2	20.3	0.66	0.67	0.68	0.7	0	0	0
new01x.dat	5	G/MDB	88	31	895.8	30.8	0.67	0.64	0.7	0.57	0.51	0	0
new01x.dat	6	G/MDB	82	29	866.1	24	0.66	0.67	0.68	0.7	0.33	0.63	0
new01x.dat	7	G/MDB	82	30	849.7	25.8	0.66	0.67	0.68	0.7	0.33	0.63	0.51
new01x.dat	1	G/MDB	64	1	190.2	30.4	0.16	0	0	0	0	0	0
new01x.dat	2	G/MDB	63	13	244.1	35.2	0.23	0.16	0	0	0	0	0
new01x.dat	3	G/MDB	63	13	240.3	36	0.19	0.23	0.16	0	0	0	0
new01x.dat	4	G/MDB	87	12	314.2	37.8	0.3	0.18	0.23	0.3	0	0	0
new01x.dat	5	G/MDB	84	6	333	36.9	0.27	0.34	0.25	0.24	0.3	0	0
new01x.dat	6	G/MDB	84	6	340.5	35.6	0.32	0.27	0.34	0.25	0.24	0.3	0
new01x.dat	7	G/MDB	84	7	360.6	35.5	0.32	0.27	0.34	0.25	0.24	0.3	0.4



new03x.dat	1	DB/MHR	85	28	68.3	7.3							
new03x.dat	2	DB/MHR	89	29	67.5	8.4							
new03x.dat	3	DB/MHR	85	29	64	6.4							
new03x.dat	4	DB/MHR	85	30	60.7	6							
new03x.dat	5	DB/MHR	89	29	57.9	6.2							
new03x.dat	6	DB/MHR	86	31	57.3	4.8							
new03x.dat	7	DB/MHR	86	31	56	4.6							
new03x.dat	1	DB/MHR	67	18	15.7	0.8							
new03x.dat	2	DB/MHR	67	19	17.5	0.9							
new03x.dat	3	DB/MHR	67	19	18.4	1							
new03x.dat	4	DB/MHR	67	19	21	1.3							
new03x.dat	5	DB/MHR	67	20	23.4	1.5							
new03x.dat	6	DB/MHR	84	13	24.3	1.6							
new03x.dat	7	DB/MHR	78	7	25.7	1.4							
new03x.dat	1	HR/MDB	90	17	9.2	59.7							
new03x.dat	2	HR/MDB	90	17	9.1	61.8							
new03x.dat	3	HR/MDB	90	17	8.4	59.9							
new03x.dat	4	HR/MDB	90	17	7.6	56.6							
new03x.dat	5	HR/MDB	90	17	7.5	57.6							
new03x.dat	6	HR/MDB	90	17	7.1	55.6							
new03x.dat	7	HR/MDB	90	17	7	55.3							
new03x.dat	1	HR/MDB	80	2	0.6	19.5							
new03x.dat	2	HR/MDB	80	2	0.7	18.3							
new03x.dat	3	HR/MDB	80	3	0.7	21.3							
new03x.dat	4	HR/MDB	80	4	0.9	26.1							
new03x.dat	5	HR/MDB	78	8	1.3	25.6							
new03x.dat	6	HR/MDB	78	7	1.3	25.4							
new03x.dat	7	HR/MDB	78	8	1.4	25.7							
new03x.dat	1	G/MDB	65	31	2130.6	34.4	0.78	0	0	0	0	0	0
new03x.dat	2	G/MDB	62	29	1926.3	54.9	0.72	0.73	0	0	0	0	0
new03x.dat	3	G/MDB	90	28	1871.8	40.3	0.68	0.74	0.71	0	0	0	0
new03x.dat	4	G/MDB	90	29	1839.4	40.9	0.68	0.74	0.71	0.65	0	0	0
new03x.dat	5	G/MDB	86	25	1834.5	39.1	0.74	0.72	0.68	0.72	0.74	0	0
new03x.dat	6	G/MDB	86	26	1823.8	42.3	0.74	0.72	0.68	0.72	0.74	0.68	0
new03x.dat	7	G/MDB	62	29	1773.1	48.4	0.69	0.73	0.67	0.66	0.56	0.72	0.73
new03x.dat	1	G/MDB	77	4	422.6	40.8	0.2	0	0	0	0	0	0
new03x.dat	2	G/MDB	76	3	453.5	36.2	0.22	0.21	0	0	0	0	0
new03x.dat	3	G/MDB	83	8	520.9	38.2	0.28	0.23	0.21	0	0	0	0
new03x.dat	4	G/MDB	83	10	545.1	39	0.23	0.21	0.32	0.22	0	0	0
new03x.dat	5	G/MDB	83	10	555.8	38.9	0.28	0.23	0.21	0.32	0.22	0	0
new03x.dat	6	G/MDB	83	11	587.5	39.1	0.28	0.23	0.21	0.32	0.22	0.33	0
new03x.dat	7	G/MDB	83	12	589.1	38.8	0.28	0.23	0.21	0.32	0.22	0.33	0.26



new07x.dat	1	DB/MHR	66	3	94.2	12							
new07x.dat	2	DB/MHR	66	3	91.7	11.7							
new07x.dat	3	DB/MHR	66	4	90.8	12.2							
new07x.dat	4	DB/MHR	66	5	88.1	12.5							
new07x.dat	5	DB/MHR	66	5	86.4	12.1							
new07x.dat	6	DB/MHR	66	7	86.1	13.2							
new07x.dat	7	DB/MHR	66	8	85.4	12.7							
new07x.dat	1	DB/MHR	72	5	60.3	8.9							
new07x.dat	2	DB/MHR	72	6	62.2	8.7							
new07x.dat	3	DB/MHR	72	7	63.7	8.8							
new07x.dat	4	DB/MHR	72	8	64.5	9.1							
new07x.dat	5	DB/MHR	72	8	65.1	9.1							
new07x.dat	6	DB/MHR	72	9	65.6	9.3							
new07x.dat	7	DB/MHR	72	10	66.5	9.5							
new07x.dat	1	HR/MDB	87	24	19	84.4							
new07x.dat	2	HR/MDB	87	25	18.5	85							
new07x.dat	3	HR/MDB	87	25	18.3	82.9							
new07x.dat	4	HR/MDB	87	25	18.1	82.2							
new07x.dat	5	HR/MDB	87	26	17.9	81.4							
new07x.dat	6	HR/MDB	87	25	17.6	81.7							
new07x.dat	7	HR/MDB	87	26	17.6	81.1							
new07x.dat	1	HR/MDB	78	1	5.3	71.3							
new07x.dat	2	HR/MDB	78	2	5.9	70.3							
new07x.dat	3	HR/MDB	79	7	6.5	67							
new07x.dat	4	HR/MDB	79	7	6.8	66.4							
new07x.dat	5	HR/MDB	79	8	7.1	68							
new07x.dat	6	HR/MDB	79	9	7.4	69.2							
new07x.dat	7	HR/MDB	79	9	7.7	70.1							
new07x.dat	1	G/MDB	65	1	2784.5	74.2	0.76	0	0	0	0	0	0
new07x.dat	2	G/MDB	71	4	2695.8	72.3	0.72	0.75	0	0	0	0	0
new07x.dat	3	G/MDB	71	5	2658	72.4	0.72	0.75	0.71	0	0	0	0
new07x.dat	4	G/MDB	78	8	2516.3	73.5	0.7	0.7	0.66	0.69	0	0	0
new07x.dat	5	G/MDB	78	9	2474.1	74.5	0.7	0.7	0.66	0.69	0.63	0	0
new07x.dat	6	G/MDB	71	8	2487.7	76.7	0.72	0.75	0.71	0.52	0.67	0.71	0
new07x.dat	7	G/MDB	71	8	2402.2	76.7	0.52	0.72	0.75	0.71	0.52	0.67	0.71
new07x.dat	1	G/MDB	81	4	697.7	71.3	0.19	0	0	0	0	0	0
new07x.dat	2	G/MDB	64	9	861	66.5	0.22	0.25	0	0	0	0	0
new07x.dat	3	G/MDB	61	15	956.1	68.5	0.26	0.32	0.21	0	0	0	0
new07x.dat	4	G/MDB	69	24	1085	68.3	0.32	0.33	0.28	0.3	0	0	0
new07x.dat	5	G/MDB	69	24	1099.7	68.3	0.33	0.32	0.33	0.28	0.3	0	0
new07x.dat	6	G/MDB	69	24	1129.4	69	0.36	0.33	0.32	0.33	0.28	0.3	0
new07x.dat	7	G/MDB	69	26	1213.4	68.2	0.33	0.32	0.33	0.28	0.3	0.53	0.33



new10x.dat	1	DB/MHR	86	1	76	12.4							
new10x.dat	2	DB/MHR	67	5	74.7	10							
new10x.dat	3	DB/MHR	90	11	73.7	13.8							
new10x.dat	4	DB/MHR	90	11	73.5	13.8							
new10x.dat	5	DB/MHR	90	10	73.4	12.3							
new10x.dat	6	DB/MHR	90	11	73.4	12.5							
new10x.dat	7	DB/MHR	90	12	73.2	12.8							
new10x.dat	1	DB/MHR	69	23	35.8	1.7							
new10x.dat	2	DB/MHR	72	20	38	2.7							
new10x.dat	3	DB/MHR	74	21	39.3	1.9							
new10x.dat	4	DB/MHR	72	21	40.5	2.8							
new10x.dat	5	DB/MHR	74	22	42.6	2.2							
new10x.dat	6	DB/MHR	74	23	44.8	2.5							
new10x.dat	7	DB/MHR	62	30	45.3	3.8							
new10x.dat	1	HR/MDB	90	13	16.1	72.3							
new10x.dat	2	HR/MDB	90	13	15.3	72.1							
new10x.dat	3	HR/MDB	90	13	14.7	72.5							
new10x.dat	4	HR/MDB	90	13	14.4	72.8							
new10x.dat	5	HR/MDB	90	13	14.4	73							
new10x.dat	6	HR/MDB	90	13	14.3	73							
new10x.dat	7	HR/MDB	90	14	14.1	73.1							
new10x.dat	1	HR/MDB	65	29	1.5	40.1							
new10x.dat	2	HR/MDB	65	30	1.7	45							
new10x.dat	3	HR/MDB	65	30	1.9	45.8							
new10x.dat	4	HR/MDB	74	22	2	42.1							
new10x.dat	5	HR/MDB	74	22	2.2	42.6							
new10x.dat	6	HR/MDB	74	23	2.5	44.8							
new10x.dat	7	HR/MDB	69	29	2.6	45.6							
new10x.dat	1	G/MDB	66	2	1681.1	54	0.75	0	0	0	0	0	0
new10x.dat	2	G/MDB	65	5	1629.2	44.8	0.73	0.77	0	0	0	0	0
new10x.dat	3	G/MDB	65	5	1567.2	49.9	0.65	0.73	0.77	0	0	0	0
new10x.dat	4	G/MDB	65	5	1588.7	53	0.74	0.65	0.73	0.77	0	0	0
new10x.dat	5	G/MDB	63	6	1467.3	61.8	0.72	0.49	0.72	0.71	0.71	0	0
new10x.dat	6	G/MDB	63	6	1473.4	61.3	0.67	0.72	0.49	0.72	0.71	0.71	0
new10x.dat	7	G/MDB	63	7	1454.8	62.7	0.67	0.72	0.49	0.72	0.71	0.71	0.63
new10x.dat	1	G/MDB	64	17	327.5	60.2	0.17	0	0	0	0	0	0
new10x.dat	2	G/MDB	83	24	407.7	53.7	0.21	0.25	0	0	0	0	0
new10x.dat	3	G/MDB	75	19	459.7	56.5	0.29	0.24	0.2	0	0	0	0
new10x.dat	4	G/MDB	83	26	481.1	51.6	0.21	0.25	0.33	0.31	0	0	0
new10x.dat	5	G/MDB	81	30	566.7	53.6	0.27	0.29	0.54	0.32	0.28	0	0
new10x.dat	6	G/MDB	81	30	554	52.9	0.28	0.27	0.29	0.54	0.32	0.28	0
new10x.dat	7	G/MDB	81	31	554.2	52.5	0.28	0.27	0.29	0.54	0.32	0.28	0.34



san01x.dat	1	DB/MHR	80	12	62.5	10.2							
san01x.dat	2	DB/MHR	80	13	61.5	10							
san01x.dat	3	DB/MHR	70	23	60.2	9.6							
san01x.dat	4	DB/MHR	70	23	59.5	9.5							
san01x.dat	5	DB/MHR	70	23	59.1	9.3							
san01x.dat	6	DB/MHR	70	24	58.3	8.9							
san01x.dat	7	DB/MHR	70	22	58.2	9							
san01x.dat	1	DB/MHR	62	21	34.6	3							
san01x.dat	2	DB/MHR	62	22	36.6	2.4							
san01x.dat	3	DB/MHR	62	23	38.1	2.5							
san01x.dat	4	DB/MHR	62	24	39.4	2.8							
san01x.dat	5	DB/MHR	68	8	40.1	4.2							
san01x.dat	6	DB/MHR	68	8	40.5	4.1							
san01x.dat	7	DB/MHR	68	8	40.8	4.1							
san01x.dat	1	HR/MDB	63	31	10.2	61.4							
san01x.dat	2	HR/MDB	80	13	10	61.5							
san01x.dat	3	HR/MDB	70	22	9.6	59.6							
san01x.dat	4	HR/MDB	70	23	9.5	59.5							
san01x.dat	5	HR/MDB	70	23	9.3	59.1							
san01x.dat	6	HR/MDB	70	23	9	58.3							
san01x.dat	7	HR/MDB	70	22	9	58.2							
san01x.dat	1	HR/MDB	63	12	1.5	40.1							
san01x.dat	2	HR/MDB	63	12	1.7	41.6							
san01x.dat	3	HR/MDB	63	13	1.9	41.5							
san01x.dat	4	HR/MDB	63	14	2.1	41.4							
san01x.dat	5	HR/MDB	63	15	2.3	41.6							
san01x.dat	6	HR/MDB	63	16	2.6	41.8							
san01x.dat	7	HR/MDB	63	17	2.9	41.8							
san01x.dat	1	G/MDB	72	30	1178.9	45	0.72	0	0	0	0	0	0
san01x.dat	2	G/MDB	72	31	1107	44	0.72	0.63	0	0	0	0	0
san01x.dat	3	G/MDB	71	29	1060.4	48.5	0.67	0.69	0.62	0	0	0	0
san01x.dat	4	G/MDB	71	30	1038.4	47.7	0.67	0.69	0.62	0.59	0	0	0
san01x.dat	5	G/MDB	79	29	1026.3	45.5	0.68	0.68	0.61	0.62	0.63	0	0
san01x.dat	6	G/MDB	75	27	999.5	48.2	0.68	0.56	0.63	0.63	0.65	0.69	0
san01x.dat	7	G/MDB	80	25	990.3	48.9	0.67	0.62	0.6	0.67	0.67	0.64	0.67
san01x.dat	1	G/MDB	66	4	192.4	51.6	0.14	0	0	0	0	0	0
san01x.dat	2	G/MDB	65	3	240.1	46.8	0.17	0.19	0	0	0	0	0
san01x.dat	3	G/MDB	65	4	255.2	48.3	0.17	0.19	0.21	0	0	0	0
san01x.dat	4	G/MDB	65	5	259	50	0.17	0.19	0.21	0.2	0	0	0
san01x.dat	5	G/MDB	65	6	306.7	50.3	0.17	0.19	0.21	0.2	0.36	0	0
san01x.dat	6	G/MDB	80	15	364.5	56.2	0.23	0.27	0.31	0.26	0.24	0.23	0
san01x.dat	7	G/MDB	80	16	366.4	56.2	0.23	0.27	0.31	0.26	0.24	0.23	0.26



san03x.dat	1	DB/MHR	78	17	64.7	8.1							
san03x.dat	2	DB/MHR	78	18	64.4	7.8							
san03x.dat	3	DB/MHR	78	18	63.4	7.9							
san03x.dat	4	DB/MHR	78	19	62.6	8							
san03x.dat	5	DB/MHR	78	20	61.9	8.1							
san03x.dat	6	DB/MHR	78	21	61.2	8.2							
san03x.dat	7	DB/MHR	78	22	60.7	8.2							
san03x.dat	1	DB/MHR	76	2	40.1	4.1							
san03x.dat	2	DB/MHR	76	2	42	4.1							
san03x.dat	3	DB/MHR	76	3	43.1	4.1							
san03x.dat	4	DB/MHR	76	4	43.9	4							
san03x.dat	5	DB/MHR	76	5	44.8	4							
san03x.dat	6	DB/MHR	76	6	45.4	4.2							
san03x.dat	7	DB/MHR	76	7	46	4.3							
san03x.dat	1	HR/MDB	86	7	10.2	60.2							
san03x.dat	2	HR/MDB	86	7	9.4	58.6							
san03x.dat	3	HR/MDB	89	10	9.2	59.1							
san03x.dat	4	HR/MDB	89	11	9.1	58.8							
san03x.dat	5	HR/MDB	89	10	8.9	57.5							
san03x.dat	6	HR/MDB	89	11	8.9	57.6							
san03x.dat	7	HR/MDB	89	12	8.7	57.2							
san03x.dat	1	HR/MDB	75	28	2.3	50							
san03x.dat	2	HR/MDB	75	29	2.8	51.2							
san03x.dat	3	HR/MDB	75	28	3	50.2							
san03x.dat	4	HR/MDB	75	29	3.1	50.7							
san03x.dat	5	HR/MDB	75	29	3.5	51.1							
san03x.dat	6	HR/MDB	75	31	3.9	50.6							
san03x.dat	7	HR/MDB	75	31	4.1	50.9							
san03x.dat	1	G/MDB	71	31	2126.8	50.6	0.75	0	0	0	0	0	0
san03x.dat	2	G/MDB	70	31	2089.3	58.3	0.74	0.74	0	0	0	0	0
san03x.dat	3	G/MDB	88	29	2055	56.6	0.76	0.74	0.73	0	0	0	0
san03x.dat	4	G/MDB	88	30	2057.6	57	0.76	0.74	0.73	0.74	0	0	0
san03x.dat	5	G/MDB	88	31	2052.6	58.3	0.76	0.74	0.73	0.74	0.72	0	0
san03x.dat	6	G/MDB	88	31	2040.7	58.5	0.73	0.76	0.74	0.73	0.74	0.72	0
san03x.dat	7	G/MDB	88	31	2023.2	58.8	0.71	0.73	0.76	0.74	0.73	0.74	0.72
san03x.dat	1	G/MDB	66	9	438.1	52.6	0.19	0	0	0	0	0	0
san03x.dat	2	G/MDB	83	17	540.8	49.9	0.24	0.19	0	0	0	0	0
san03x.dat	3	G/MDB	89	6	576	52.1	0.2	0.33	0.22	0	0	0	0
san03x.dat	4	G/MDB	78	4	638	56.7	0.27	0.29	0.3	0.29	0	0	0
san03x.dat	5	G/MDB	89	8	627	53.8	0.2	0.33	0.22	0.37	0.23	0	0
san03x.dat	6	G/MDB	89	9	644.4	54.8	0.2	0.33	0.22	0.37	0.23	0.31	0
san03x.dat	7	G/MDB	89	10	632	55.5	0.2	0.33	0.22	0.37	0.23	0.31	0.23



san07x.dat	1	DB/MHR	70	2	77.6	8.5							
san07x.dat	2	DB/MHR	72	14	75.4	9.1							
san07x.dat	3	DB/MHR	72	14	72.7	9							
san07x.dat	4	DB/MHR	72	15	71.3	9.2							
san07x.dat	5	DB/MHR	72	16	70.4	9.3							
san07x.dat	6	DB/MHR	72	17	69.5	9.4							
san07x.dat	7	DB/MHR	72	17	68.7	9.3							
san07x.dat	1	DB/MHR	65	5	53.3	7.1							
san07x.dat	2	DB/MHR	65	6	53.7	7.2							
san07x.dat	3	DB/MHR	65	5	53.8	7.1							
san07x.dat	4	DB/MHR	65	6	53.9	7.2							
san07x.dat	5	DB/MHR	65	6	53.9	7.2							
san07x.dat	6	DB/MHR	65	7	54.4	7.2							
san07x.dat	7	DB/MHR	65	7	54.8	7.3							
san07x.dat	1	HR/MDB	88	24	10.4	66.8							
san07x.dat	2	HR/MDB	88	25	10.3	65.9							
san07x.dat	3	HR/MDB	88	25	10.2	66.2							
san07x.dat	4	HR/MDB	88	25	10.1	65.8							
san07x.dat	5	HR/MDB	88	26	10	65.4							
san07x.dat	6	HR/MDB	88	26	10	64.9							
san07x.dat	7	HR/MDB	88	26	9.9	64.9							
san07x.dat	1	HR/MDB	85	2	5.8	69.7							
san07x.dat	2	HR/MDB	85	2	5.9	72.6							
san07x.dat	3	HR/MDB	77	5	6.4	57.3							
san07x.dat	4	HR/MDB	77	6	6.4	57.8							
san07x.dat	5	HR/MDB	77	7	6.5	57.7							
san07x.dat	6	HR/MDB	77	9	6.5	57.8							
san07x.dat	7	HR/MDB	77	9	6.5	57.6							
san07x.dat	1	G/MDB	73	1	2741.1	59.7	0.75	0	0	0	0	0	0
san07x.dat	2	G/MDB	74	2	2725.9	60	0.74	0.74	0	0	0	0	0
san07x.dat	3	G/MDB	69	4	2677.9	60.5	0.73	0.72	0.75	0	0	0	0
san07x.dat	4	G/MDB	73	4	2669.9	59.6	0.75	0.7	0.74	0.73	0	0	0
san07x.dat	5	G/MDB	62	5	2670.2	58.7	0.75	0.73	0.7	0.73	0.74	0	0
san07x.dat	6	G/MDB	62	6	2668.8	58.9	0.75	0.73	0.7	0.73	0.74	0.73	0
san07x.dat	7	G/MDB	69	8	2629.3	60.2	0.73	0.72	0.75	0.68	0.72	0.71	0.73
san07x.dat	1	G/MDB	74	8	725.9	61.1	0.2	0	0	0	0	0	0
san07x.dat	2	G/MDB	64	4	1033.9	55.5	0.29	0.27	0	0	0	0	0
san07x.dat	3	G/MDB	71	29	1223.3	56.8	0.35	0.32	0.39	0	0	0	0
san07x.dat	4	G/MDB	71	29	1427.2	56.8	0.58	0.35	0.32	0.39	0	0	0
san07x.dat	5	G/MDB	71	29	1545.2	57.4	0.57	0.58	0.35	0.32	0.39	0	0
san07x.dat	6	G/MDB	71	29	1572.8	57.2	0.48	0.57	0.58	0.35	0.32	0.39	0
san07x.dat	7	G/MDB	71	30	1646	57.7	0.48	0.57	0.58	0.35	0.32	0.39	0.6



san10x.dat	1	DB/MHR	87	5	77.9	7.3							
san10x.dat	2	DB/MHR	80	2	75.8	7.5							
san10x.dat	3	DB/MHR	87	6	73.7	8							
san10x.dat	4	DB/MHR	87	6	71.2	8.2							
san10x.dat	5	DB/MHR	87	7	69.5	8.3							
san10x.dat	6	DB/MHR	87	7	68	8.3							
san10x.dat	7	DB/MHR	67	17	67	6.7							
san10x.dat	1	DB/MHR	71	30	49.8	5.5							
san10x.dat	2	DB/MHR	71	30	50	4							
san10x.dat	3	DB/MHR	71	30	50.2	3.4							
san10x.dat	4	DB/MHR	71	30	50.5	3.8							
san10x.dat	5	DB/MHR	71	31	50.9	4.2							
san10x.dat	6	DB/MHR	71	31	51.2	4.6							
san10x.dat	7	DB/MHR	71	31	51.4	4.7							
san10x.dat	1	HR/MDB	62	12	11.1	63.9							
san10x.dat	2	HR/MDB	62	12	11	63.7							
san10x.dat	3	HR/MDB	62	12	10.8	63.2							
san10x.dat	4	HR/MDB	62	12	10.6	63.3							
san10x.dat	5	HR/MDB	62	12	10.5	63.2							
san10x.dat	6	HR/MDB	62	13	10.4	62.5							
san10x.dat	7	HR/MDB	62	14	10	61.7							
san10x.dat	1	HR/MDB	71	28	2.1	50.5							
san10x.dat	2	HR/MDB	71	29	2.3	50.3							
san10x.dat	3	HR/MDB	71	29	3.2	50.8							
san10x.dat	4	HR/MDB	71	30	3.8	50.5							
san10x.dat	5	HR/MDB	71	31	4.2	50.9							
san10x.dat	6	HR/MDB	71	30	4.6	51.3							
san10x.dat	7	HR/MDB	71	30	4.7	51.6							
san10x.dat	1	G/MDB	71	1	1786	57.4	0.75	0	0	0	0	0	0
san10x.dat	2	G/MDB	71	2	1763.8	57.9	0.75	0.74	0	0	0	0	0
san10x.dat	3	G/MDB	71	3	1746.8	58.7	0.75	0.74	0.73	0	0	0	0
san10x.dat	4	G/MDB	71	4	1727.7	60.3	0.75	0.74	0.73	0.72	0	0	0
san10x.dat	5	G/MDB	71	5	1725.7	60.9	0.75	0.74	0.73	0.72	0.75	0	0
san10x.dat	6	G/MDB	71	6	1714.9	60.1	0.75	0.74	0.73	0.72	0.75	0.73	0
san10x.dat	7	G/MDB	71	7	1705.8	59.7	0.75	0.74	0.73	0.72	0.75	0.73	0.73
san10x.dat	1	G/MDB	83	29	407.7	63.9	0.22	0	0	0	0	0	0
san10x.dat	2	G/MDB	83	30	421.3	64.3	0.22	0.24	0	0	0	0	0
san10x.dat	3	G/MDB	62	12	502	63.2	0.2	0.27	0.23	0	0	0	0
san10x.dat	4	G/MDB	62	13	489.9	62.2	0.2	0.27	0.23	0.21	0	0	0
san10x.dat	5	G/MDB	64	29	642.2	58.2	0.34	0.53	0.29	0.25	0.3	0	0
san10x.dat	6	G/MDB	64	29	631.7	57.6	0.3	0.34	0.53	0.29	0.25	0.3	0
san10x.dat	7	G/MDB	64	29	699	57.2	0.57	0.3	0.34	0.53	0.29	0.25	0.3



sea01x.dat	1	DB/MHR	81	21	56	6.5							
sea01x.dat	2	DB/MHR	81	21	55.5	5.9							
sea01x.dat	3	DB/MHR	81	21	54.5	5.8							
sea01x.dat	4	DB/MHR	81	21	54.2	5.6							
sea01x.dat	5	DB/MHR	81	22	53.5	5.9							
sea01x.dat	6	DB/MHR	81	22	52.4	5.6							
sea01x.dat	7	DB/MHR	81	23	51.5	5.7							
sea01x.dat	1	DB/MHR	63	11	17	0.7							
sea01x.dat	2	DB/MHR	63	12	19.1	0.8							
sea01x.dat	3	DB/MHR	63	12	20.7	0.9							
sea01x.dat	4	DB/MHR	63	13	22.5	1.2							
sea01x.dat	5	DB/MHR	69	30	23.8	1.9							
sea01x.dat	6	DB/MHR	69	28	24.2	1.5							
sea01x.dat	7	DB/MHR	69	29	24.2	1.6							
sea01x.dat	1	HR/MDB	84	4	8.2	55.4							
sea01x.dat	2	HR/MDB	84	4	8.1	54.8							
sea01x.dat	3	HR/MDB	84	5	7.7	52.7							
sea01x.dat	4	HR/MDB	84	6	7.6	52.2							
sea01x.dat	5	HR/MDB	84	7	7.3	51.2							
sea01x.dat	6	HR/MDB	84	7	7	50.3							
sea01x.dat	7	HR/MDB	84	8	6.7	49.7							
sea01x.dat	1	HR/MDB	79	1	0.6	25.6							
sea01x.dat	2	HR/MDB	80	28	0.6	23.5							
sea01x.dat	3	HR/MDB	80	29	0.7	23.5							
sea01x.dat	4	HR/MDB	80	29	0.7	24.4							
sea01x.dat	5	HR/MDB	80	30	0.7	25.5							
sea01x.dat	6	HR/MDB	80	31	1	27.2							
sea01x.dat	7	HR/MDB	79	7	1	33.4							
sea01x.dat	1	G/MDB	72	30	761.4	27.4	0.69	0	0	0	0	0	0
sea01x.dat	2	G/MDB	79	31	731.6	33.7	0.68	0.63	0	0	0	0	0
sea01x.dat	3	G/MDB	79	30	720.8	34.4	0.68	0.63	0.68	0	0	0	0
sea01x.dat	4	G/MDB	79	31	718	33.9	0.68	0.63	0.68	0.63	0	0	0
sea01x.dat	5	G/MDB	80	30	651	25.5	0.62	0.62	0.63	0.62	0.53	0	0
sea01x.dat	6	G/MDB	80	30	614	27.3	0.42	0.62	0.62	0.63	0.62	0.53	0
sea01x.dat	7	G/MDB	79	31	570.1	35.3	0.56	0.2	0.31	0.68	0.63	0.68	0.63
sea01x.dat	1	G/MDB	79	10	58.3	40.3	0.07	0	0	0	0	0	0
sea01x.dat	2	G/MDB	89	9	89.6	40.1	0.1	0.11	0	0	0	0	0
sea01x.dat	3	G/MDB	78	5	96.5	44.3	0.11	0.13	0.11	0	0	0	0
sea01x.dat	4	G/MDB	84	5	106.4	51	0.13	0.14	0.11	0.14	0	0	0
sea01x.dat	5	G/MDB	84	6	112.3	50.9	0.13	0.14	0.11	0.14	0.16	0	0
sea01x.dat	6	G/MDB	78	8	116.3	43.6	0.11	0.13	0.11	0.24	0.11	0.14	0
sea01x.dat	7	G/MDB	78	9	114.9	44.4	0.11	0.13	0.11	0.24	0.11	0.14	0.12



sea03x.dat	1	DB/MHR	66	29	57.6	5.8							
sea03x.dat	2	DB/MHR	87	31	56.7	3.9							
sea03x.dat	3	DB/MHR	87	31	55.7	3.2							
sea03x.dat	4	DB/MHR	72	17	54.2	7.1							
sea03x.dat	5	DB/MHR	72	17	53.6	7.1							
sea03x.dat	6	DB/MHR	72	17	53.5	7.2							
sea03x.dat	7	DB/MHR	72	17	53.2	7.1							
sea03x.dat	1	DB/MHR	89	2	28.4	2.5							
sea03x.dat	2	DB/MHR	89	3	29.1	2.4							
sea03x.dat	3	DB/MHR	89	3	29.7	2.7							
sea03x.dat	4	DB/MHR	89	4	31.5	2.7							
sea03x.dat	5	DB/MHR	76	5	33.7	2.8							
sea03x.dat	6	DB/MHR	76	6	34.7	3.1							
sea03x.dat	7	DB/MHR	76	7	35.5	3.3							
sea03x.dat	1	HR/MDB	83	9	8.2	55.1							
sea03x.dat	2	HR/MDB	79	6	7.7	54.5							
sea03x.dat	3	HR/MDB	79	6	7.4	53.7							
sea03x.dat	4	HR/MDB	72	18	7.2	53.8							
sea03x.dat	5	HR/MDB	72	16	7.3	53.3							
sea03x.dat	6	HR/MDB	72	17	7.2	53.5							
sea03x.dat	7	HR/MDB	72	18	7.1	53							
sea03x.dat	1	HR/MDB	65	24	1.4	40							
sea03x.dat	2	HR/MDB	65	19	1.7	39.8							
sea03x.dat	3	HR/MDB	65	19	1.8	39.1							
sea03x.dat	4	HR/MDB	65	19	2.1	39.7							
sea03x.dat	5	HR/MDB	65	20	2.4	40.8							
sea03x.dat	6	HR/MDB	65	20	2.7	41.3							
sea03x.dat	7	HR/MDB	65	24	2.8	42.3							
sea03x.dat	1	G/MDB	62	30	1822.4	53.3	0.74	0	0	0	0	0	0
sea03x.dat	2	G/MDB	62	31	1806.7	52.4	0.74	0.72	0	0	0	0	0
sea03x.dat	3	G/MDB	62	31	1799.9	51.9	0.74	0.74	0.72	0	0	0	0
sea03x.dat	4	G/MDB	62	31	1771.6	49.5	0.7	0.74	0.74	0.72	0	0	0
sea03x.dat	5	G/MDB	79	24	1588.8	51.9	0.71	0.7	0.71	0.7	0.7	0	0
sea03x.dat	6	G/MDB	79	24	1573.1	51.3	0.69	0.71	0.7	0.71	0.7	0.7	0
sea03x.dat	7	G/MDB	79	24	1542.8	50.9	0.63	0.69	0.71	0.7	0.71	0.7	0.7
sea03x.dat	1	G/MDB	84	25	207.6	43.6	0.09	0	0	0	0	0	0
sea03x.dat	2	G/MDB	83	9	270.7	52.7	0.11	0.17	0	0	0	0	0
sea03x.dat	3	G/MDB	79	5	308.7	50.5	0.15	0.19	0.18	0	0	0	0
sea03x.dat	4	G/MDB	90	9	341.3	42.3	0.14	0.17	0.22	0.2	0	0	0
sea03x.dat	5	G/MDB	90	9	411.8	43.4	0.38	0.14	0.17	0.22	0.2	0	0
sea03x.dat	6	G/MDB	83	9	477.8	49.7	0.37	0.26	0.39	0.26	0.11	0.17	0
sea03x.dat	7	G/MDB	83	9	460.3	49	0.2	0.37	0.26	0.39	0.26	0.11	0.17



sea07x.dat	1	DB/MHR	61	12	82.4	10.9							
sea07x.dat	2	DB/MHR	79	17	80.5	8.5							
sea07x.dat	3	DB/MHR	61	13	79.1	10.6							
sea07x.dat	4	DB/MHR	79	19	77.7	8.8							
sea07x.dat	5	DB/MHR	79	19	76.8	8.7							
sea07x.dat	6	DB/MHR	79	20	75.7	8.8							
sea07x.dat	7	DB/MHR	79	20	74.3	8.6							
sea07x.dat	1	DB/MHR	79	1	52.3	6.1							
sea07x.dat	2	DB/MHR	66	2	53.1	7.7							
sea07x.dat	3	DB/MHR	66	3	53.4	7.9							
sea07x.dat	4	DB/MHR	66	4	54.9	7.9							
sea07x.dat	5	DB/MHR	66	5	55.3	8							
sea07x.dat	6	DB/MHR	66	6	55.9	7.9							
sea07x.dat	7	DB/MHR	66	7	56.8	8							
sea07x.dat	1	HR/MDB	90	12	11.3	77							
sea07x.dat	2	HR/MDB	90	12	11.1	76.4							
sea07x.dat	3	HR/MDB	61	13	10.6	79.1							
sea07x.dat	4	HR/MDB	61	14	10.4	76							
sea07x.dat	5	HR/MDB	61	14	10.2	75							
sea07x.dat	6	HR/MDB	71	31	10.1	69.5							
sea07x.dat	7	HR/MDB	71	31	10.1	69.9							
sea07x.dat	1	HR/MDB	70	9	5.5	64.9							
sea07x.dat	2	HR/MDB	62	3	5.7	60.8							
sea07x.dat	3	HR/MDB	62	3	5.8	59.6							
sea07x.dat	4	HR/MDB	81	9	6	57.4							
sea07x.dat	5	HR/MDB	77	6	6.1	59.3							
sea07x.dat	6	HR/MDB	81	11	6.2	57.2							
sea07x.dat	7	HR/MDB	81	12	6.4	57.7							
sea07x.dat	1	G/MDB	61	9	2719.9	68.5	0.75	0	0	0	0	0	0
sea07x.dat	2	G/MDB	61	9	2717.2	66.5	0.75	0.75	0	0	0	0	0
sea07x.dat	3	G/MDB	61	10	2681.9	68	0.75	0.75	0.72	0	0	0	0
sea07x.dat	4	G/MDB	61	11	2665.7	70.5	0.75	0.75	0.72	0.73	0	0	0
sea07x.dat	5	G/MDB	61	12	2655.7	72.9	0.75	0.75	0.72	0.73	0.73	0	0
sea07x.dat	6	G/MDB	61	13	2649.2	73.5	0.75	0.75	0.72	0.73	0.73	0.73	0
sea07x.dat	7	G/MDB	61	13	2594.9	72	0.62	0.75	0.75	0.72	0.73	0.73	0.73
sea07x.dat	1	G/MDB	90	25	583.3	58.6	0.17	0	0	0	0	0	0
sea07x.dat	2	G/MDB	66	3	705.3	53.5	0.22	0.16	0	0	0	0	0
sea07x.dat	3	G/MDB	66	3	764.4	53.4	0.24	0.22	0.16	0	0	0	0
sea07x.dat	4	G/MDB	90	26	852.1	60.2	0.31	0.25	0.17	0.26	0	0	0
sea07x.dat	5	G/MDB	66	5	965.8	55.3	0.24	0.22	0.16	0.45	0.25	0	0
sea07x.dat	6	G/MDB	80	14	1041.6	59.2	0.25	0.23	0.25	0.5	0.24	0.27	0
sea07x.dat	7	G/MDB	80	15	1186.2	59.8	0.25	0.23	0.25	0.5	0.24	0.27	0.58



sea10x.dat	1	DB/MHR	80	5	66.7	8.8							
sea10x.dat	2	DB/MHR	61	14	65.2	9.7							
sea10x.dat	3	DB/MHR	80	6	63.8	8							
sea10x.dat	4	DB/MHR	80	6	63.2	7.9							
sea10x.dat	5	DB/MHR	80	6	62.7	7.9							
sea10x.dat	6	DB/MHR	80	6	61.7	7.9							
sea10x.dat	7	DB/MHR	87	7	60.8	7.9							
sea10x.dat	1	DB/MHR	71	28	36	2.6							
sea10x.dat	2	DB/MHR	71	29	37.1	2.8							
sea10x.dat	3	DB/MHR	71	29	37.4	2.8							
sea10x.dat	4	DB/MHR	71	30	38	3.2							
sea10x.dat	5	DB/MHR	71	30	39.1	3.4							
sea10x.dat	6	DB/MHR	71	31	39.9	3.7							
sea10x.dat	7	DB/MHR	71	31	41.5	4							
sea10x.dat	1	HR/MDB	86	26	10.1	58.7							
sea10x.dat	2	HR/MDB	86	26	10	58.7							
sea10x.dat	3	HR/MDB	61	15	9.6	62.9							
sea10x.dat	4	HR/MDB	61	15	9.3	61.3							
sea10x.dat	5	HR/MDB	88	6	9.2	57.9							
sea10x.dat	6	HR/MDB	88	6	9.2	58.8							
sea10x.dat	7	HR/MDB	88	7	9.1	58.3							
sea10x.dat	1	HR/MDB	69	13	2.3	49.5							
sea10x.dat	2	HR/MDB	69	14	2.7	49.4							
sea10x.dat	3	HR/MDB	69	15	2.7	52							
sea10x.dat	4	HR/MDB	69	15	2.9	52							
sea10x.dat	5	HR/MDB	69	16	3.3	51.8							
sea10x.dat	6	HR/MDB	69	17	3.6	50.9							
sea10x.dat	7	HR/MDB	69	18	3.8	49.9							
sea10x.dat	1	G/MDB	89	2	1411.9	57.3	0.73	0	0	0	0	0	0
sea10x.dat	2	G/MDB	89	3	1398.3	56.3	0.73	0.73	0	0	0	0	0
sea10x.dat	3	G/MDB	64	5	1325.3	58	0.72	0.7	0.7	0	0	0	0
sea10x.dat	4	G/MDB	64	6	1302.1	58.1	0.72	0.7	0.7	0.67	0	0	0
sea10x.dat	5	G/MDB	80	6	1292.5	62.7	0.67	0.7	0.66	0.7	0.7	0	0
sea10x.dat	6	G/MDB	80	6	1255.5	61.7	0.55	0.67	0.7	0.66	0.7	0.7	0
sea10x.dat	7	G/MDB	74	8	1217.9	53	0.6	0.7	0.49	0.72	0.66	0.73	0.69
sea10x.dat	1	G/MDB	81	19	62.4	48.1	0.04	0	0	0	0	0	0
sea10x.dat	2	G/MDB	89	23	206.8	54.2	0.15	0.13	0	0	0	0	0
sea10x.dat	3	G/MDB	89	23	249.7	53.7	0.23	0.15	0.13	0	0	0	0
sea10x.dat	4	G/MDB	88	14	294.8	56.9	0.16	0.21	0.17	0.16	0	0	0
sea10x.dat	5	G/MDB	88	15	304.8	57.2	0.16	0.21	0.17	0.16	0.21	0	0
sea10x.dat	6	G/MDB	88	16	305.6	56.6	0.16	0.21	0.17	0.16	0.21	0.19	0
sea10x.dat	7	G/MDB	75	31	352.3	46.8	0.31	0.19	0.35	0.22	0.2	0.3	0.27



wes01x.dat	1	DB/MHR	73	22	77.1	15							
wes01x.dat	2	DB/MHR	73	3	76.8	15.1							
wes01x.dat	3	DB/MHR	73	4	76.5	15.1							
wes01x.dat	4	DB/MHR	73	4	76.1	14.7							
wes01x.dat	5	DB/MHR	73	5	75.7	14.5							
wes01x.dat	6	DB/MHR	73	6	75.4	14.4							
wes01x.dat	7	DB/MHR	73	7	74.9	14.1							
wes01x.dat	1	DB/MHR	77	19	36.8	2.6							
wes01x.dat	2	DB/MHR	70	10	39.4	2.3							
wes01x.dat	3	DB/MHR	70	10	40.3	2.4							
wes01x.dat	4	DB/MHR	77	21	42.8	3.4							
wes01x.dat	5	DB/MHR	77	22	43.9	3.4							
wes01x.dat	6	DB/MHR	77	22	44.9	3.7							
wes01x.dat	7	DB/MHR	77	23	46.2	3.9							
wes01x.dat	1	HR/MDB	90	5	16.1	75.5							
wes01x.dat	2	HR/MDB	90	6	16	75.6							
wes01x.dat	3	HR/MDB	90	7	15.7	75.2							
wes01x.dat	4	HR/MDB	90	7	15.3	75.4							
wes01x.dat	5	HR/MDB	90	8	15.1	75.1							
wes01x.dat	6	HR/MDB	80	14	14.5	71.4							
wes01x.dat	7	HR/MDB	90	25	14.3	74.5							
wes01x.dat	1	HR/MDB	70	9	2.1	39.8							
wes01x.dat	2	HR/MDB	85	22	2.3	40.2							
wes01x.dat	3	HR/MDB	70	10	2.4	40.3							
wes01x.dat	4	HR/MDB	70	11	3.1	43.2							
wes01x.dat	5	HR/MDB	77	22	3.4	43.9							
wes01x.dat	6	HR/MDB	77	22	3.7	44.9							
wes01x.dat	7	HR/MDB	77	23	3.9	46.2							
wes01x.dat	1	G/MDB	76	30	1615.4	52.7	0.74	0	0	0	0	0	0
wes01x.dat	2	G/MDB	78	31	1582.9	52.1	0.73	0.71	0	0	0	0	0
wes01x.dat	3	G/MDB	78	31	1560.5	50.7	0.7	0.73	0.71	0	0	0	0
wes01x.dat	4	G/MDB	71	30	1517.9	57.2	0.72	0.72	0.71	0.65	0	0	0
wes01x.dat	5	G/MDB	87	31	1491.8	59.1	0.69	0.7	0.71	0.65	0.69	0	0
wes01x.dat	6	G/MDB	87	31	1468.9	59.9	0.63	0.69	0.7	0.71	0.65	0.69	0
wes01x.dat	7	G/MDB	61	24	1416.3	55.3	0.72	0.65	0.72	0.6	0.66	0.73	0.69
wes01x.dat	1	G/MDB	83	23	346.5	68.7	0.16	0	0	0	0	0	0
wes01x.dat	2	G/MDB	86	9	467.9	69.2	0.21	0.26	0	0	0	0	0
wes01x.dat	3	G/MDB	86	9	520.4	69.8	0.32	0.21	0.26	0	0	0	0
wes01x.dat	4	G/MDB	83	7	563.4	66	0.3	0.24	0.32	0.3	0	0	0
wes01x.dat	5	G/MDB	61	13	564.6	69.2	0.19	0.35	0.31	0.3	0.26	0	0
wes01x.dat	6	G/MDB	83	9	599.4	67.5	0.3	0.24	0.32	0.3	0.42	0.26	0
wes01x.dat	7	G/MDB	83	11	609.1	67.7	0.24	0.32	0.3	0.42	0.26	0.35	0.27



wes03x.dat	1	DB/MHR	84	28	80.3	16.9							
wes03x.dat	2	DB/MHR	84	28	79.1	16.5							
wes03x.dat	3	DB/MHR	73	16	78.6	13.9							
wes03x.dat	4	DB/MHR	73	16	78	13.9							
wes03x.dat	5	DB/MHR	73	16	78	13.9							
wes03x.dat	6	DB/MHR	73	16	78	14							
wes03x.dat	7	DB/MHR	73	16	77.8	14							
wes03x.dat	1	DB/MHR	80	3	41	3.3							
wes03x.dat	2	DB/MHR	80	3	48.6	5.9							
wes03x.dat	3	DB/MHR	80	4	51.7	6.1							
wes03x.dat	4	DB/MHR	68	4	54.3	4.9							
wes03x.dat	5	DB/MHR	68	5	55.2	4.9							
wes03x.dat	6	DB/MHR	68	6	56	4.9							
wes03x.dat	7	DB/MHR	68	7	57.2	5.4							
wes03x.dat	1	HR/MDB	80	30	18	78.1							
wes03x.dat	2	HR/MDB	80	30	17.3	77.6							
wes03x.dat	3	HR/MDB	80	30	16.6	77.1							
wes03x.dat	4	HR/MDB	80	30	16.3	76.7							
wes03x.dat	5	HR/MDB	80	30	16.1	76							
wes03x.dat	6	HR/MDB	80	31	15.9	75.9							
wes03x.dat	7	HR/MDB	80	31	15.5	75.5							
wes03x.dat	1	HR/MDB	68	1	2.9	46.3							
wes03x.dat	2	HR/MDB	68	2	3.3	48.9							
wes03x.dat	3	HR/MDB	86	3	4.4	53							
wes03x.dat	4	HR/MDB	68	4	4.9	54.3							
wes03x.dat	5	HR/MDB	68	5	4.9	55.2							
wes03x.dat	6	HR/MDB	68	6	4.9	56							
wes03x.dat	7	HR/MDB	68	7	5.4	57.2							
wes03x.dat	1	G/MDB	74	31	2318.2	73	0.75	0	0	0	0	0	0
wes03x.dat	2	G/MDB	72	24	2234.8	68.7	0.73	0.76	0	0	0	0	0
wes03x.dat	3	G/MDB	72	25	2167.3	69.7	0.73	0.76	0.67	0	0	0	0
wes03x.dat	4	G/MDB	72	26	2106	68.9	0.73	0.76	0.67	0.63	0	0	0
wes03x.dat	5	G/MDB	72	27	2066.1	68.7	0.73	0.76	0.67	0.63	0.63	0	0
wes03x.dat	6	G/MDB	72	28	2021.6	69	0.73	0.76	0.67	0.63	0.63	0.59	0
wes03x.dat	7	G/MDB	71	26	1967.1	67.4	0.71	0.72	0.61	0.67	0.66	0.62	0.61
wes03x.dat	1	G/MDB	84	23	620.7	68.5	0.21	0	0	0	0	0	0
wes03x.dat	2	G/MDB	80	2	763.5	60	0.26	0.31	0	0	0	0	0
wes03x.dat	3	G/MDB	88	7	790.5	71.4	0.29	0.31	0.27	0	0	0	0
wes03x.dat	4	G/MDB	88	7	869.2	72.6	0.41	0.29	0.31	0.27	0	0	0
wes03x.dat	5	G/MDB	87	6	903.8	68.5	0.31	0.49	0.3	0.31	0.27	0	0
wes03x.dat	6	G/MDB	87	6	898.8	69.8	0.33	0.31	0.49	0.3	0.31	0.27	0
wes03x.dat	7	G/MDB	87	7	937.7	70.1	0.33	0.31	0.49	0.3	0.31	0.27	0.43



wes07x.dat	1	DB/MHR	83	26	87.3	17.5							
wes07x.dat	2	DB/MHR	83	26	87.2	17.6							
wes07x.dat	3	DB/MHR	83	26	87	18.2							
wes07x.dat	4	DB/MHR	83	26	86.6	18.3							
wes07x.dat	5	DB/MHR	83	26	86.2	18.5							
wes07x.dat	6	DB/MHR	83	26	85.7	18.6							
wes07x.dat	7	DB/MHR	83	26	85.6	18.6							
wes07x.dat	1	DB/MHR	68	8	74.2	16							
wes07x.dat	2	DB/MHR	65	21	74.9	15.5							
wes07x.dat	3	DB/MHR	68	8	75.1	16.3							
wes07x.dat	4	DB/MHR	68	8	75.5	16.3							
wes07x.dat	5	DB/MHR	65	22	75.9	15.5							
wes07x.dat	6	DB/MHR	65	22	76.1	15.5							
wes07x.dat	7	DB/MHR	65	22	76.3	15.5							
wes07x.dat	1	HR/MDB	84	17	19.6	81.8							
wes07x.dat	2	HR/MDB	90	29	19.4	83.2							
wes07x.dat	3	HR/MDB	90	30	19.3	83.6							
wes07x.dat	4	HR/MDB	87	7	19.2	83.6							
wes07x.dat	5	HR/MDB	87	7	19.2	83.5							
wes07x.dat	6	HR/MDB	87	8	19.2	83.6							
wes07x.dat	7	HR/MDB	87	7	19.1	83.1							
wes07x.dat	1	HR/MDB	74	14	12.8	81.6							
wes07x.dat	2	HR/MDB	74	14	13.3	79.5							
wes07x.dat	3	HR/MDB	74	15	13.9	79.4							
wes07x.dat	4	HR/MDB	74	16	14.2	79.9							
wes07x.dat	5	HR/MDB	74	17	14.4	79.4							
wes07x.dat	6	HR/MDB	74	17	14.6	79.2							
wes07x.dat	7	HR/MDB	74	17	14.8	79.7							
wes07x.dat	1	G/MDB	65	6	2539.5	81.3	0.71	0	0	0	0	0	0
wes07x.dat	2	G/MDB	65	4	2414.9	81.1	0.69	0.66	0	0	0	0	0
wes07x.dat	3	G/MDB	71	14	2374	81.6	0.67	0.68	0.66	0	0	0	0
wes07x.dat	4	G/MDB	65	6	2381.9	81.1	0.69	0.66	0.6	0.71	0	0	0
wes07x.dat	5	G/MDB	65	6	2358.9	80.8	0.63	0.69	0.66	0.6	0.71	0	0
wes07x.dat	6	G/MDB	65	6	2359.5	80.6	0.66	0.63	0.69	0.66	0.6	0.71	0
wes07x.dat	7	G/MDB	65	7	2333.3	80.7	0.66	0.63	0.69	0.66	0.6	0.71	0.61
wes07x.dat	1	G/MDB	85	23	711.7	74.9	0.2	0	0	0	0	0	0
wes07x.dat	2	G/MDB	90	14	905.7	77.8	0.24	0.27	0	0	0	0	0
wes07x.dat	3	G/MDB	90	15	1038.4	78.9	0.24	0.27	0.37	0	0	0	0
wes07x.dat	4	G/MDB	68	8	1115.8	75.5	0.34	0.31	0.31	0.29	0	0	0
wes07x.dat	5	G/MDB	70	23	1211.6	81.7	0.31	0.37	0.33	0.37	0.34	0	0
wes07x.dat	6	G/MDB	62	13	1257.2	78.9	0.38	0.25	0.36	0.38	0.35	0.4	0
wes07x.dat	7	G/MDB	62	12	1311.2	79.2	0.38	0.48	0.38	0.25	0.36	0.38	0.35



wes10x.dat	1	DB/MHR	90	4	83.8	19.5							
wes10x.dat	2	DB/MHR	90	4	83.7	19.1							
wes10x.dat	3	DB/MHR	90	5	83.6	18.8							
wes10x.dat	4	DB/MHR	90	6	83.4	17.8							
wes10x.dat	5	DB/MHR	90	7	83.2	17.5							
wes10x.dat	6	DB/MHR	90	8	83.2	17.4							
wes10x.dat	7	DB/MHR	90	8	83	17.5							
wes10x.dat	1	DB/MHR	89	20	60.9	6.4							
wes10x.dat	2	DB/MHR	89	21	61.1	6.8							
wes10x.dat	3	DB/MHR	89	22	63	7.6							
wes10x.dat	4	DB/MHR	89	23	65.4	8.2							
wes10x.dat	5	DB/MHR	68	30	65.3	9.1							
wes10x.dat	6	DB/MHR	68	31	66.1	9.2							
wes10x.dat	7	DB/MHR	68	31	67	9.9							
wes10x.dat	1	HR/MDB	90	4	19.5	83.8							
wes10x.dat	2	HR/MDB	90	4	19.1	83.7							
wes10x.dat	3	HR/MDB	90	12	19.1	82.8							
wes10x.dat	4	HR/MDB	90	12	18.9	82.2							
wes10x.dat	5	HR/MDB	90	13	18.6	81.9							
wes10x.dat	6	HR/MDB	90	14	18.4	81.7							
wes10x.dat	7	HR/MDB	90	15	18.2	81.7							
wes10x.dat	1	HR/MDB	89	20	6.4	60.9							
wes10x.dat	2	HR/MDB	89	21	6.8	61.1							
wes10x.dat	3	HR/MDB	89	22	7.6	63							
wes10x.dat	4	HR/MDB	77	17	7.8	66.3							
wes10x.dat	5	HR/MDB	77	18	8.1	66.6							
wes10x.dat	6	HR/MDB	77	18	8.6	67.3							
wes10x.dat	7	HR/MDB	77	19	9	67.4							
wes10x.dat	1	G/MDB	72	8	1957.5	74.5	0.73	0	0	0	0	0	0
wes10x.dat	2	G/MDB	88	12	1886.3	74	0.72	0.72	0	0	0	0	0
wes10x.dat	3	G/MDB	77	16	1846.5	66.6	0.72	0.72	0.73	0	0	0	0
wes10x.dat	4	G/MDB	77	17	1821.8	66.3	0.72	0.72	0.73	0.69	0	0	0
wes10x.dat	5	G/MDB	77	18	1814.6	66.6	0.72	0.72	0.73	0.69	0.71	0	0
wes10x.dat	6	G/MDB	77	19	1781.8	66.9	0.72	0.72	0.73	0.69	0.71	0.65	0
wes10x.dat	7	G/MDB	77	20	1756.6	67.3	0.72	0.72	0.73	0.69	0.71	0.65	0.65
wes10x.dat	1	G/MDB	61	18	479.6	77.7	0.19	0	0	0	0	0	0
wes10x.dat	2	G/MDB	64	29	530.3	72.8	0.21	0.24	0	0	0	0	0
wes10x.dat	3	G/MDB	64	30	579.4	72.2	0.21	0.24	0.29	0	0	0	0
wes10x.dat	4	G/MDB	64	31	592.8	72.2	0.21	0.24	0.29	0.27	0	0	0
wes10x.dat	5	G/MDB	64	31	622.5	73.3	0.31	0.21	0.24	0.29	0.27	0	0
wes10x.dat	6	G/MDB	64	31	736.5	74.1	0.55	0.31	0.21	0.24	0.29	0.27	0
wes10x.dat	7	G/MDB	69	30	758.9	76.7	0.28	0.36	0.34	0.36	0.29	0.29	0.31



Location	Hot Daily Range °F	Cold Daily Range °F	Average Daily Range °F	SD Average Daily Range °F
alb01	22.0	18.0	22.3	6.6
alb03	22.0	11.0	26.4	7.8
alb07	30.0	6.0	25.3	4.7
alb10	29.0	16.0	25.4	7.0
atl01	9.0	26.0	17.8	7.8
atl03	27.0	11.0	20.7	7.6
atl07	26.0	10.0	17.2	4.2
atl10	17.0	14.0	19.5	6.7
bal01	21.0	14.0	15.6	7.0
bal03	22.0	6.0	18.6	8.5
bal07	20.0	9.0	18.8	5.4
bal10	17.0	19.0	20.1	7.5
cha01	14.0	21.0	19.8	8.0
cha03	26.0	3.0	20.8	7.0
cha07	16.0	6.0	16.1	3.7
cha10	17.0	19.0	20.1	6.7
chi01	23.0	22.0	15.1	7.0
chi03	33.0	25.0	16.3	8.0
chi07	15.0	11.0	19.8	6.2
chi10	17.0	15.0	20.0	7.9
hou01	13.0	11.0	18.9	8.8
hou03	16.0	12.0	20.2	7.9
hou07	22.0	6.0	18.3	4.1
hou10	17.0	24.0	21.2	7.4
kan01	20.0	11.0	17.2	7.4
kan03	10.0	20.0	19.4	8.9
kan07	25.0	8.0	18.9	5.0
kan10	32.0	22.0	20.5	7.7
los01	27.0	8.0	16.0	7.2
los03	25.0	16.0	13.1	5.4
los07	29.0	12.0	11.1	2.8
los10	25.0	14.0	13.7	6.7
mad01	14.0	9.0	16.1	7.4
mad03	36.0	30.0	17.9	8.5
mad07	21.0	13.0	22.2	6.1
mad10	16.0	11.0	20.9	8.3
mia01	11.0	21.0	15.1	5.8
mia03	7.0	21.0	13.9	5.4
mia07	8.0	5.0	11.5	2.8
mia10	14.0	15.0	11.7	3.6
new01	13.0	11.0	10.9	5.2
new03	17.0	5.0	13.1	5.9
new07	19.0	6.0	13.9	4.1
new10	16.0	9.0	12.8	4.6

Location	Hot Daily Range °F	Cold Daily Range °F	Average Daily Range °F	SD Average Daily Range °F
san01	6.0	8.0	11.8	4.9
san03	20.0	5.0	12.9	5.3
san07	35.0	10.0	15.9	5.9
san10	35.0	16.0	16.0	6.9
sea01	10.0	11.0	8.6	3.8
sea03	24.0	9.0	12.8	5.4
sea07	29.0	10.0	18.8	6.3
sea10	29.0	13.0	12.8	5.4
wes01	12.0	14.0	16.7	6.2
wes03	13.0	20.0	15.6	5.8
wes07	14.0	12.0	13.4	3.1
wes10	12.0	16.0	12.4	4.4
<b>Average</b>	19.9	13.3	17.0	6.2

#### Extreme and Average Daily Ranges

## Appendix C

### Regression and Time Series Overview

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This section is intended to serve as a brief overview of some important concepts concerning multiple regression and time series analyses used for this project. More detailed information can be found in Draper [1981], McClave [1988] and Wei [1990].

#### **Multiple Regression Analysis**

The general multiple regression model consists of a deterministic portion plus a random component and is of the form

$$y = \mathbf{b}_o + \mathbf{b}_1 x_1 + \mathbf{b}_2 x_2 + \dots + \mathbf{b}_k x_k + \mathbf{e}$$

The dependent or response variable is  $y$ . The deterministic component consists of  $\mathbf{b}_o, \mathbf{b}_1, \dots, \mathbf{b}_k$ ; the unknown parameters and  $x_1, x_2, \dots, x_k$ ; the independent or predictor variables. The predictor variables may include first order or higher order terms as well as cross terms. The error component is  $\mathbf{e}$ . The general model may also be expressed in matrix form as follows:

$$\mathbf{Y} = \mathbf{X}\mathbf{b} + \mathbf{e}$$

where:  $\mathbf{Y} = (n \times 1)$  vector of the dependent variable

$\mathbf{X} = (n \times k)$  matrix

$\mathbf{b} = (k \times 1)$  vector of the unknown parameters

$\mathbf{e} = (n \times 1)$  vector of errors

$n$  = number of observations

$k$  = number of parameters (including the constant) in the model

Minimizing the sum of the squares of the errors,  $\varepsilon' \varepsilon$ , leads to the normal equations:

$$(X'X)b = X'Y$$

The solution to the normal equation is:

$$b = (X'X)^{-1} X'Y$$

where  $b$  is the least squares estimate of  $\beta$

The errors have a mean of zero,  $E(\varepsilon) = 0$ . If the errors are assumed to be uncorrelated or independent in a probabilistic sense then  $\text{Var}(\varepsilon) = I\sigma^2$ , where  $I$  is the identity matrix. This implies that the variance of the errors is constant.

### **Evaluating the Significance of the Individual Estimated $b$ Parameters**

If the errors are assumed to be normally distributed then the  $t$  statistic may be used to test the significance of  $\beta_i$ . The hypotheses used are:

$$\text{null hypothesis} \quad - H_0: b_i = 0$$

$$\text{alternative hypothesis} \quad - H_a: b_i \neq 0$$

$$t\text{-statistic} \quad - t = \frac{b_i}{s_{b_i}}$$

If  $|t| > |t_\alpha|$  then the null hypothesis is rejected. The  $\alpha$  chosen determines the significance level of the test. An  $\alpha$  of 0.05 is normally used.

### **Checking the Usefulness of the Model**

Conducting individual  $t$  tests on each  $b_i$  in the regression model is not a good way to test whether the model is a useful tool for the prediction of  $y$ . In other words, the individual  $t$  values of the  $b_i$  estimates may not be significant, however the overall model may be useful.

This may occur when the independent variables are correlated (multicollinearity). A test to evaluate the overall model is the F statistic. The hypotheses used are:

$$\text{null hypothesis} \quad - H_0: b_1 = b_2 = \dots = b_k = 0$$

$$\text{alternative hypothesis} - H_a: \text{at least one } b_i \neq 0$$

$$\text{F-statistic} \quad - F = \frac{MS_{\text{model}}}{MS_{\text{error}}}$$

If  $F > F_\alpha$  with ( $k$  numerator degrees of freedom and  $[n - (k + 1)]$  denominator degrees of freedom) then the null hypothesis is rejected. As with the  $t$  test an  $\alpha$  of 0.05 is typically used. The fact that a model is useful does not mean it is the best model. A better or more useful model may exist. This is discussed in the stepwise procedure section later.

Another commonly used measure of the usefulness of a model is the coefficient of determination defined as follows:

$$R^2 = \frac{\text{Explained Variability}}{\text{Total Variability}}$$

This measure is somewhat qualitative. A coefficient of determination equal to zero implies a complete lack of fit while a value of one implies a perfect fit.

### **Residual Analysis**

Finally, before any regression model can be deemed adequate the residuals or errors must be examined for any behavior that violates the assumptions made previously. Namely, the residuals must behave as independent, identically normally distributed (i.i.d.) random variables. To test these assumptions the following plots are examined:

- normal probability plot of the residuals
- residuals versus the predictor variables

- residuals versus the predicted or fitted dependent variables
- residuals versus time, if appropriate.

The plots are inspected for any patterns. Typical examples of unsatisfactory residuals behavior include non-constant variance, indicating a transformation of the dependent variable is needed. A curvature seen in the residuals plots indicates the need to add higher-order or cross product terms to the model. The residual plots should appear random and be approximately evenly distributed both above and below the x-axis. If the standardized residual are used in the plots any outliers, observations greater than three or four standard deviations from the mean, should be checked to determine why they are so different from the other observations.

### **Use of the Model Outside of the Development Region**

The use of the model to predict the dependent variable  $y$  using independent variables that are outside those that were used to develop the model is not recommended. The behavior of model when used in this manner cannot be predicted.

### **Selecting the “Best” Regression Equation**

Given a set of appropriate independent variables how does one determine which ones to include in the final regression equation? There are several procedures available to determine the “best” regression equation given a set of predictors. Such methods include all possible regressions, backward and forward regressions and stepwise regressions. The stepwise is the one selected for this project.

### **Stepwise Regression Procedure**

Once the dependent variable is chosen a set of appropriate independent variables must be selected. The stepwise procedure cannot do this therefore it is important that only

independent variables be chosen that are reasonably expected to affect the dependent variable. Consequently, the possibility exists that important terms may be left out. However, since the number of independent variables was severely constrained due to the requirements of this project this is not a factor. Given a set of  $k$  independent variables,  $x_1, x_2, \dots, x_k$  and a dependent variable,  $y$ , where the independent variables may include first order and higher order terms as well as cross terms. The general procedure is as follows, although the exact algorithm used in MINITAB [1996] is not known.

**STEP 1** - All possible models one-variable models of the form  $E(y) = b_o + b_1x_i$  are fit to the data. The t or corresponding F test is used to evaluate the null hypothesis ( $H_0: \beta_1 = 0$ ) against the alternative hypothesis ( $H_a: \beta_1 \neq 0$ ) at the desired significance level. This is equivalent to selecting the predictor variable that is most highly correlated to the dependent variable. This is the best one-variable predictor of  $y$ .

**STEP 2** - The remaining  $(k - 1)$  independent variables are fit to the two-variable model of the form  $E(y) = b_o + b_1x_1 + b_2x_i$ . The partial F values are calculated to evaluate the null hypothesis  $H_0: \beta_2 = 0$ . The variable having the highest partial F value is retained. This is equivalent to choosing the remaining independent variable with the highest partial correlation to the dependent variable. At this point the t value for  $\beta_1$  should be recalculated to ensure that it is still significant. In addition, the overall model must be still be significant. This step is repeated until no other dependent variables can be found that yield significant  $t$  values (at the specified  $\alpha$  level) in the presence of those variables already in the model.

After the stepwise procedure is complete it is still necessary perform a residual analysis to ensure that higher order of cross product terms are not needed. If it is found that

extra terms are needed these should be added and an additional stepwise regression should be done.

## Time Series Analysis

A time series analysis differs from a regression analysis in that the observations are always ordered in time and tend to be dependent on each other. A typical time series is represented symbolically as:

$$\dots Y_{t-2}, Y_{t-1}, Y_t, Y_{t+1}, Y_{t+2}, \dots$$

where:  $Y_t$  is the observation at time,  $t$

### Stationarity

To estimate parameters such as the mean, variance or covariance from a single realization of a time series it must be at least weakly stationary. A weakly stationary time series has the following properties:

- the mean,  $m$  of the series is constant for all time
- the variance,  $s^2$  or  $g(0)$  of the series is constant for all time
- the covariance,  $g(k)$  of the series is function of the lag,  $k$  only and not time

An example of a stationary time series is a white noise process,  $a_t$ . A white noise process is defined as:

- all  $a_t$  are i.i.d. random variables (usually assumed to be normally distributed)
- $E(a_t) = 0$  for all  $t$
- $\text{Var}(a_t) = s^2$  for all  $t$
- $\text{Cov}(a_t) = 0$  by definition.

If a series does not exhibit these properties then some transformation is needed to make the series stationary. For example to remove a linear trend from the non-stationary series,  $Y_t$  the first difference may be formed to produce a stationary series,  $W_t$ :

$$W_t = (Y_t - Y_{t-1}) = Y_t(1-B)$$

where:  $B$  is the backward shift operator defined by the property  $BY_t = Y_{t-1}$

If the non-stationary series,  $Y_t$  contains a deterministic seasonal component with a period,  $s$ , it may be removed using a seasonal difference to form the stationary series,  $W_t$ :

$$W_t = (Y_t - Y_{t-s}) = Y_t(1-B^s)$$

where:  $s$  is the period.

### General Seasonal ARIMA Model

The general form of the multiplicative seasonal ARIMA model of orders  $(p,d,q)x(P,D,Q)$  with period  $s$ , for the seasonal time series,  $Y_t$  is:

$$\Phi(B^s)f(B)(1-B^s)^D(1-B)^d Y_t = d + \Theta(B^s)q(B)a_t$$

where:  $f(B)$  and  $q(B)$  are non-seasonal AR and MA operators in  $B$  of orders  $p$  and  $q$  respectively

$\Phi(B^s)$  and  $\Theta(B^s)$  are seasonal AR and MA operators in  $B^s$  of orders  $P$  and  $Q$

$d$  is a constant

$a_t$  is a white noise process

If  $D > 0$  or  $d > 0$  than the differenced series,  $W_t$  is stationary:

$$W_t = (1-B^s)^D(1-B)^d Y_t$$

If the process does not exhibit a seasonal component the general model reduces to an ARIMA model of order  $(p,d,q)$ :

$$\mathbf{f}(B)(1-B)^d Y_t = \mathbf{d} + \mathbf{q}(B)a_t$$

Finally, for the stationary process the ARIMA reduces to the ARMA mode of order (p,q):

$$\mathbf{f}(B)Y_t = \mathbf{d} + \mathbf{q}(B)a_t$$

The humidity ratio time series investigated in this project were determined to be an ARMA(1,0) or simply an AR(1) model:

$$\mathbf{f}_1 Y_t = \mathbf{d} + a_t$$

### **Model Identification**

There are two basic tools used to aid in time series model identification. They are the sample autocorrelation function (ACF) and the sample partial autocorrelation function (PACF). The ACF summarizes the correlations among values in a series at various lags, k. The PACF is equal to the partial correlation between  $Y_t$  and  $Y_{t-k}$  after adjusting (removing the influence) for the intermediate values  $Y_{t-1}, Y_{t-2}, \dots, Y_{t-k+1}$ . The theoretical behavior of the ACF and PACF for stationary processed is summarized below. In practice

Process	ACF	PACF
AR(p)	Tails off as exponential decay or damped sinusoid	Cuts off after lag p
MA(q)	Cuts off after lag q	Tails off as exponential decay or damped sinusoid
ARMA(p,q)	Tails off after lag (q-p)	Tails off after lag (p-q)

the theoretical ACF and PACF, only the sample values are known, therefore values within 2 standard deviations (approximately  $\pm \frac{2}{\sqrt{t}}$ ) are considered to be zero.

### **Checking the Model for Adequacy**

The estimated parameters for the ARMA model are checked to see if they differ significantly from zero using the same procedure as the one used for the estimated parameters in the multiple regression model. Finally, the residuals must behave as white

noise, in other words, they should have a mean of zero, be stationary, uncorrelated and normally distributed. If the residuals are correlated they may be modeled as a normal time series and the residual model may be added to the original time series model and then reevaluated. In addition, many model selection criteria are available to aid when several models appear to adequately represent the data.

## Appendix D

### Regression and Time Series Supporting Plots

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Regression Parameter Estimates, Analysis of Variance and Residual Plots

Time Series Residual Plots

**Equation 3.5**

$$\bar{T}_{\text{min,day}} = -4.32 + 0.923\bar{T}_{\text{mon}} - 0.317\text{Range} + 19.8\text{Skew Index}$$

S = 3.057 °F    R<sup>2</sup> = 98.6%

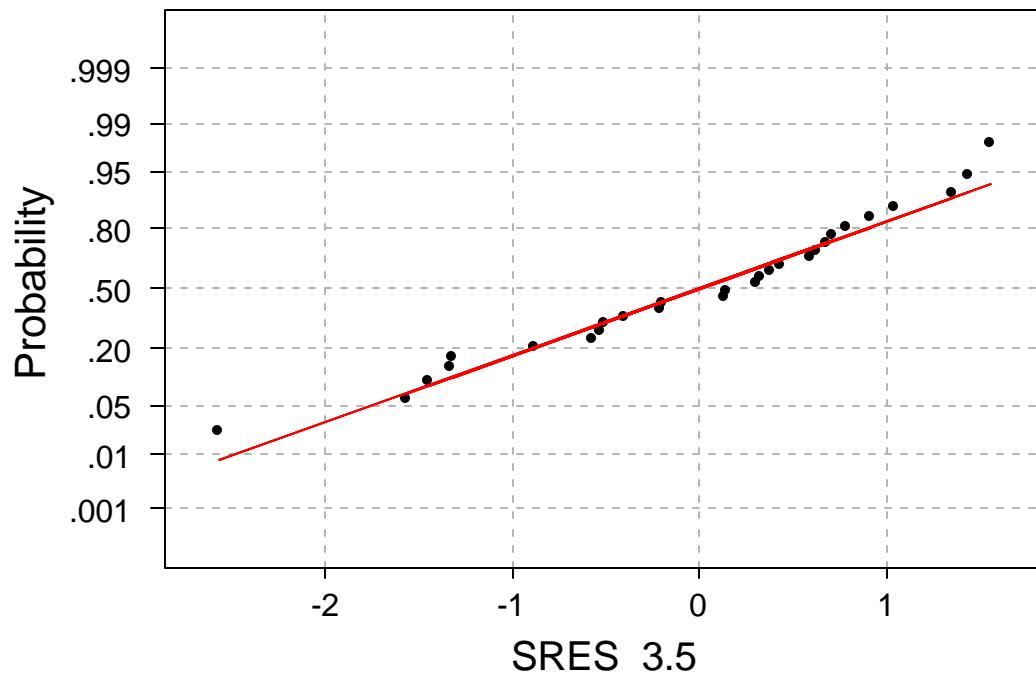
**Parameter Estimates**

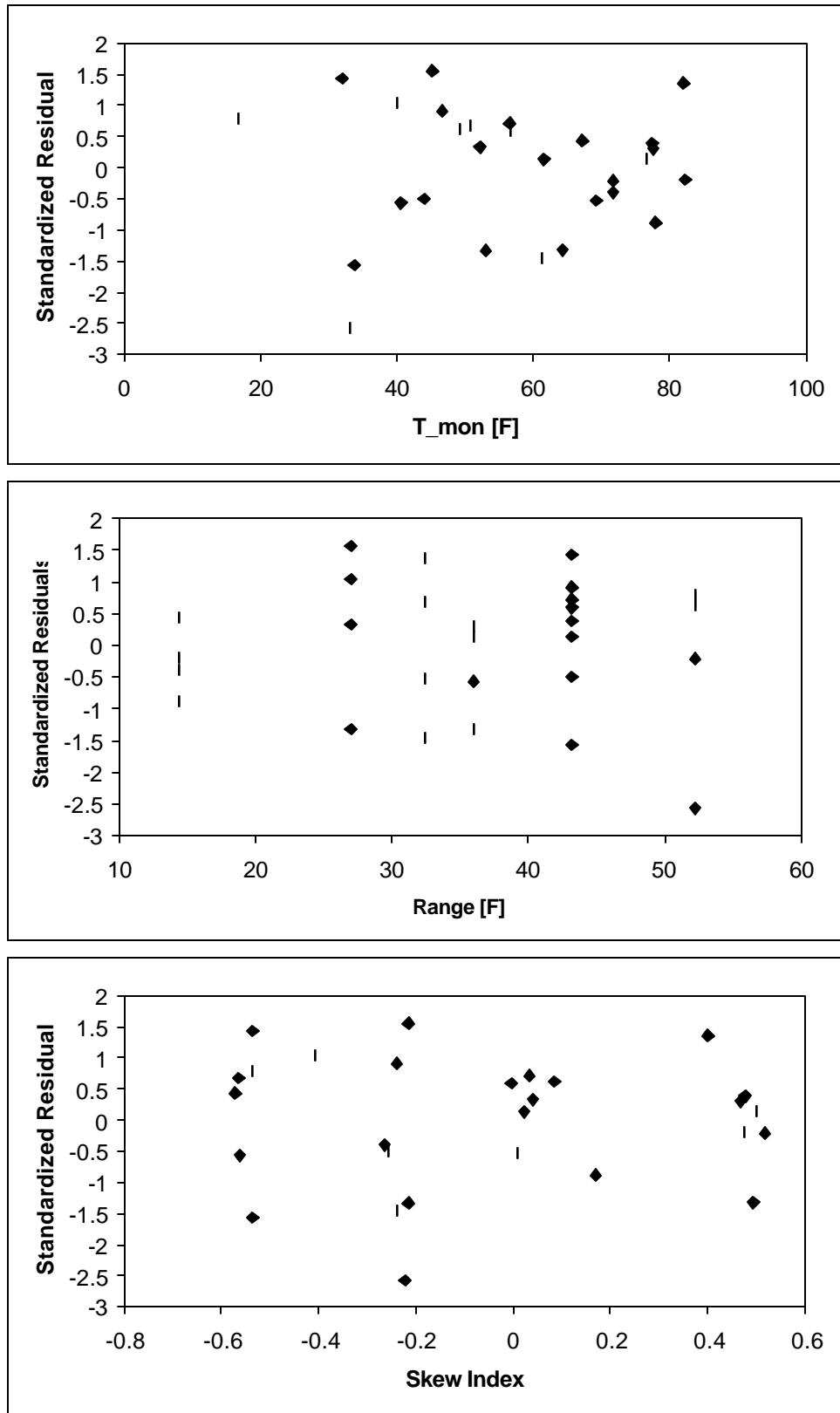
Predictor	Coeff	StDev	t-value	p-value
Constant	-4.325	6.467	-0.67	0.510
$\bar{T}_{\text{mon}}$	0.92342	0.07417	12.45	0.000
Range	-0.31693	0.07177	-4.42	0.000
Skew Index	19.802	2.995	6.61	0.000

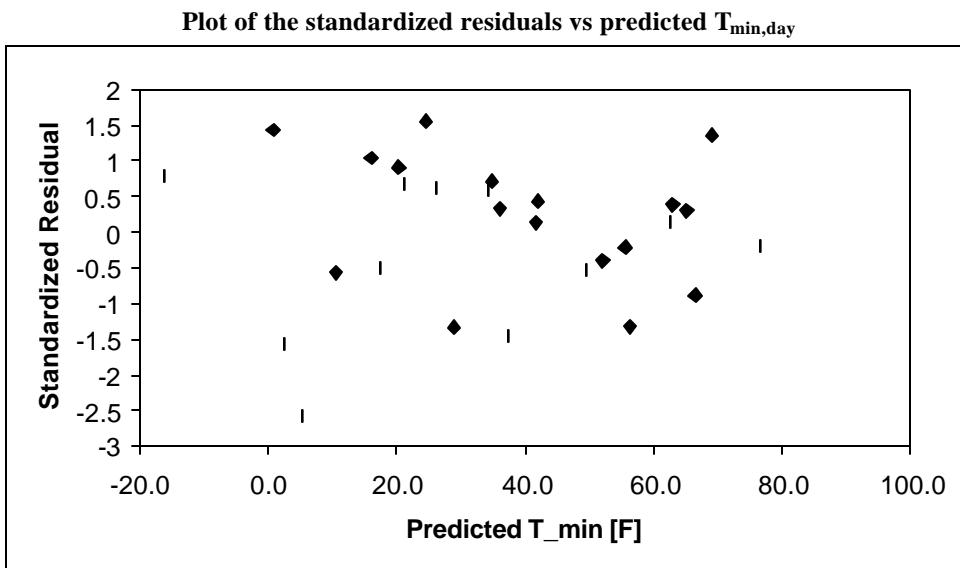
**Analysis of Variance**

Source	DF	SS	MS	F-statistic	p-value
Regression	3	15393.5	5131.2	549.17	0.000
Error	24	224.2	9.3		
Total	27	15617.7			

Source	DF	Seq SS
$\bar{T}_{\text{mon}}$	1	14982.6
Range	1	2.3
Skew Index	1	408.5

**Normal probability plot of the standardized residuals**

**Plots of the standardized residuals vs predictors**



### Equation 3.6

$$\bar{T}_{\max, \text{day}} = 17.1 + 0.651\bar{T}_{\text{mon}} + 0.796\sigma_{\text{yr}} - 0.00190z + 24.7\bar{K}_t$$

$S = 2.647 \text{ }^{\circ}\text{F}$        $R^2 = 95.7\%$

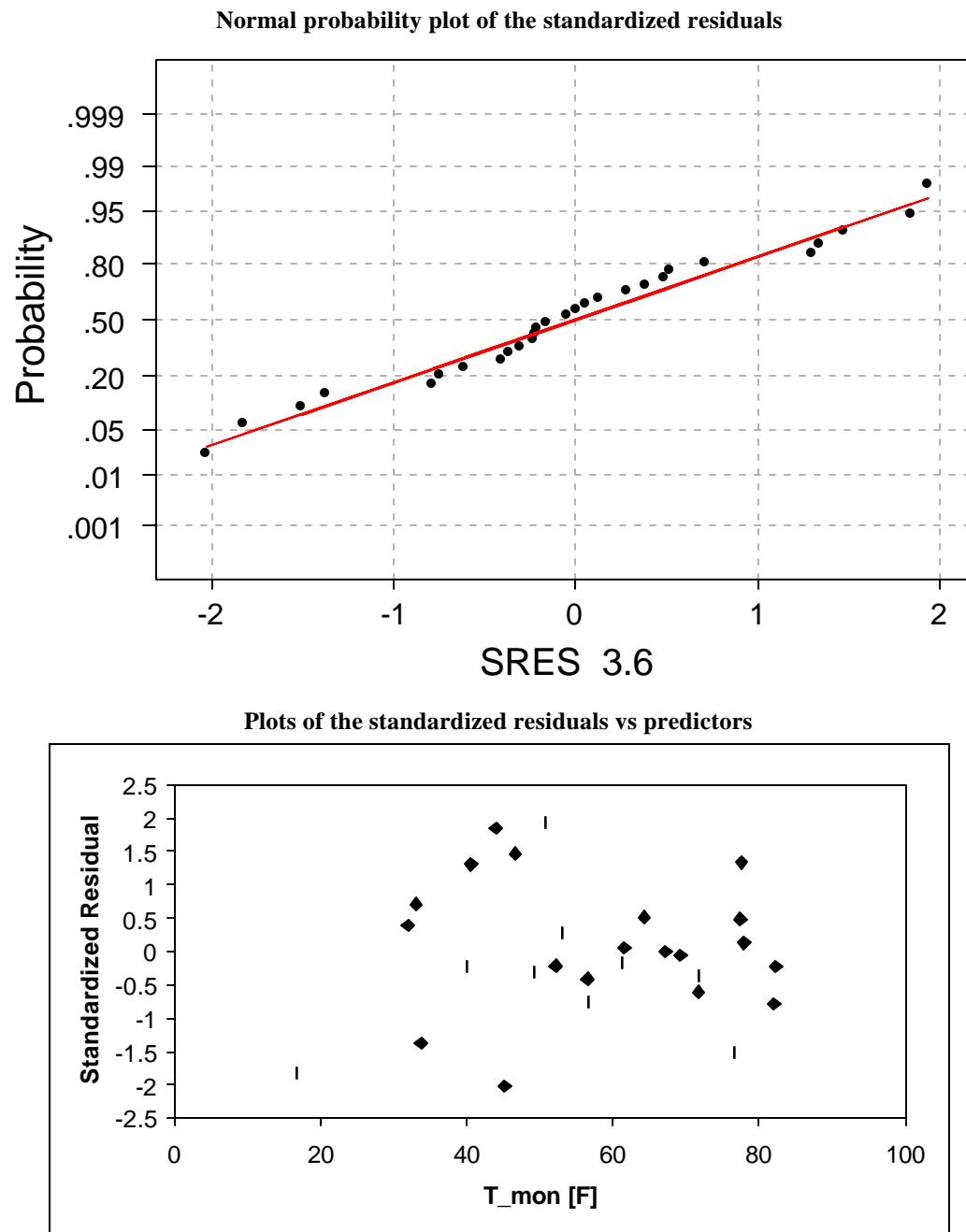
#### Parameter Estimates

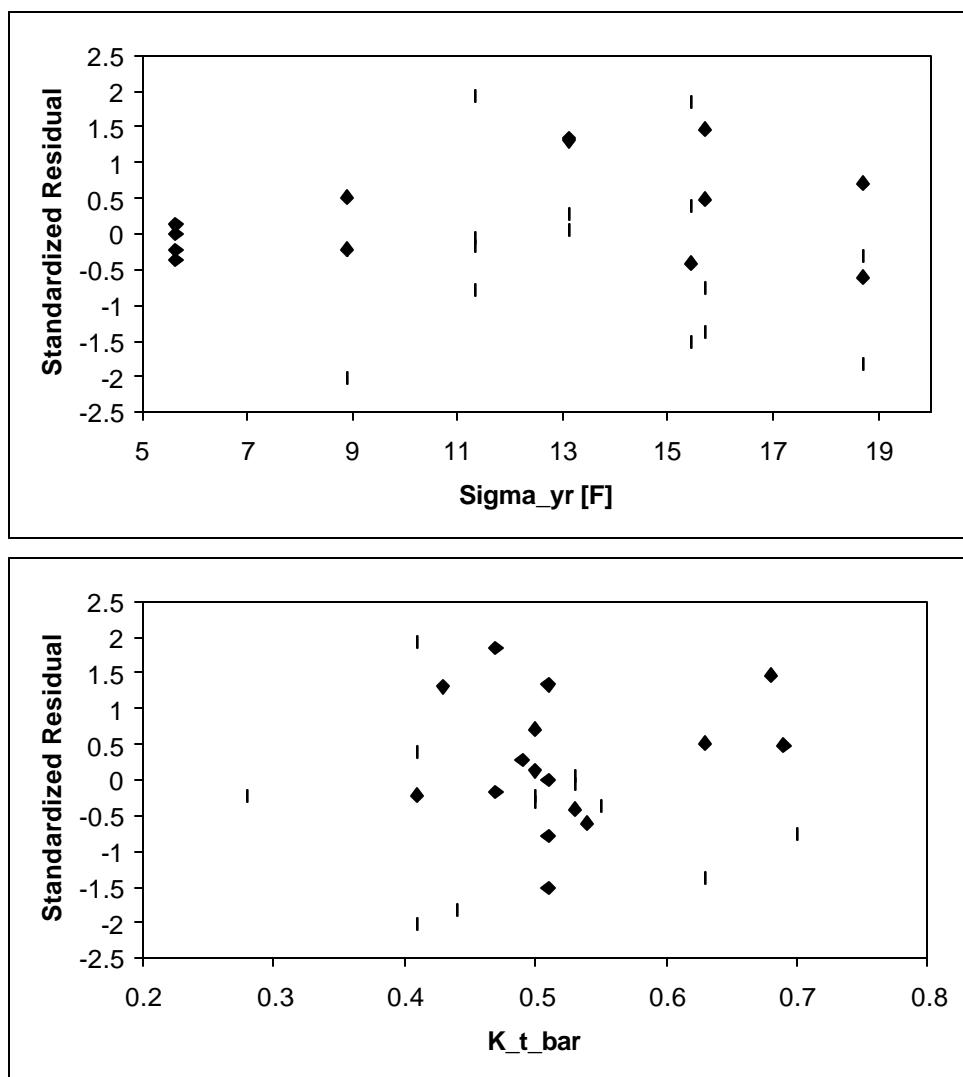
Predictor	Coef	StDev	t-value	p-value
Constant	17.145	4.136	4.15	0.000
$\bar{T}_{\text{mon}}$	0.65094	0.04304	15.12	0.000
$\sigma_{\text{yr}}$	0.7958	0.1519	5.24	0.000
$z$	-0.0019002	0.0004999	-3.80	0.001
$\bar{K}_t$	24.66	10.25	2.41	0.025

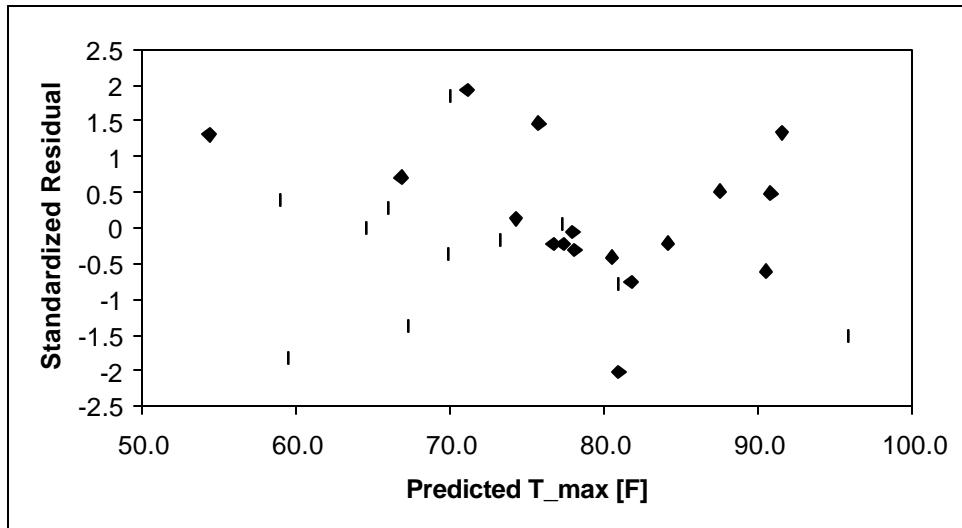
#### Analysis of Variance

Source	DF	SS	MS	F-statistic	p-value
Regression	4	3614.92	903.73	128.95	0.000
Error	23	161.19	7.01		
Total	27	3776.11			

Source	DF	Seq SS
$\bar{T}_{\text{mon}}$	1	3313.30
$\sigma_{\text{yr}}$	1	194.83
$z$	1	66.19
$\bar{K}_t$	1	40.60





**Plot of the standardized residuals vs predicted  $T_{\max, \text{day}}$** **Equation 3.8**

$$A = 1.0 + 35.6 \bar{K}_t - 0.000902 \mathbf{v}_{mon}^3$$

$S = 2.627 \text{ } ^\circ\text{F}$      $R^2 = 66.4\%$

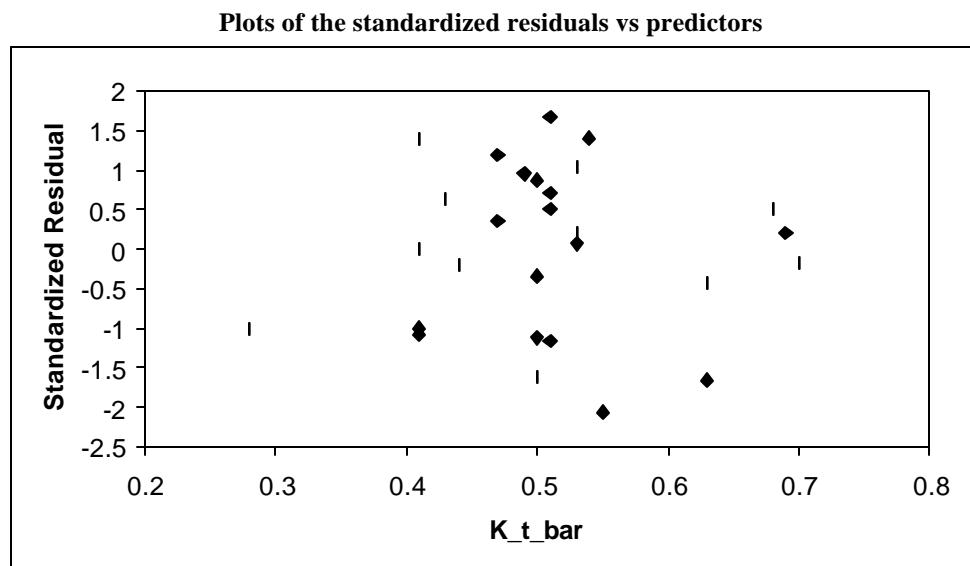
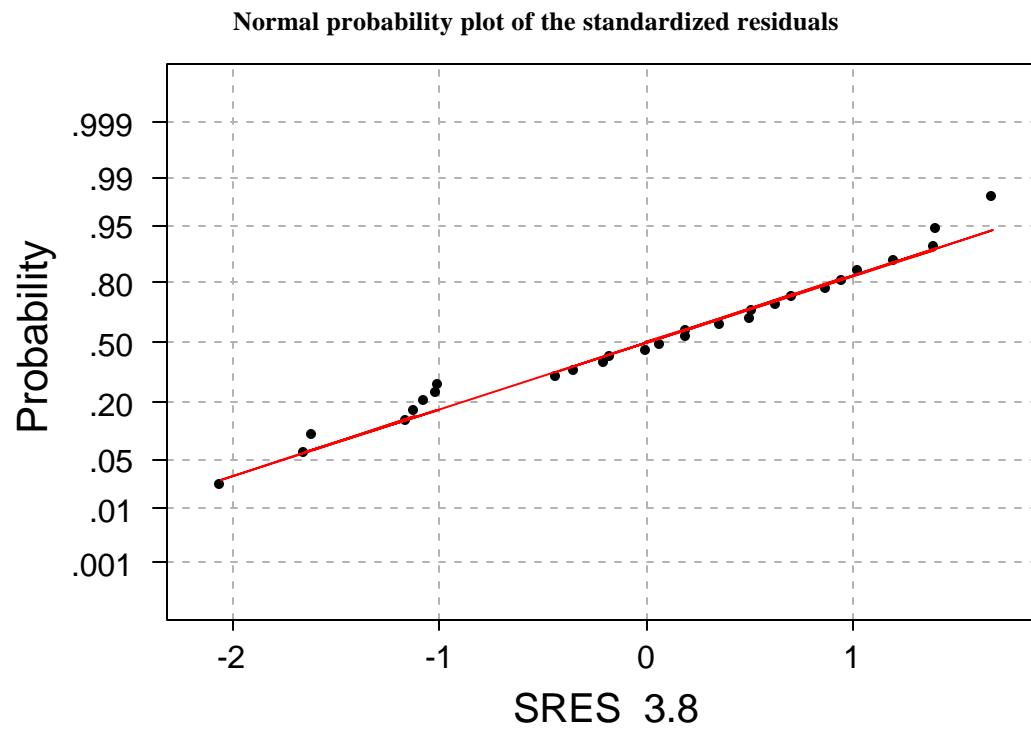
Parameter Estimates

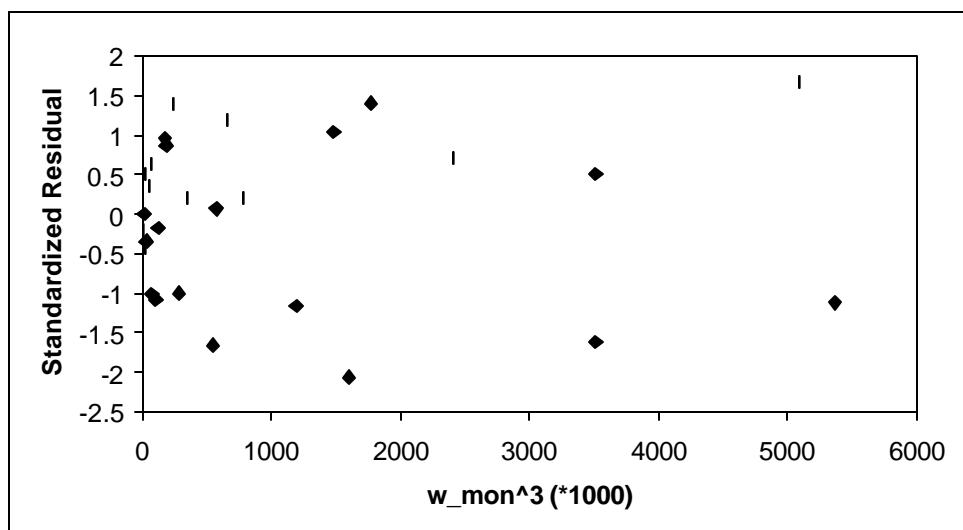
Predictor	Coef	StDev	t-value	p-value
Constant	0.997	2.797	0.36	0.724
$\bar{K}_t$	35.591	5.391	6.60	0.000
$\mathbf{v}_{mon}^3$	-0.0009022	0.0003293	-2.74	0.011

Analysis of Variance

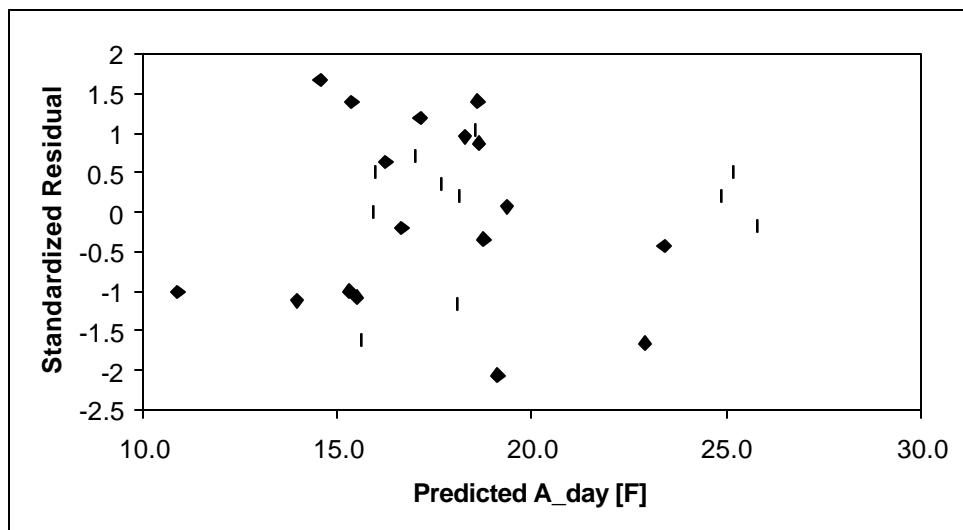
Source	DF	SS	MS	F-statistic	p-value
Regression	2	340.55	170.28	24.67	0.000
Error	25	172.54	6.90		
Total	27	513.09			

Source	DF	Seq SS
$\bar{K}_t$	1	288.76
$\mathbf{v}_{mon}^3$	1	51.79





Plot of the standardized residuals vs predicted daily Amplitude



**Equation 3.8a**

$$A = 3.88 + 0.170\bar{T}_{mon} - 3.68s_{yr} + 1.61Range - 0.368f + 22.8\bar{K}_t - 0.00764\bar{T}_{mon}\mathbf{V}_{mon}$$

S = 0.8751 °F    R<sup>2</sup> = 96.9%

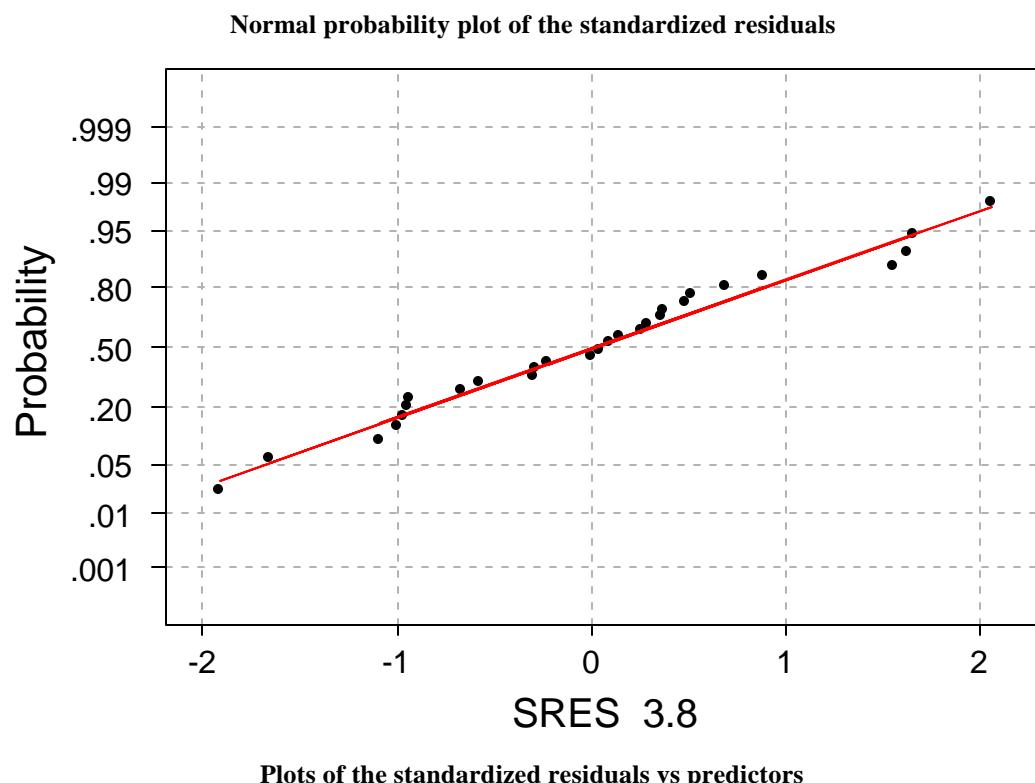
Parameter Estimates

Predictor	Coef	StDev	t-value	p-value
Constant	3.881	1.900	2.04	0.054
$\bar{T}_{mon}$	0.16979	0.03043	5.58	0.000
$s_{yr}$	-3.6795	0.7431	-4.95	0.000
Range	1.6097	0.2728	5.90	0.000
$f$	-0.36818	0.04527	-8.13	0.000
$\bar{K}_t$	22.792	2.571	8.87	0.000
$\bar{T}_{mon}\mathbf{V}_{mon}$	-0.007640	0.001167	-6.55	0.000

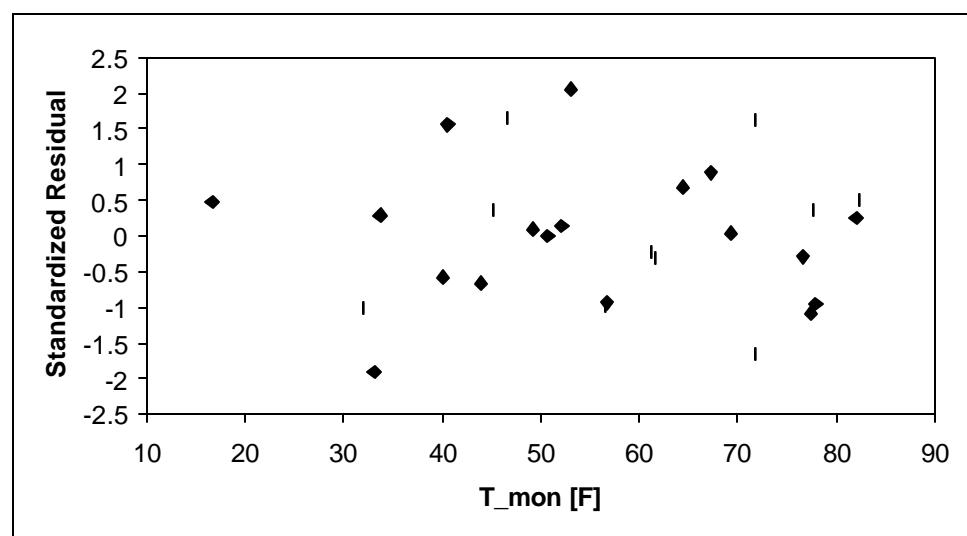
Analysis of Variance

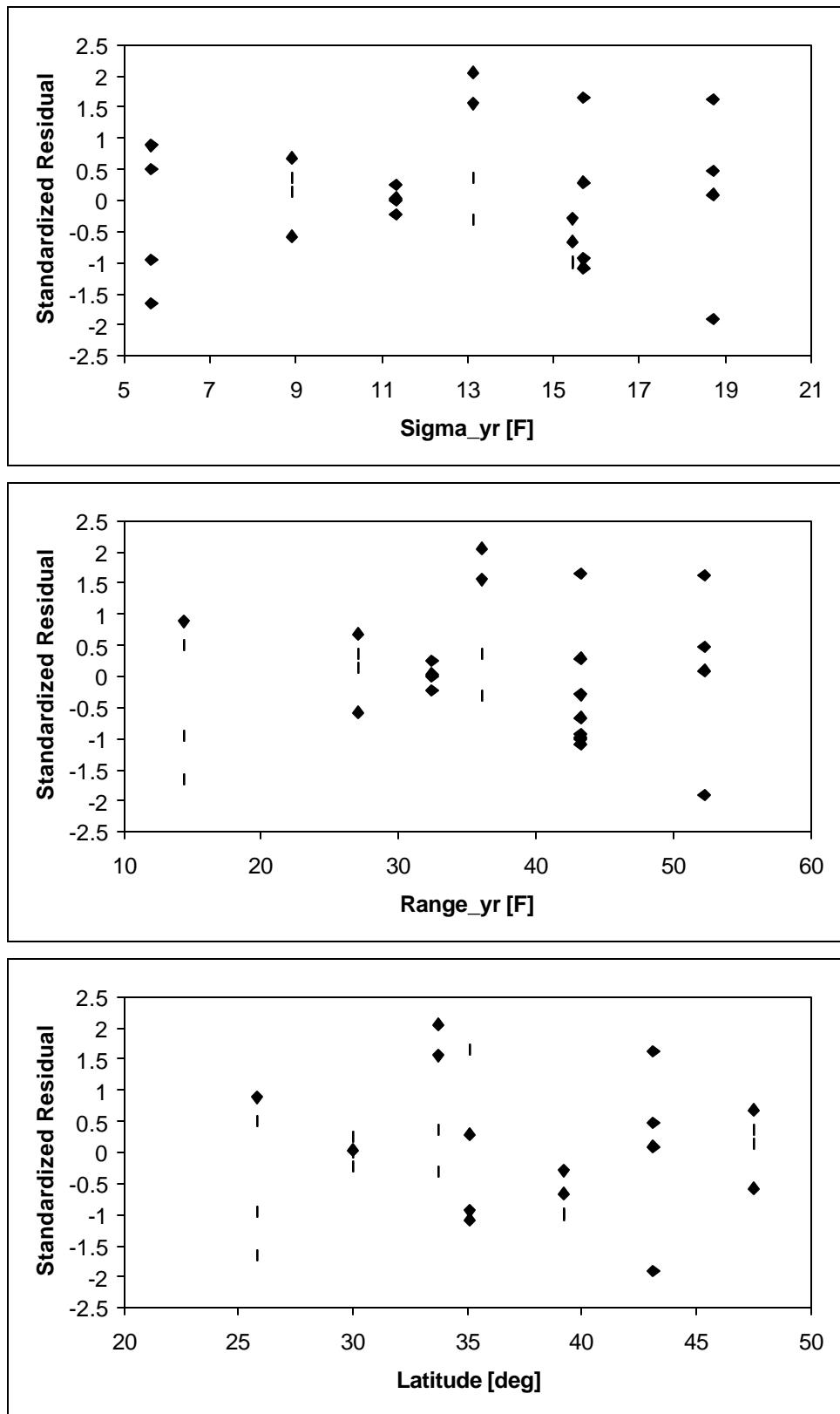
Source	DF	SS	MS	F-statistic	p-value
Regression	6	497.013	82.836	108.17	0.000
Error	21	16.081	0.766		
Total	27	513.094			

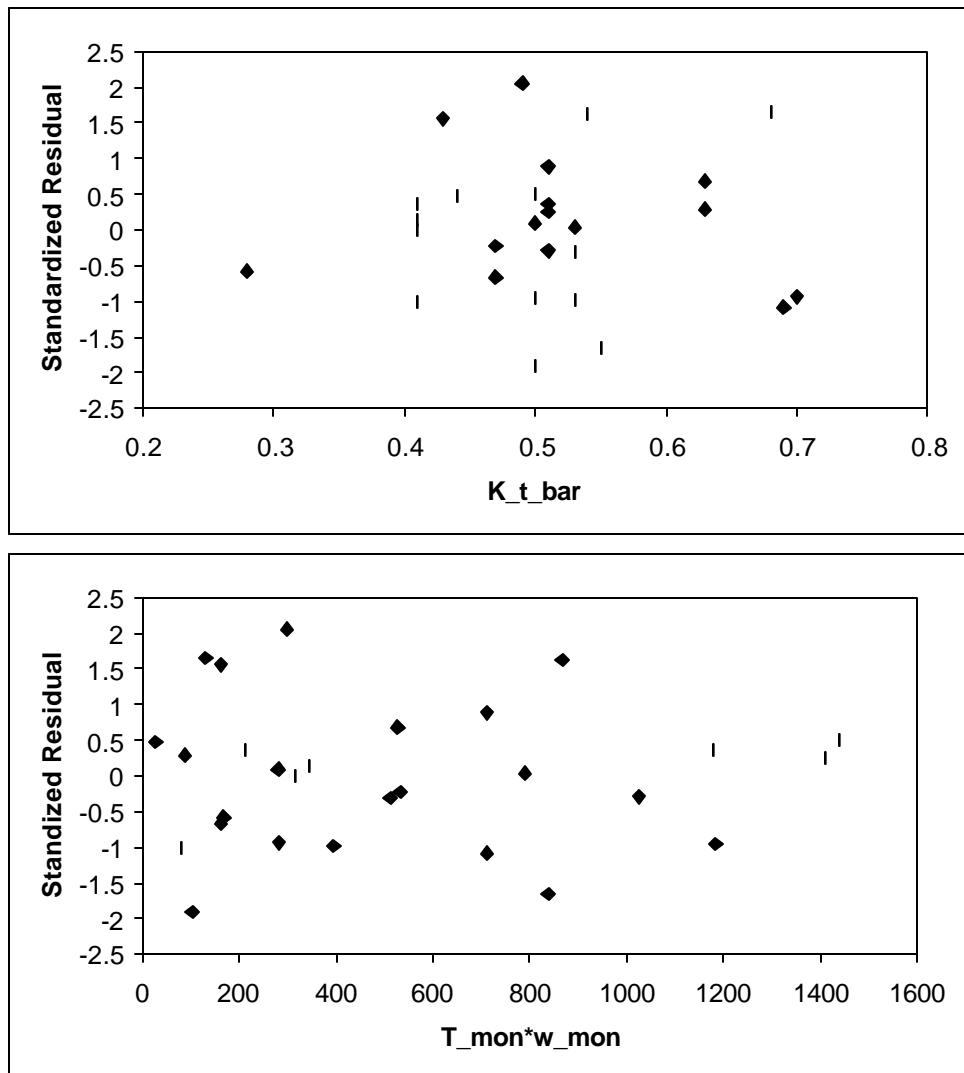
Source	DF	Seq SS
$\bar{T}_{mon}$	1	0.213
$s_{yr}$	1	278.055
Range	1	4.391
$f$	1	39.039
$\bar{K}_t$	1	142.481
$\bar{T}_{mon}\mathbf{V}_{mon}$	1	32.835



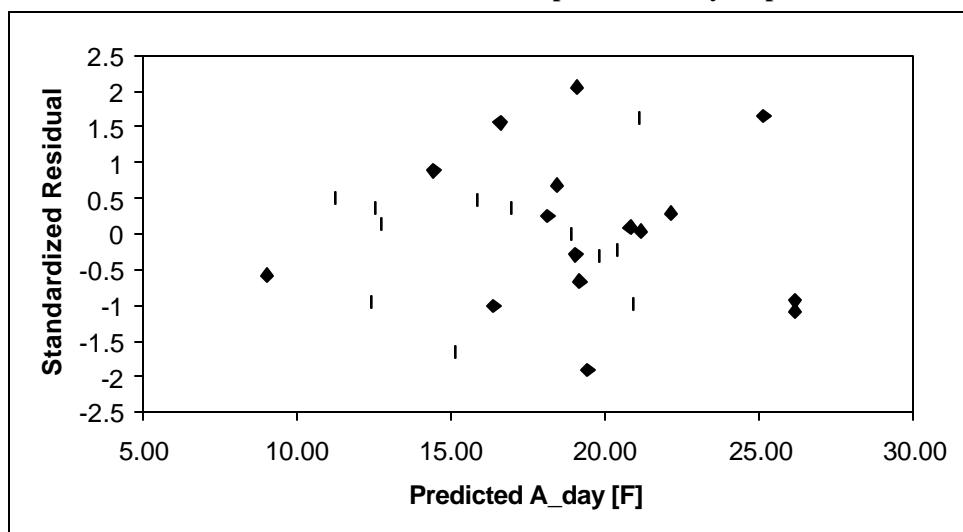
Plots of the standardized residuals vs predictors







Plot of the standardized residuals vs predicted daily amplitude



**Equation 3.9**

$$SD_{Range} = -30.8 - 0.000655z + 8.26\bar{K}_t + 0.756Long - 0.00395Long^2 - 0.0196V_{mon}^2$$

$S = 0.5860 \text{ } ^\circ\text{F}$     $R^2 = 89.9\%$

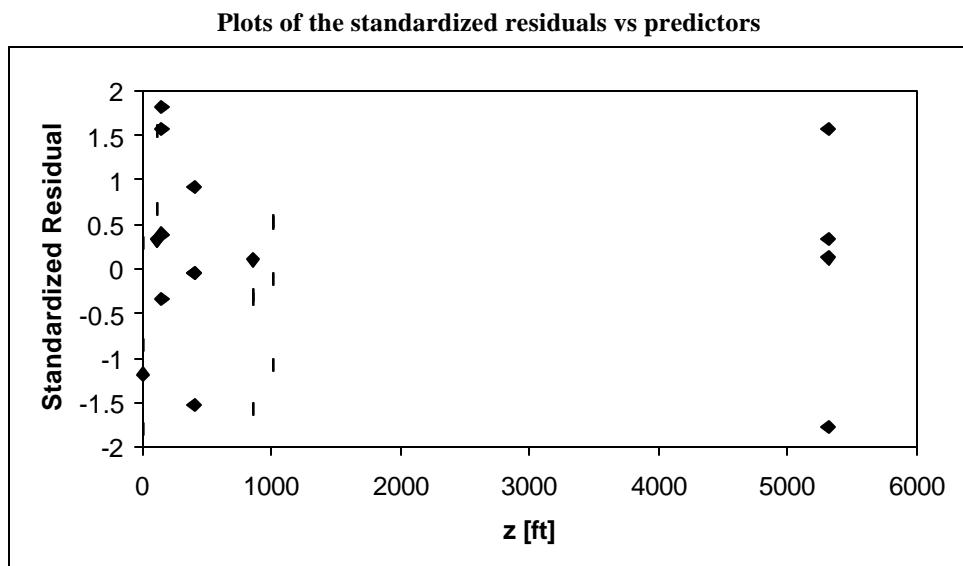
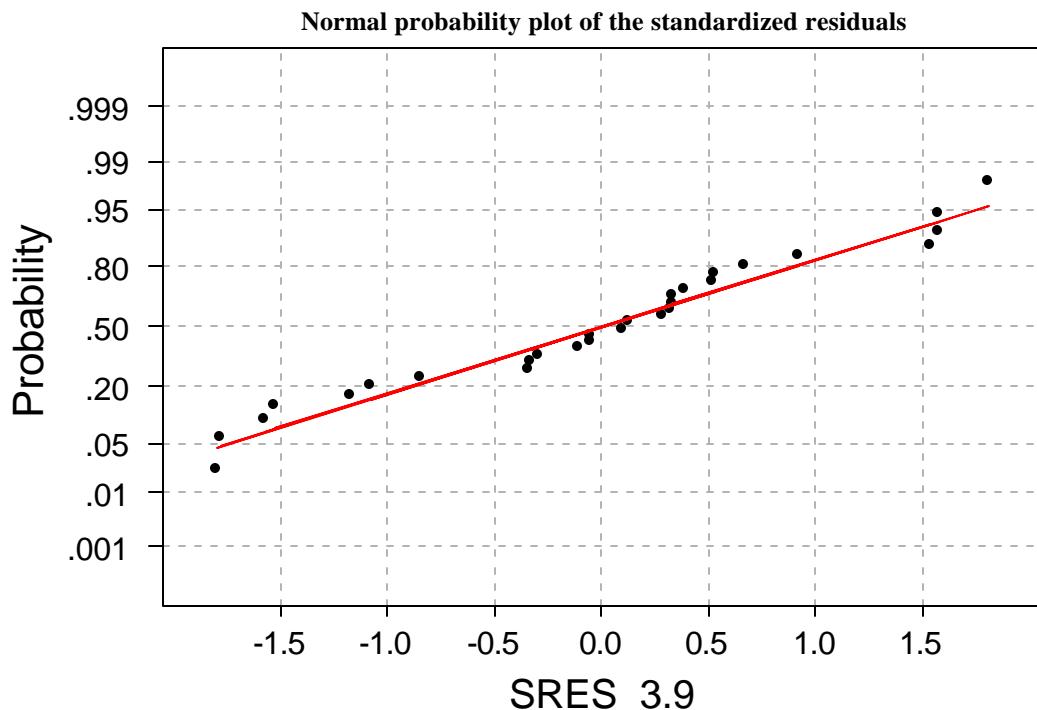
Parameter Estimates

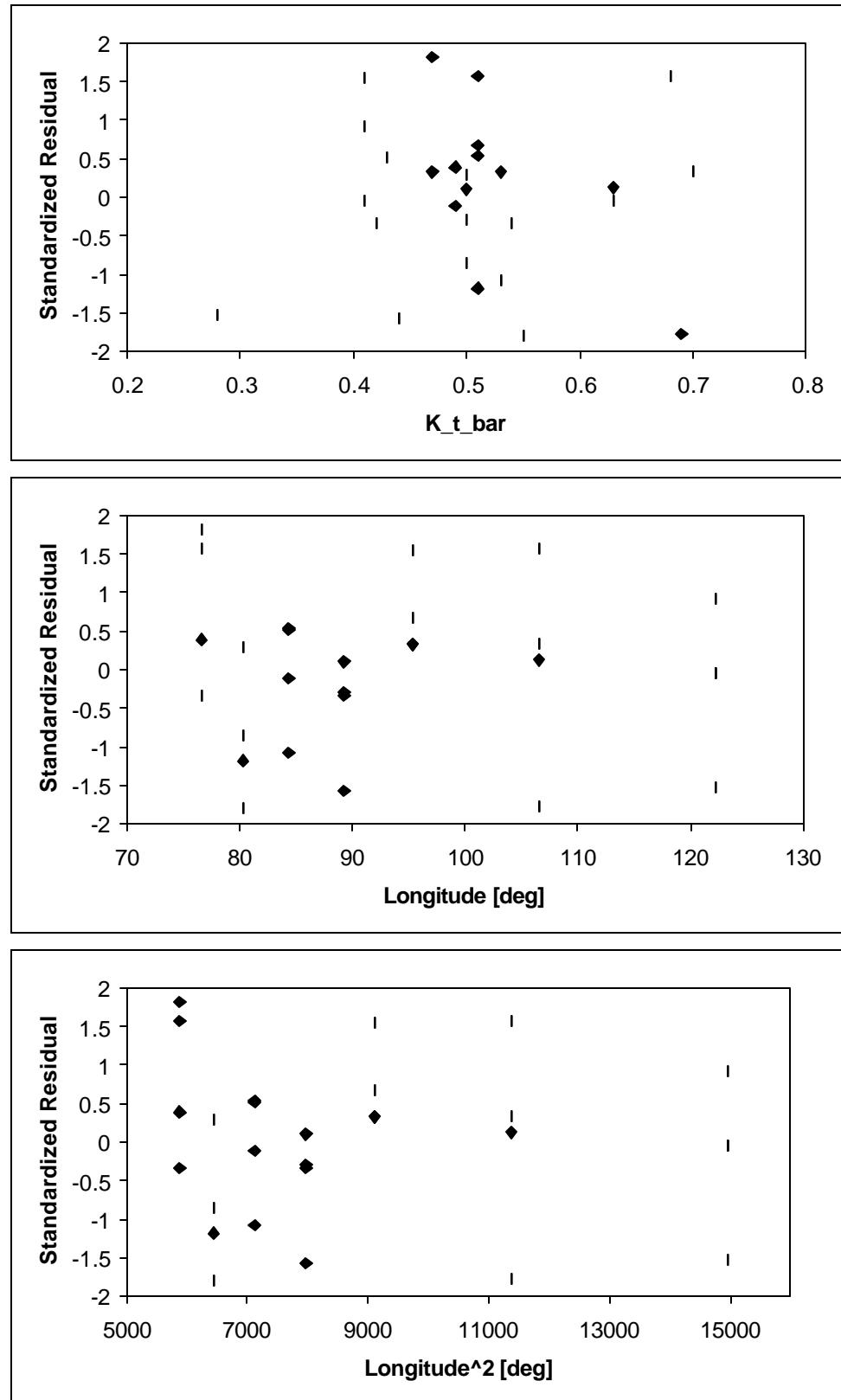
Predictor	Coef	StDev	t-value	p-value
Constant	-30.806	6.464	-4.77	0.000
$z$	-0.0006547	0.0001223	-5.36	0.000
$\bar{K}_t$	8.256	1.992	4.14	0.000
Long	0.7565	0.1310	5.77	0.000
$Long^2$	-0.0039464	0.0006515	-6.06	0.000
$V_{mon}^2$	-0.019572	0.001512	-12.95	0.000

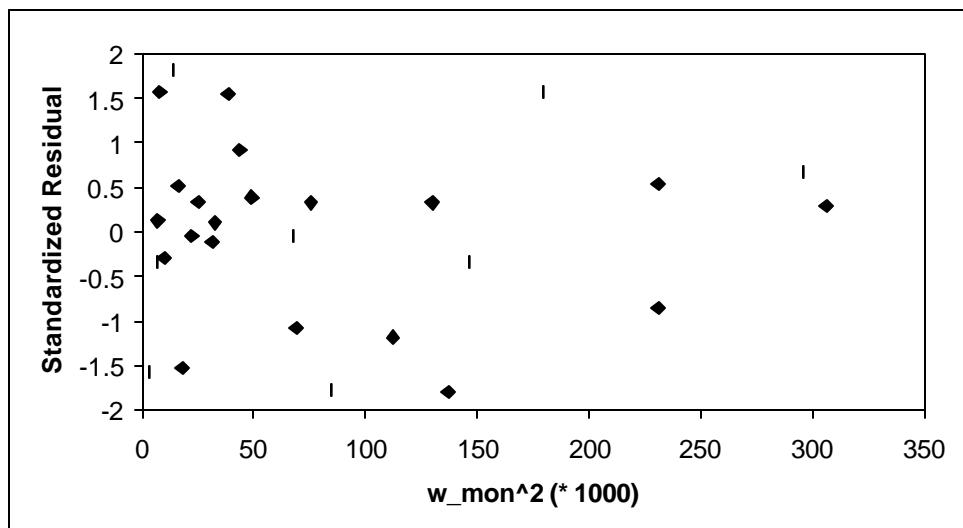
Analysis of Variance

Source	DF	SS	MS	F-statistic	p-value
Regression	5	67.415	13.483	39.26	0.000
Error	22	7.555	0.343		
Total	7	74.970			

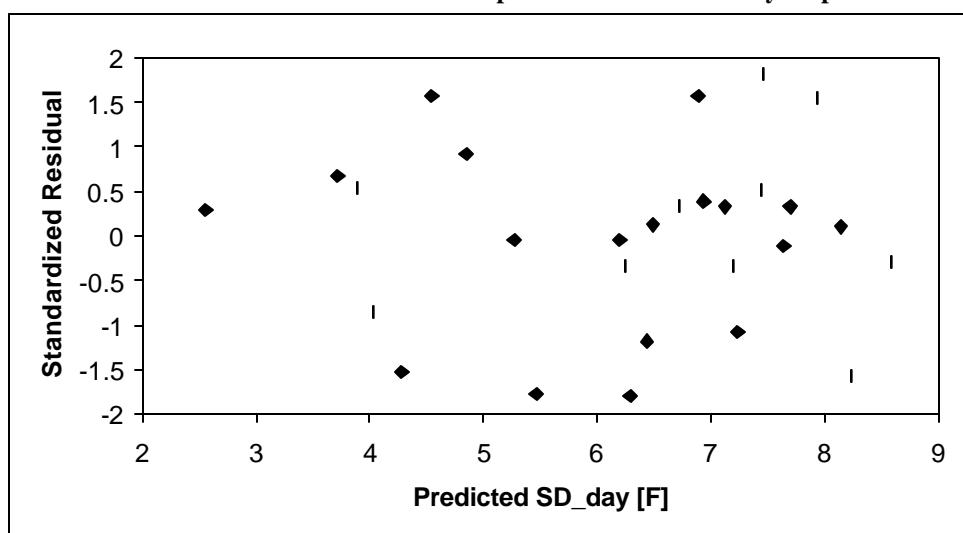
Source	DF	Seq SS
$z$	1	0.660
$\bar{K}_t$	1	0.029
Long	1	2.997
$Long^2$	1	12.600
$V_{mon}^2$	1	51.129







Plot of the standardized residuals vs predicted SD of the daily amplitude



**Equation 4.2**

$$\mathbf{W}_{sa,\max} = -17.8 + 0.0717\bar{T}_{mon} + 2.85\mathbf{v}_{mon} + 0.395Long - 0.00235Long^2 - 0.0242\bar{T}_{mon}\mathbf{v}_{mon}$$

S = 0.6910 R<sup>2</sup> = 98.4%

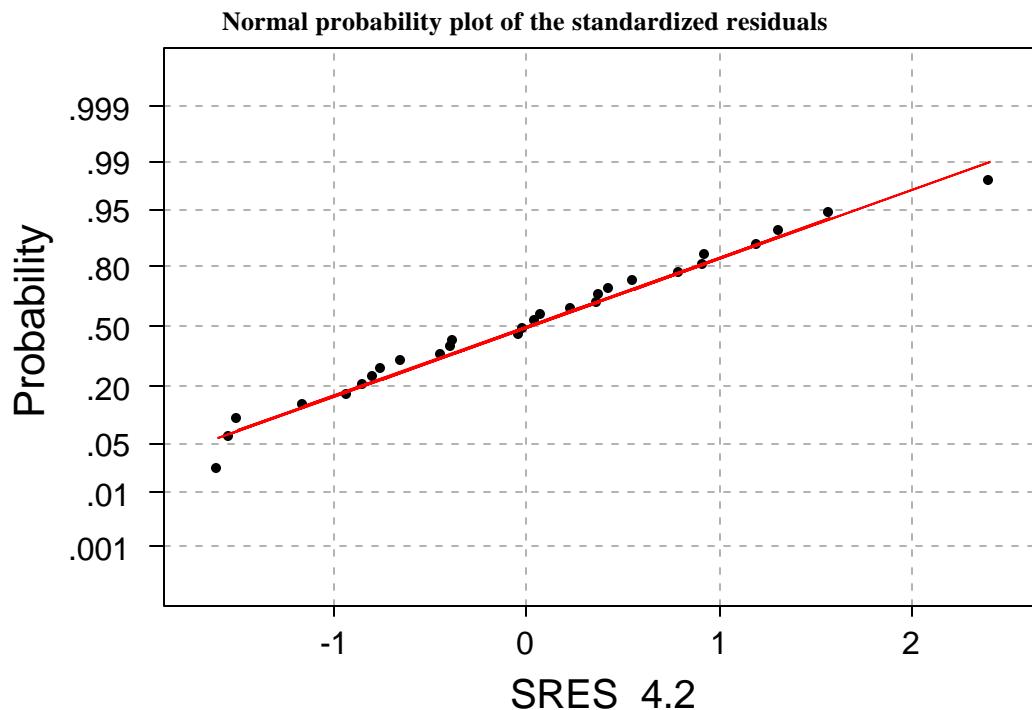
Parameter Estimates

Predictor	Coef	StDev	t-value	p-value
Constant	-17.837	6.625	-2.69	0.013
$\bar{T}_{mon}$	0.07169	0.02160	3.32	0.003
$\mathbf{v}_{mon}$	2.8465	0.3117	9.13	0.000
<i>Long</i>	0.3951	0.1337	2.95	0.007
<i>Long</i> <sup>2</sup>	-0.0023450	0.0006713	-3.49	0.002
$\bar{T}_{mon}\mathbf{v}_{mon}$	-0.024233	0.003221	-7.52	0.000

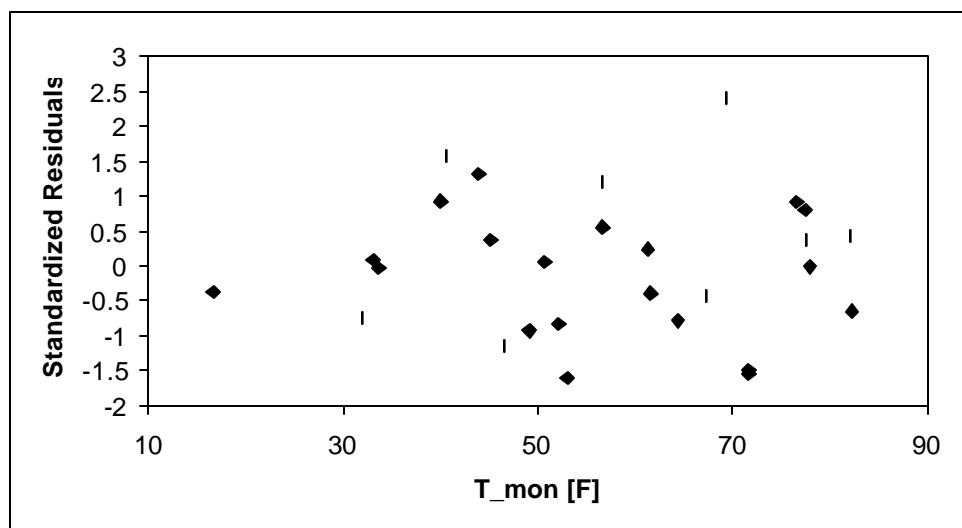
Analysis of Variance

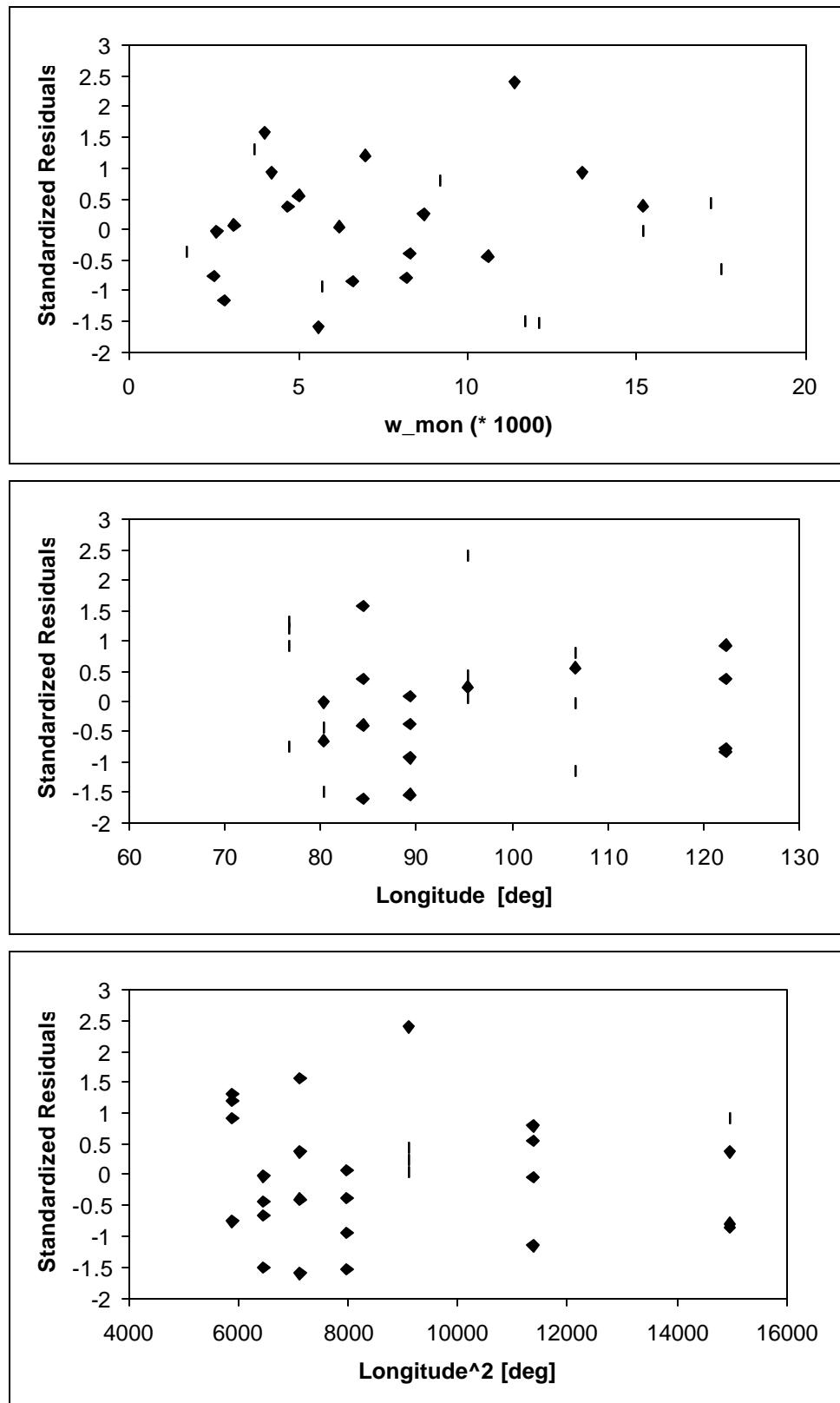
Source	DF	SS	MS	F-statistic	p-value
Regression	5	644.00	128.80	269.77	0.000
Error	22	10.50	0.48		
Total	27	654.50			

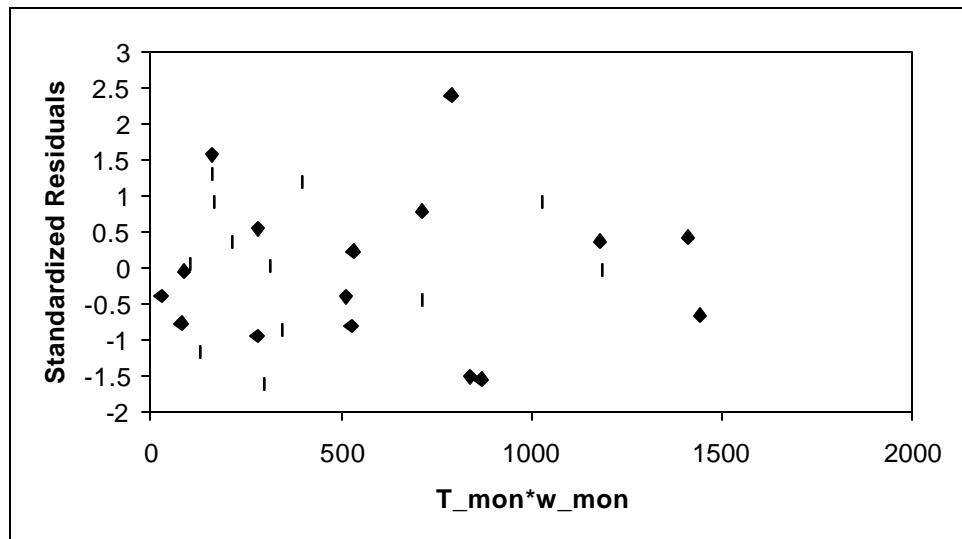
Source	DF	Seq SS
$\bar{T}_{mon}$	1	538.38
$\mathbf{v}_{mon}$	1	50.19
<i>Long</i>	1	26.27
<i>Long</i> <sup>2</sup>	1	2.14
$\bar{T}_{mon}\mathbf{v}_{mon}$	1	27.02



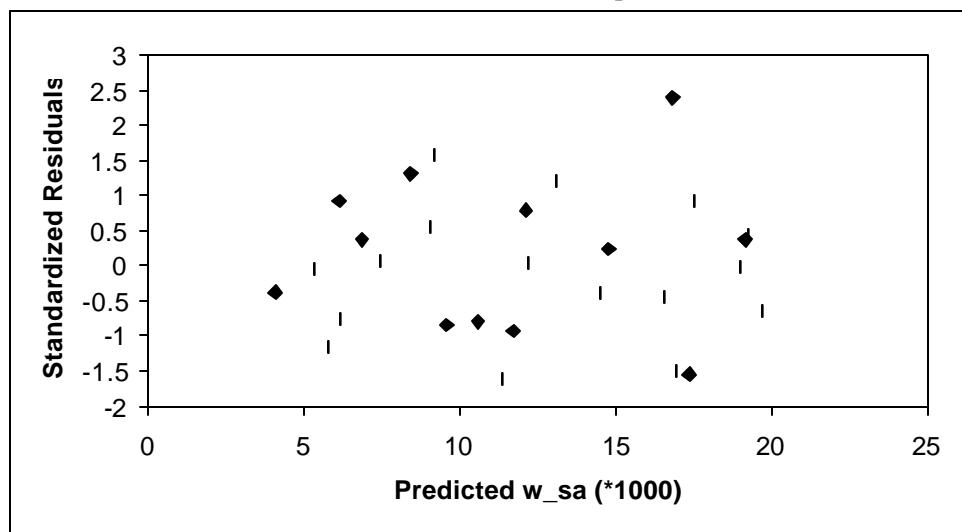
Plots of the standardized residuals vs predictors







Plot of the standardized residuals vs predicted  $w_{sa}$



**Equation 4.3**

$$T_{sa,\max} = -52.7 + 0.916\bar{T}_{mon} + \bar{T}_{yr} + 1.42f - 45.2\bar{K}_t - 0.00195\mathbf{v}_{mon}^3$$

S = 3.404 °F     R<sup>2</sup> = 94.9%

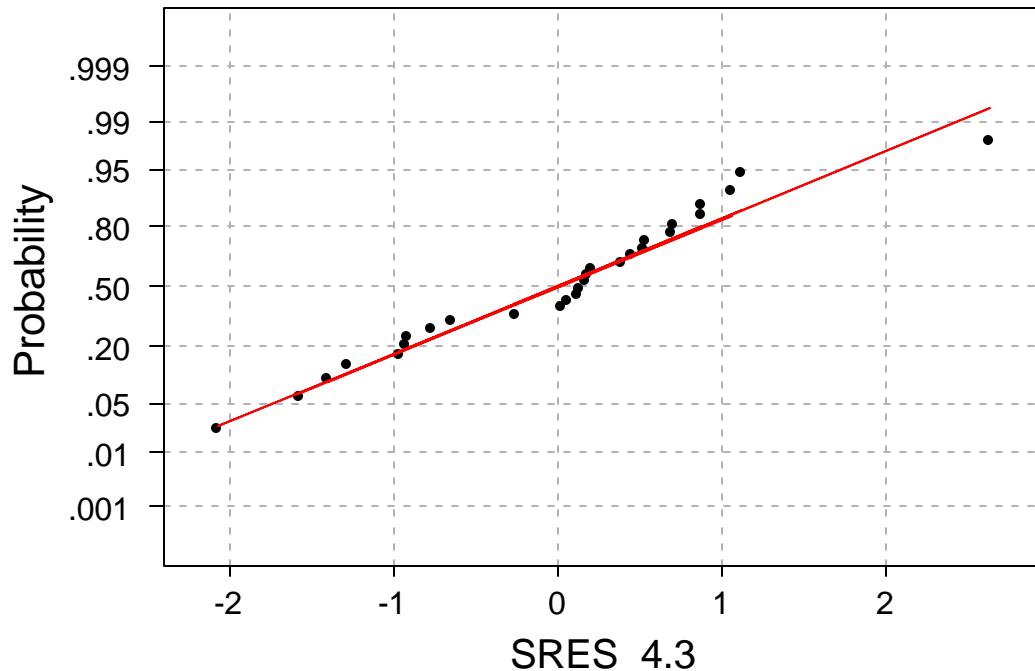
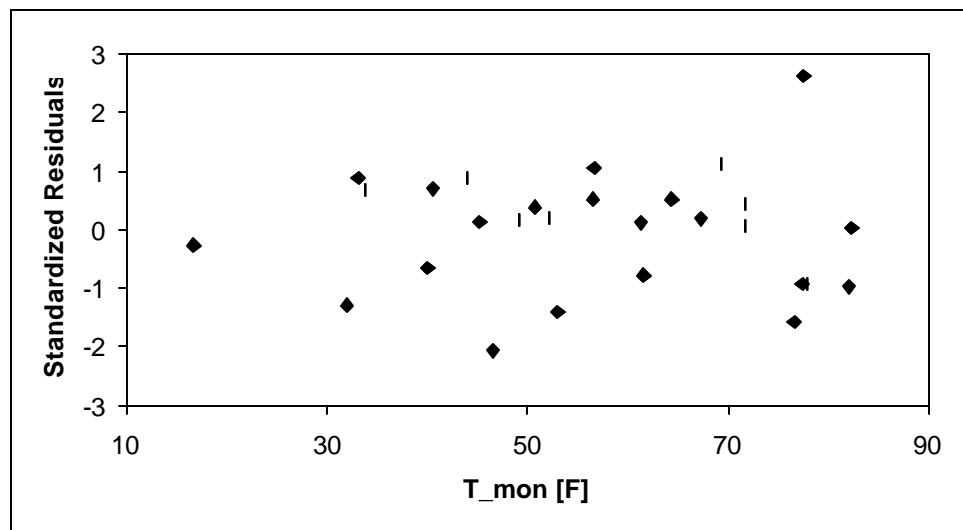
Parameter Estimates

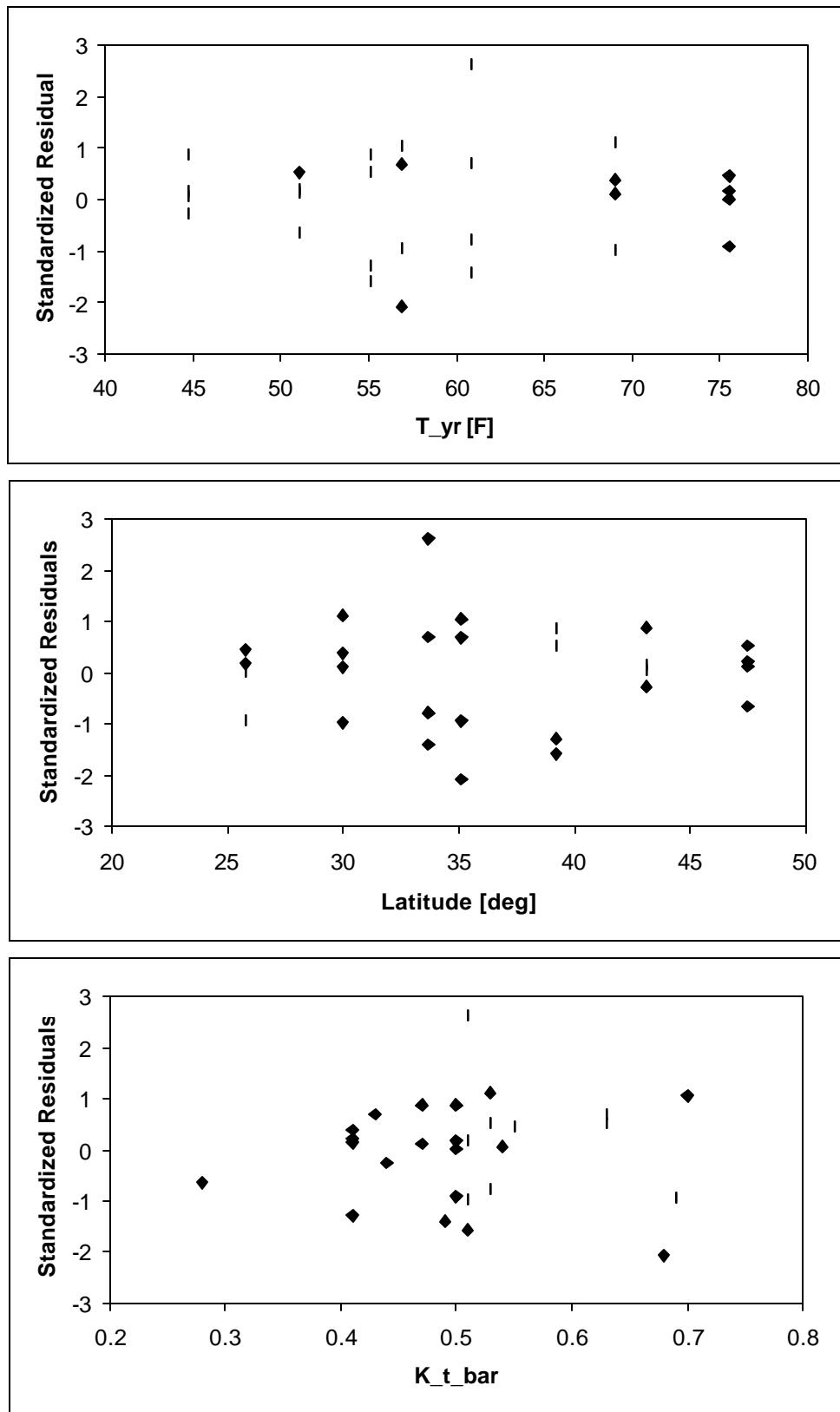
Predictor	Coef	StDev	t-value	p-value
Constant	-52.71	24.69	-2.14	0.044
$\bar{T}_{mon}$	0.91613	0.07463	12.28	0.000
$\bar{T}_{yr}$	0.7348	0.2178	3.37	0.003
$f$	1.4230	0.2939	4.84	0.000
$\bar{K}_t$	-45.171	9.685	-4.66	0.000
$\mathbf{v}_{mon}^3$	-0.0019518	0.0007448	-2.62	0.016

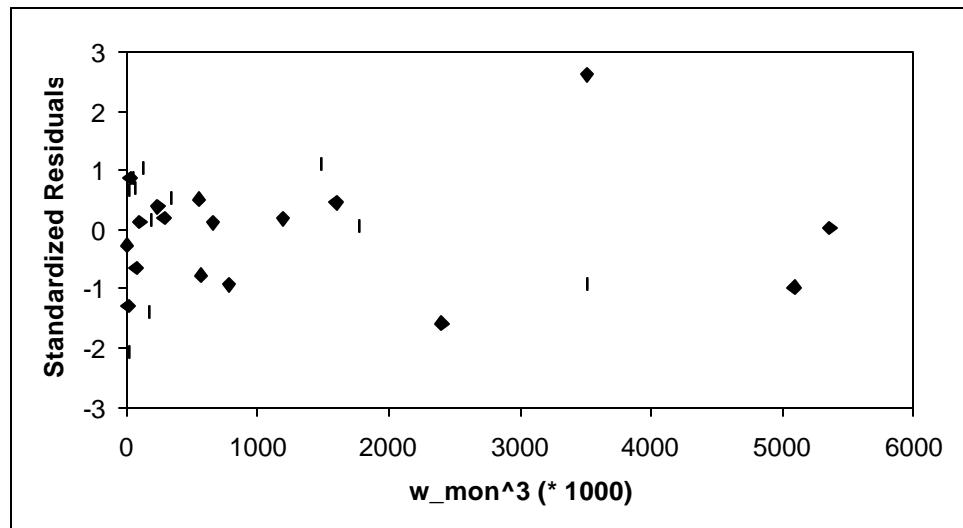
Analysis of Variance

Source	DF	SS	MS	F-statistic	p-value
Regression	5	4774.86	954.97	82.43	0.000
Error	22	254.87	11.59		
Total	27	5029.73			

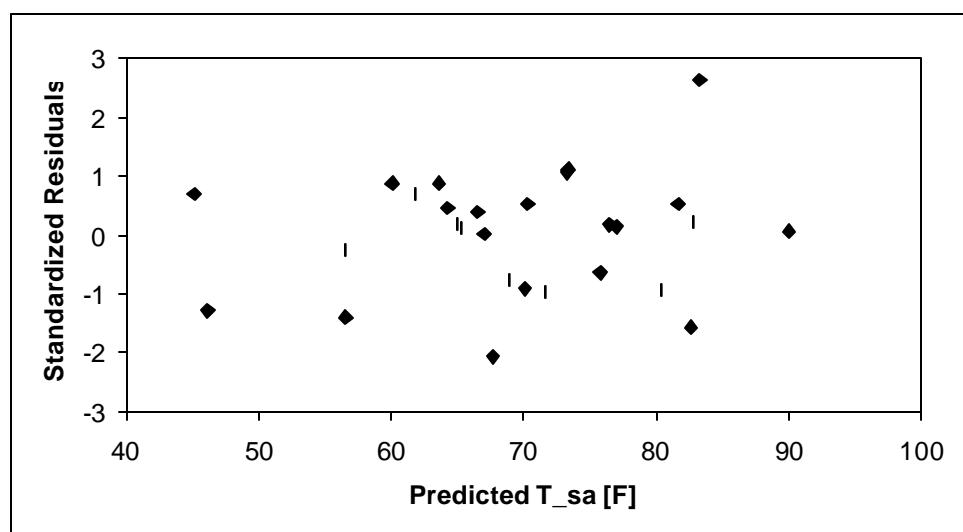
Source	DF	Seq SS
$\bar{T}_{mon}$	1	3434.25
$\bar{T}_{yr}$	1	57.55
$f$	1	1023.54
$\bar{K}_t$	1	179.96
$\mathbf{v}_{mon}^3$	1	79.57

**Normality plot of the standardized residuals****Plots of the standardized residuals vs predictors**





Plot of the standardized residuals vs predicted  $\bar{T}_{sa,\max}$



**Equation 4.4**

$$\mathbf{w}_{coin,max} = 0.070 + 4.76\mathbf{v}_{mon} - 0.000510Long^2 - 0.0429\bar{T}_{mon}\mathbf{v}_{mon}$$

S = 1.025      R<sup>2</sup> = 96.8%

Parameter Estimates

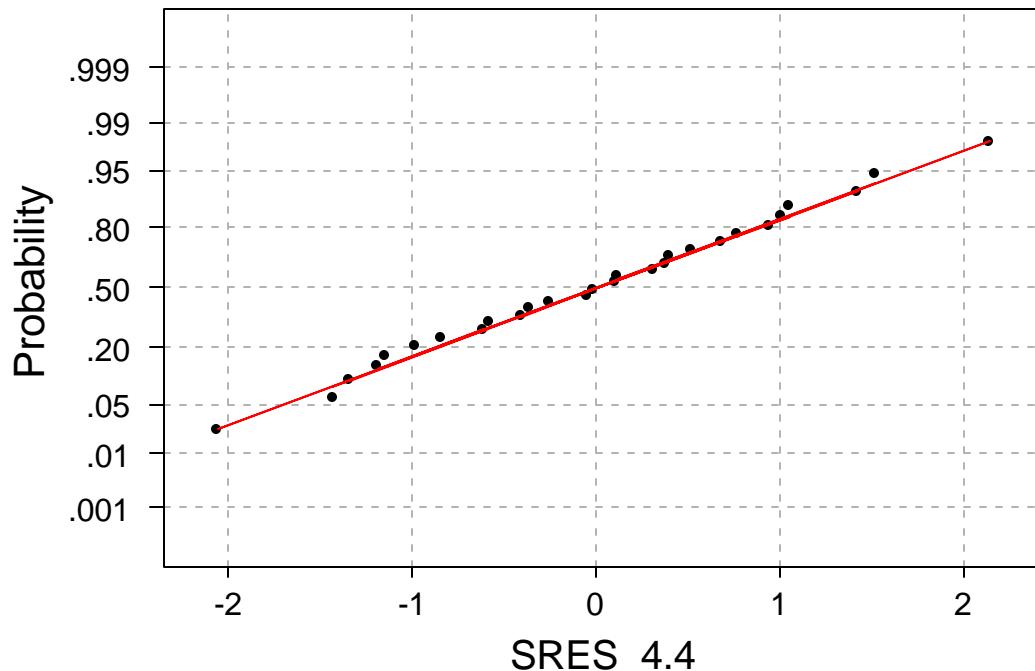
Predictor	Coef	StDev	t-value	p-value
Constant	0.074	1.158	0.06	0.949
$\mathbf{v}_{mon}$	4.7578	0.4164	11.43	0.000
$Long^2$	-0.00051010	0.00006824	-7.47	0.000
$\bar{T}_{mon}\mathbf{v}_{mon}$	-0.042854	0.004635	-9.25	0.000

Analysis of Variance

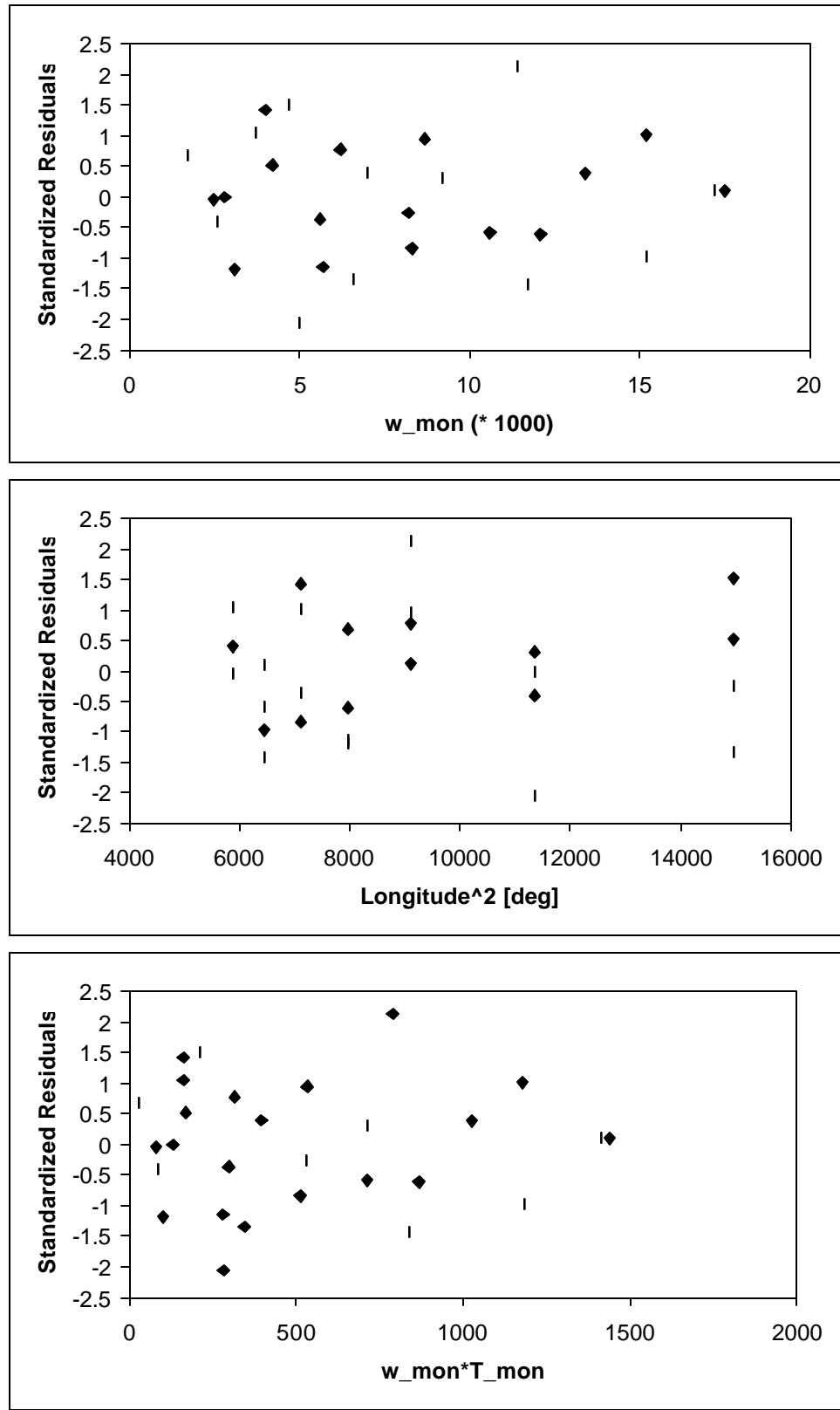
Source	DF	SS	MS	F-statistic	p-value
Regression	3	754.93	251.64	239.64	0.000
Error	24	25.20	1.05		
Total	27	780.13			

Source	DF	Seq SS
$\mathbf{v}_{mon}$	1	615.60
$Long^2$	1	49.57
$\bar{T}_{mon}\mathbf{v}_{mon}$	1	89.76

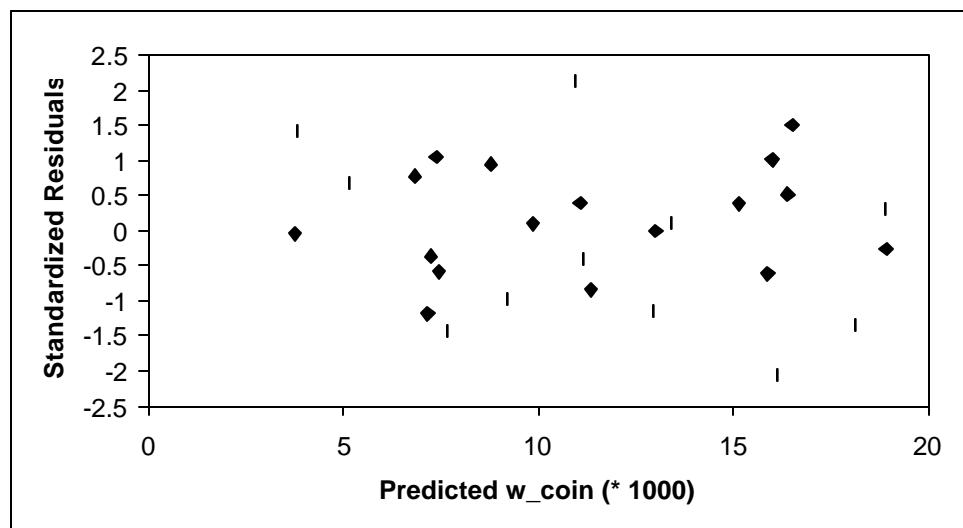
Normality plot of the standardized residuals

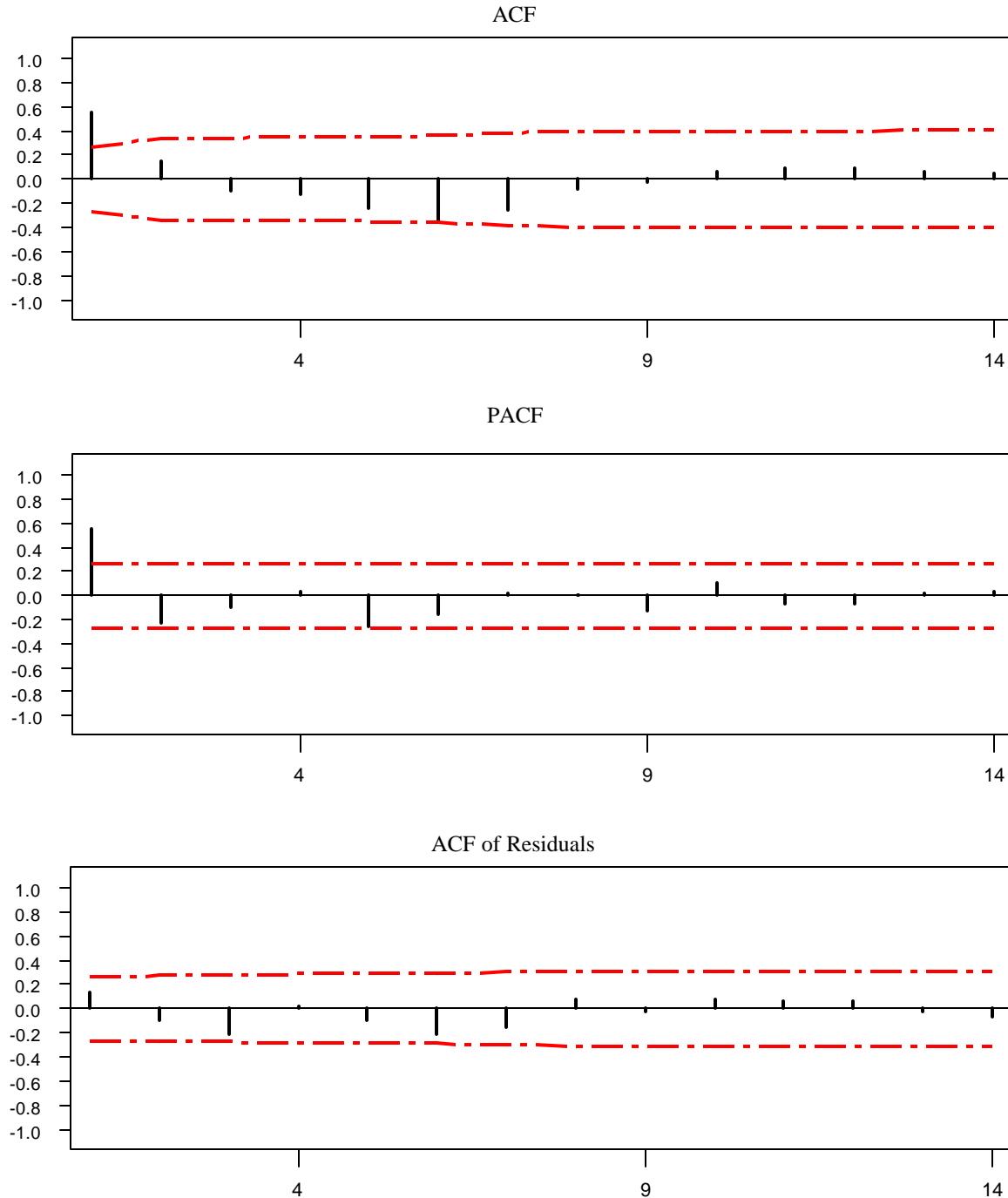


**Plots of the standardized residuals vs predictors**



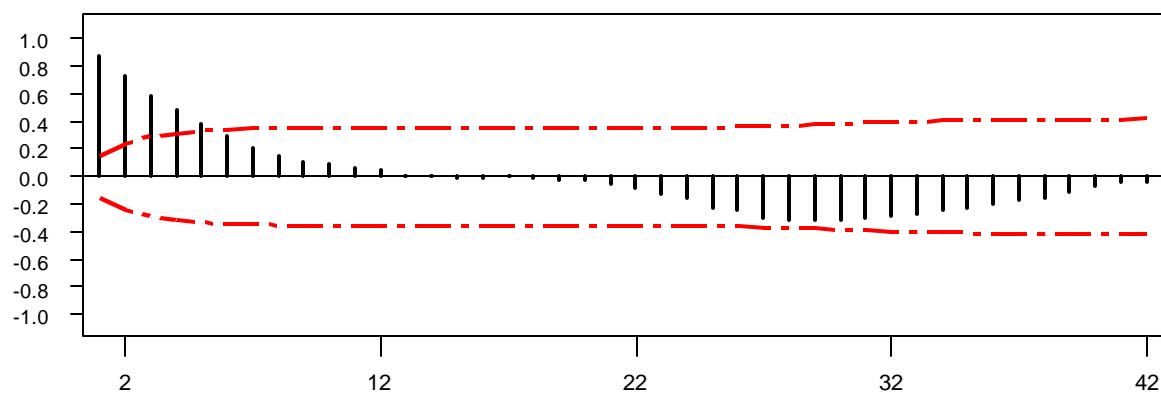
Plot of the standardized residuals vs predicted  $V_{sa,\max}$



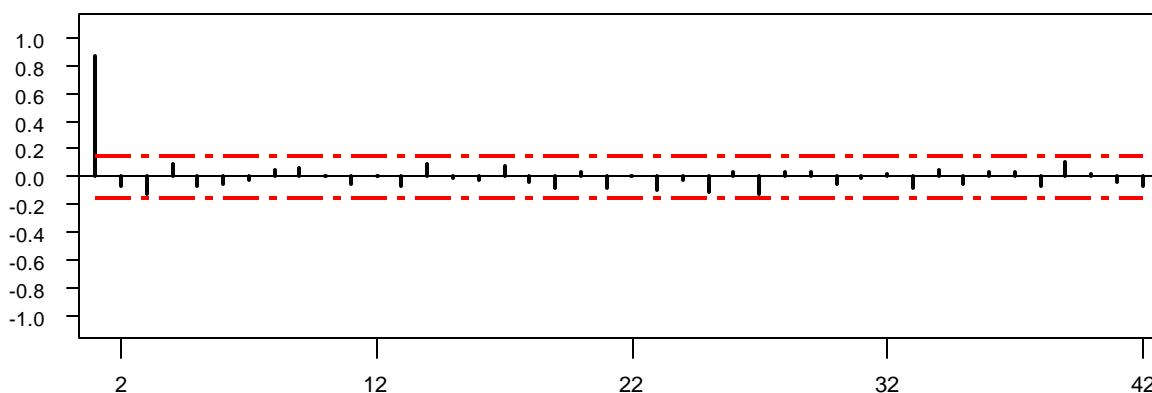
**Stand-Alone Humidity Ratio****Albuquerque, MN**

**Atlanta, GA**

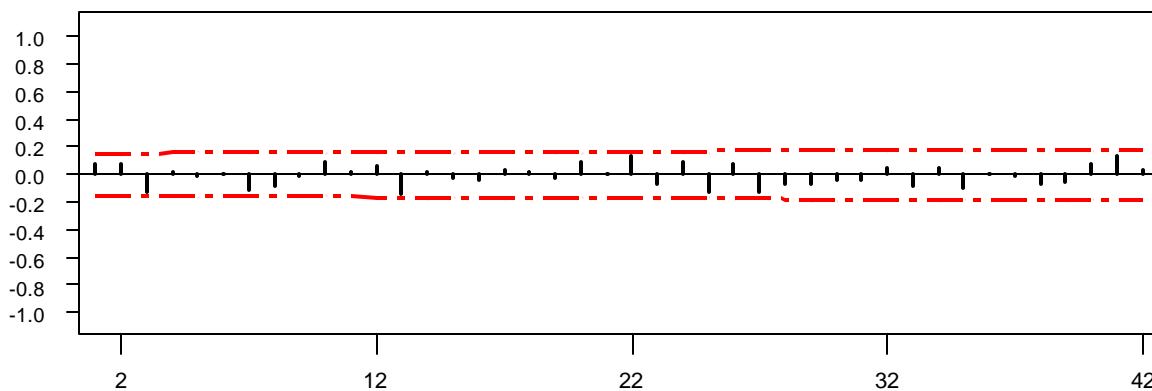
ACF

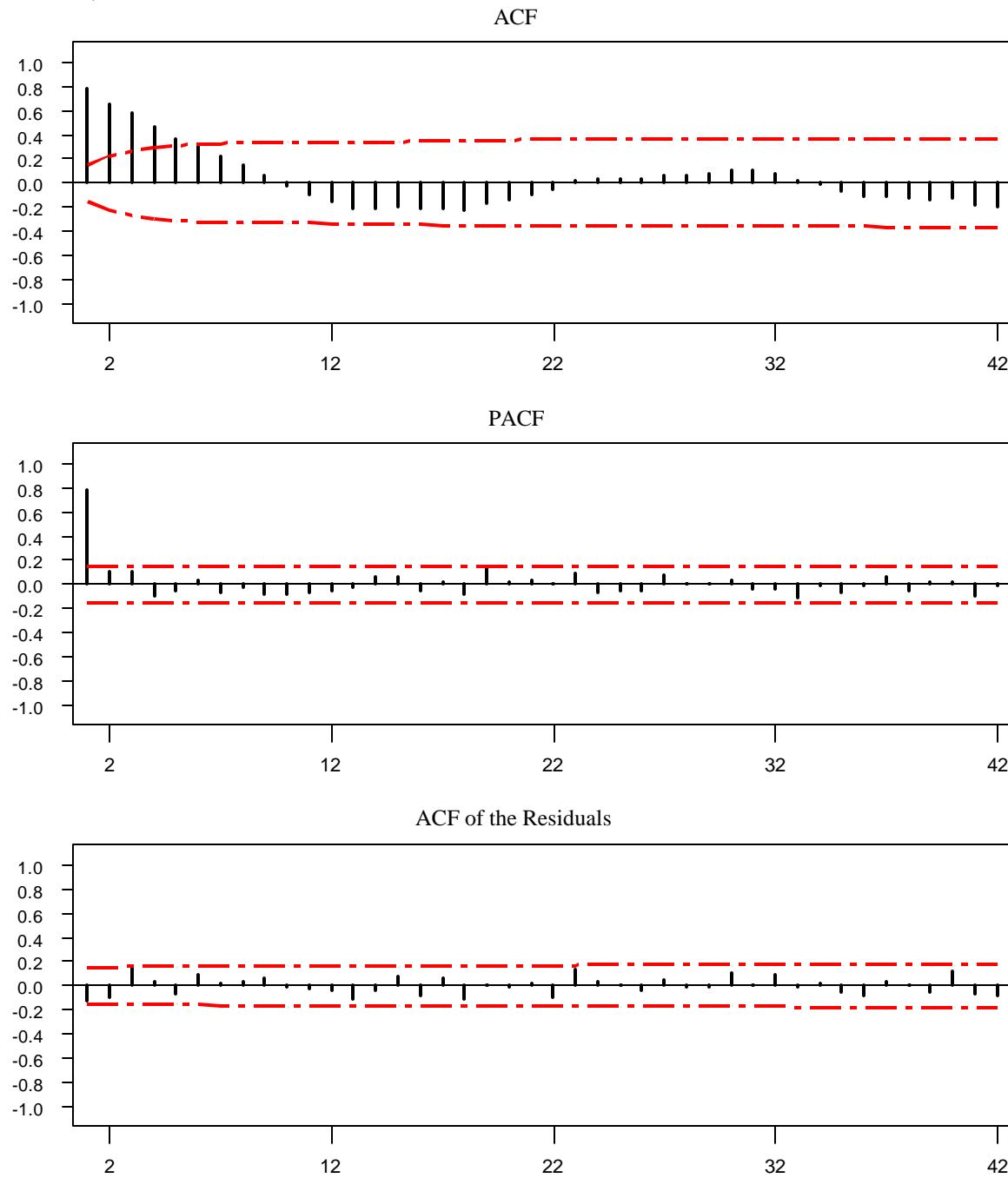


PACF

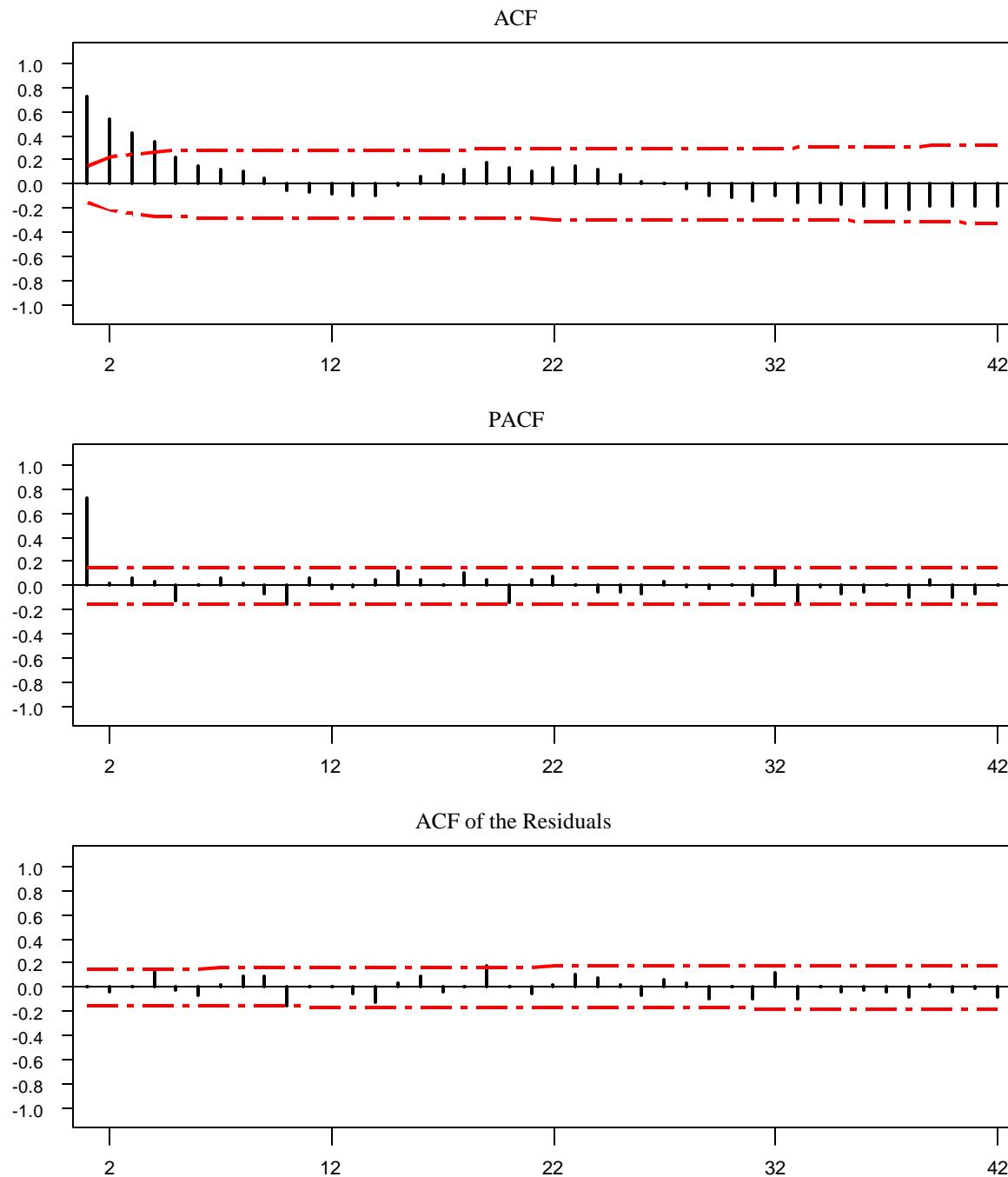


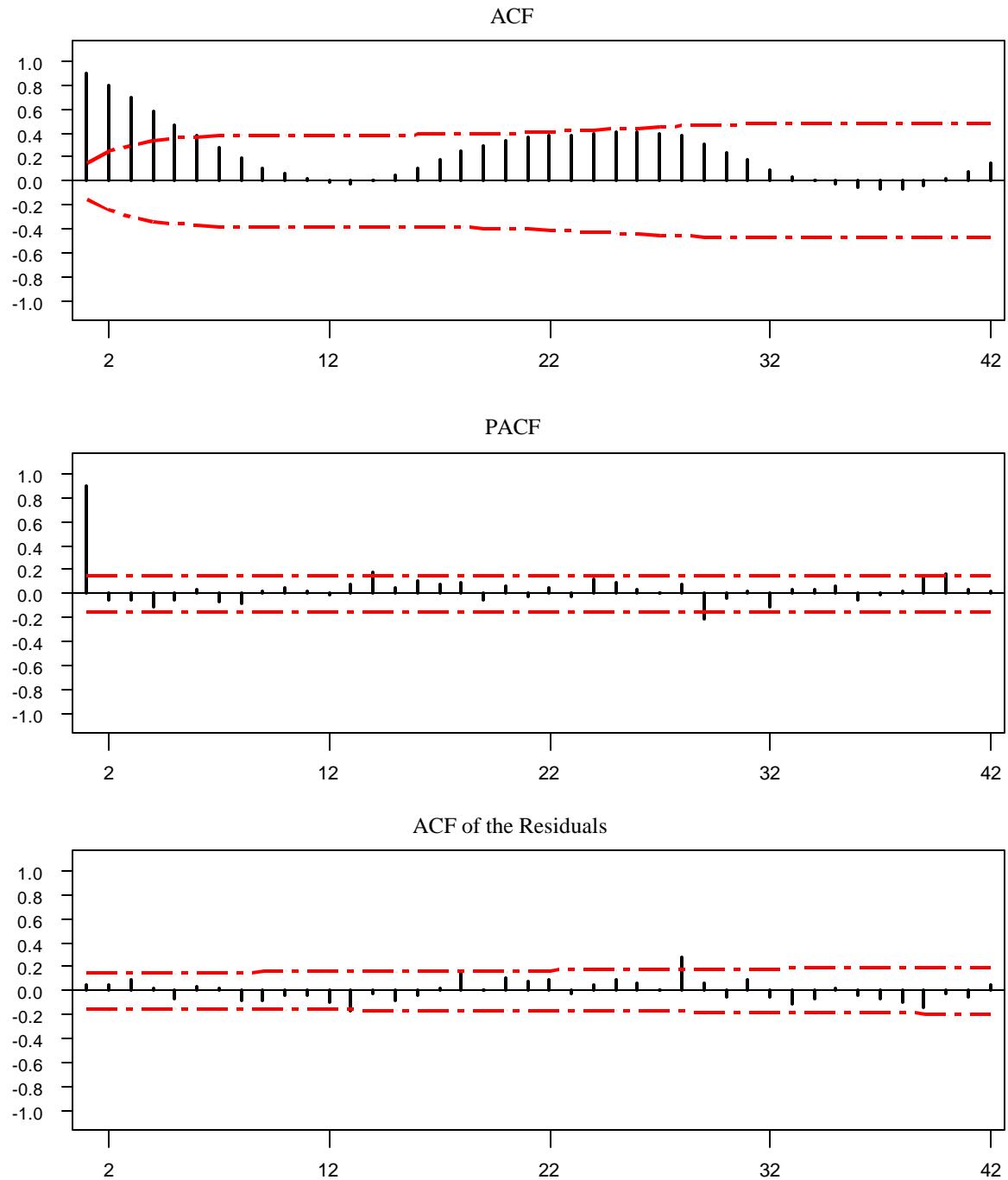
ACF of the Residuals



**Baltimore, MD**

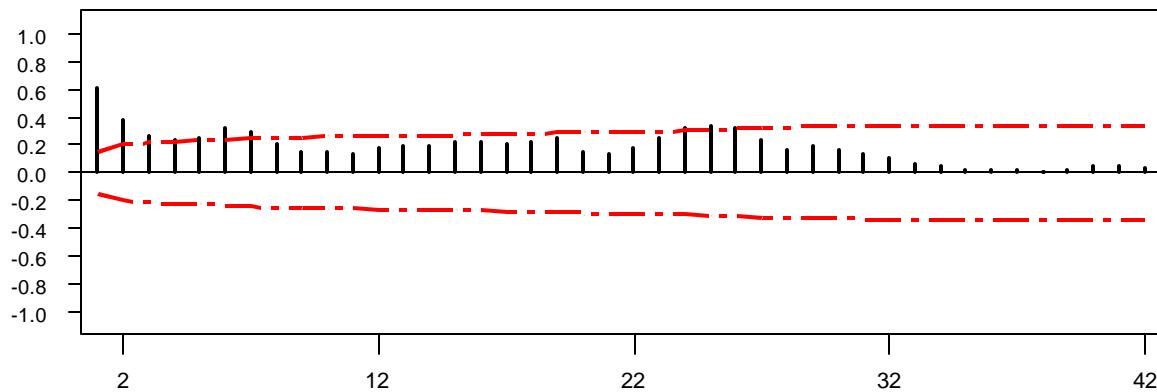
Houston, TX



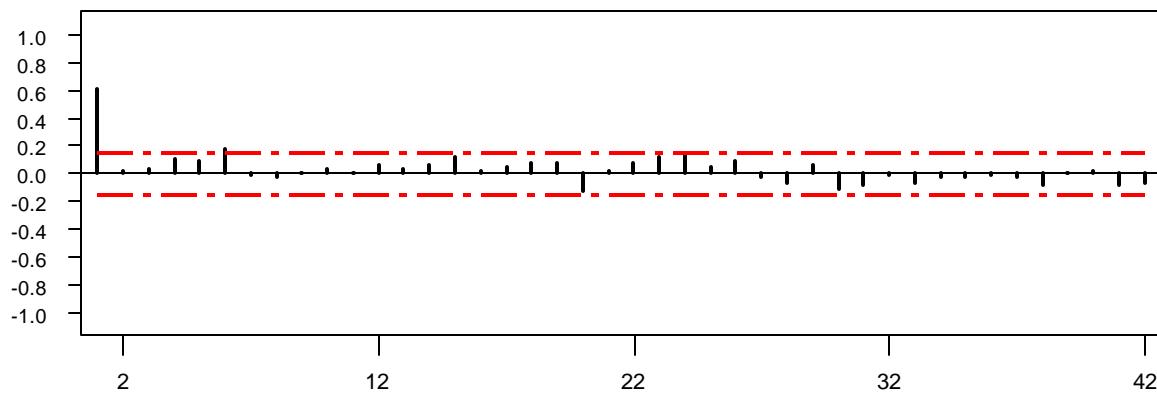
**Madison, WI**

**Miami, FL**

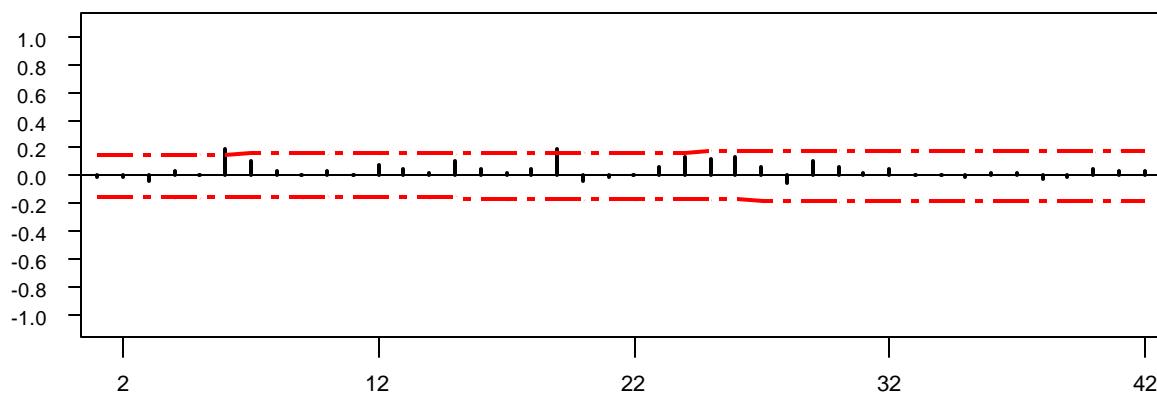
ACF

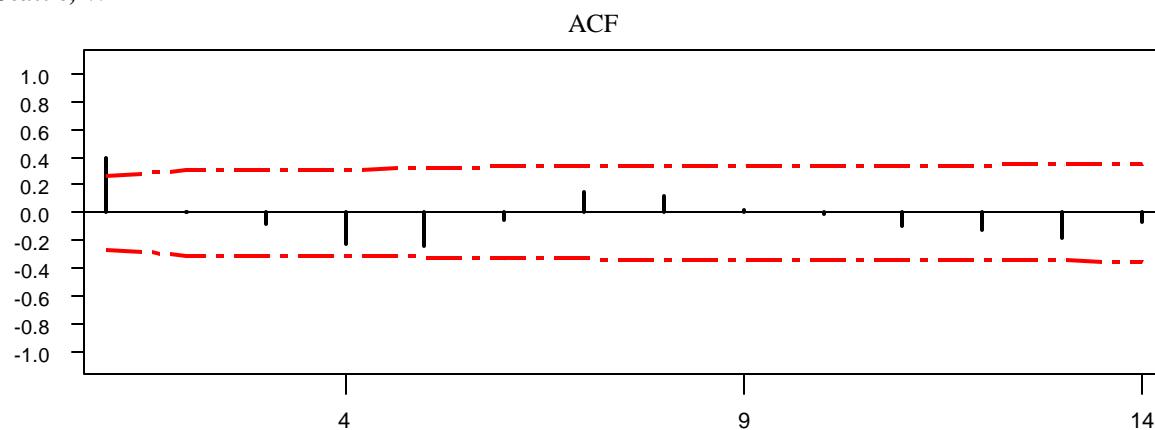


PACF

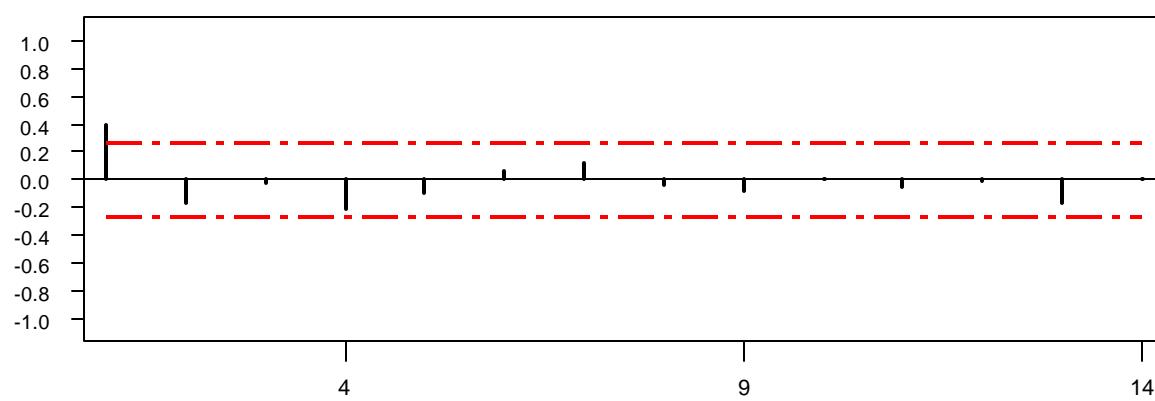


ACF of the Residuals

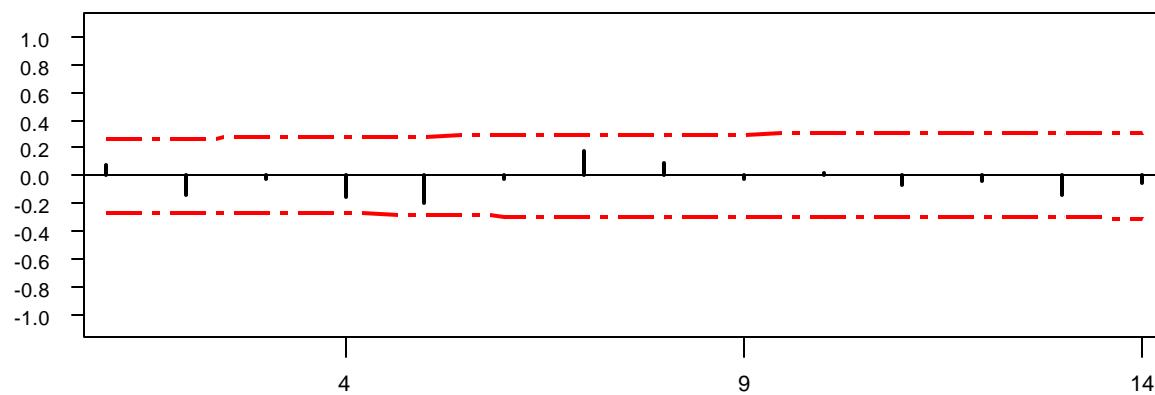


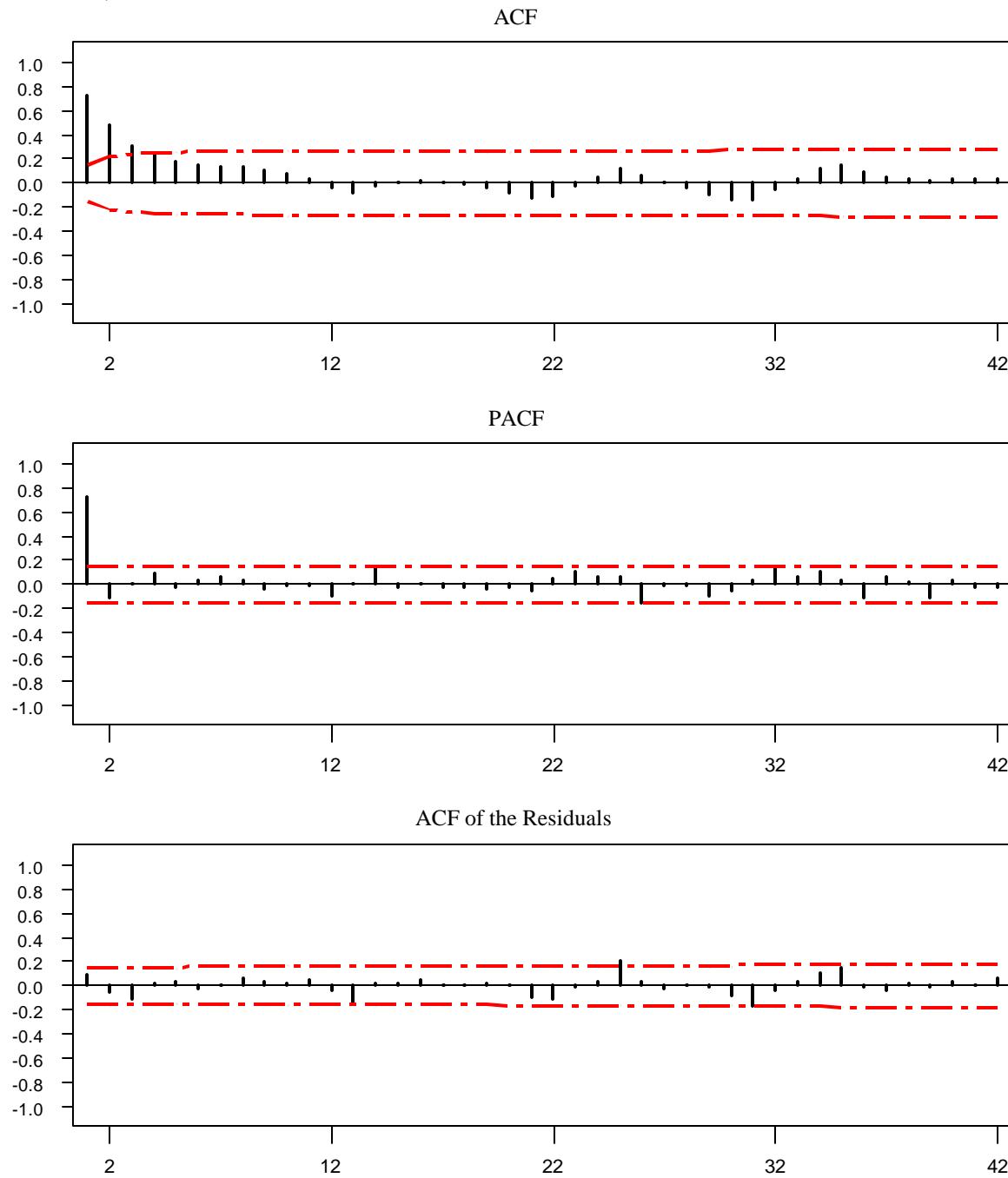
**Seattle, WA**

PACF



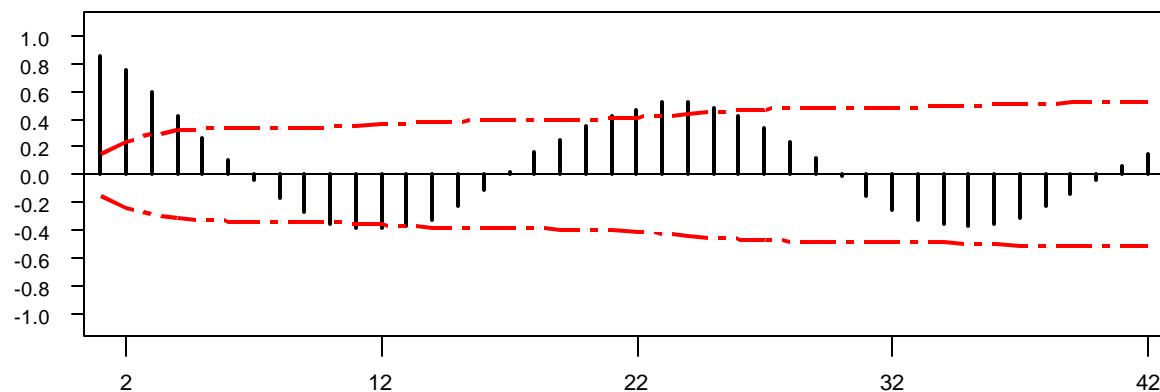
ACF of the Residuals



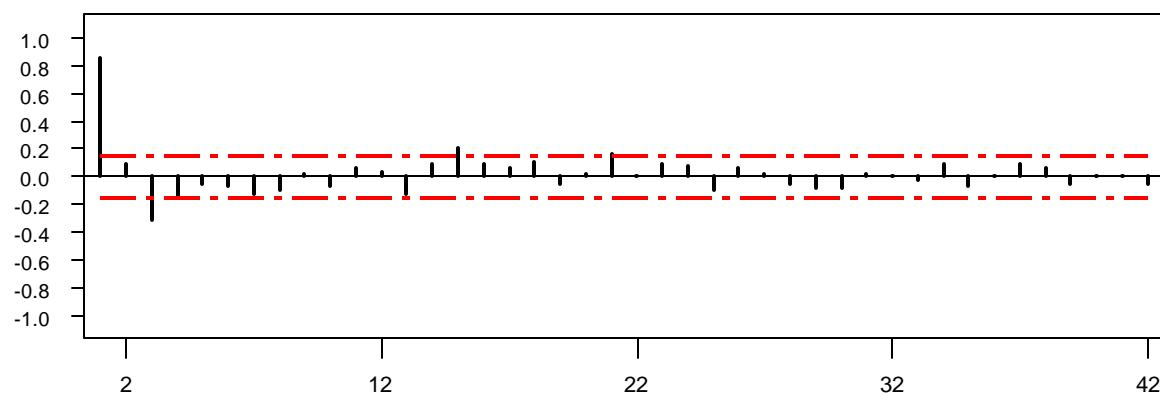
**Charleston, SC**

**Chicago, IL**

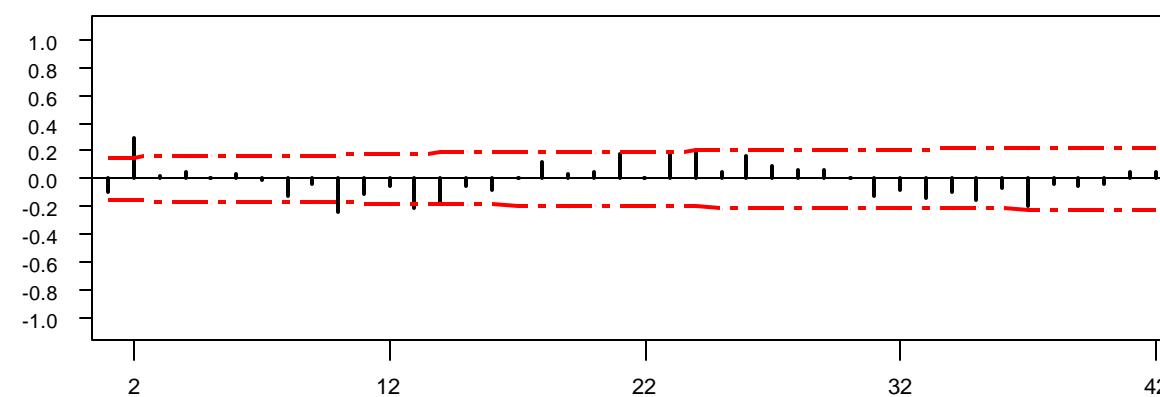
ACF



PACF

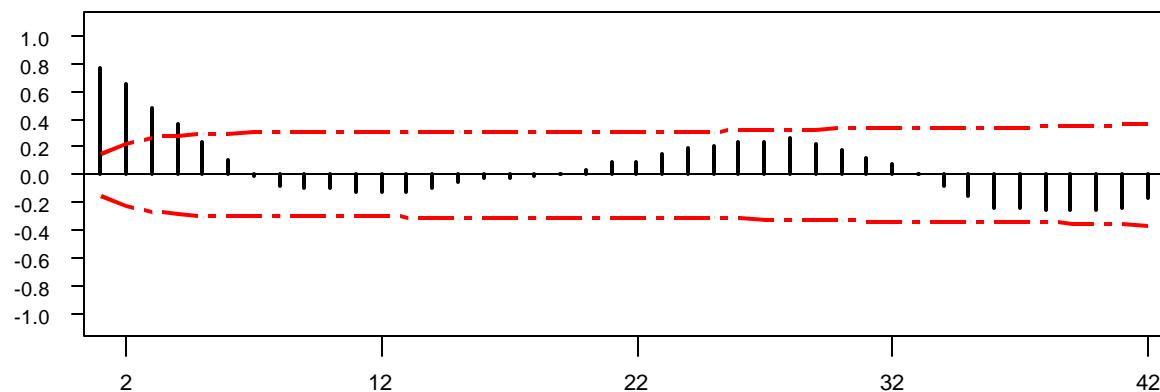


ACF of the Residuals

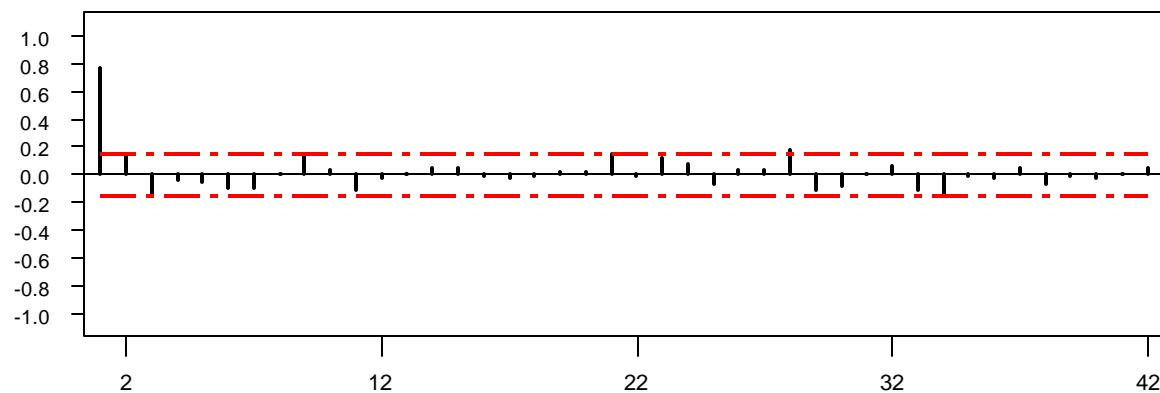


**Kansas, MO**

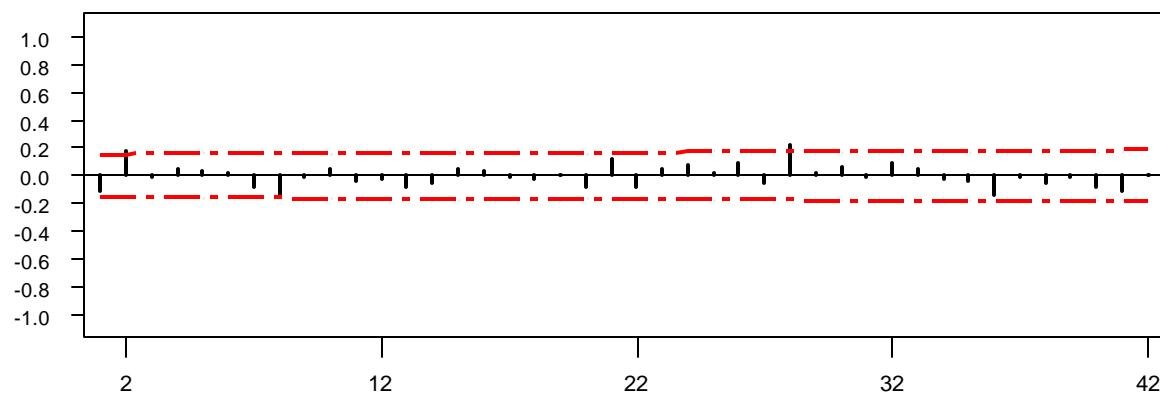
ACF

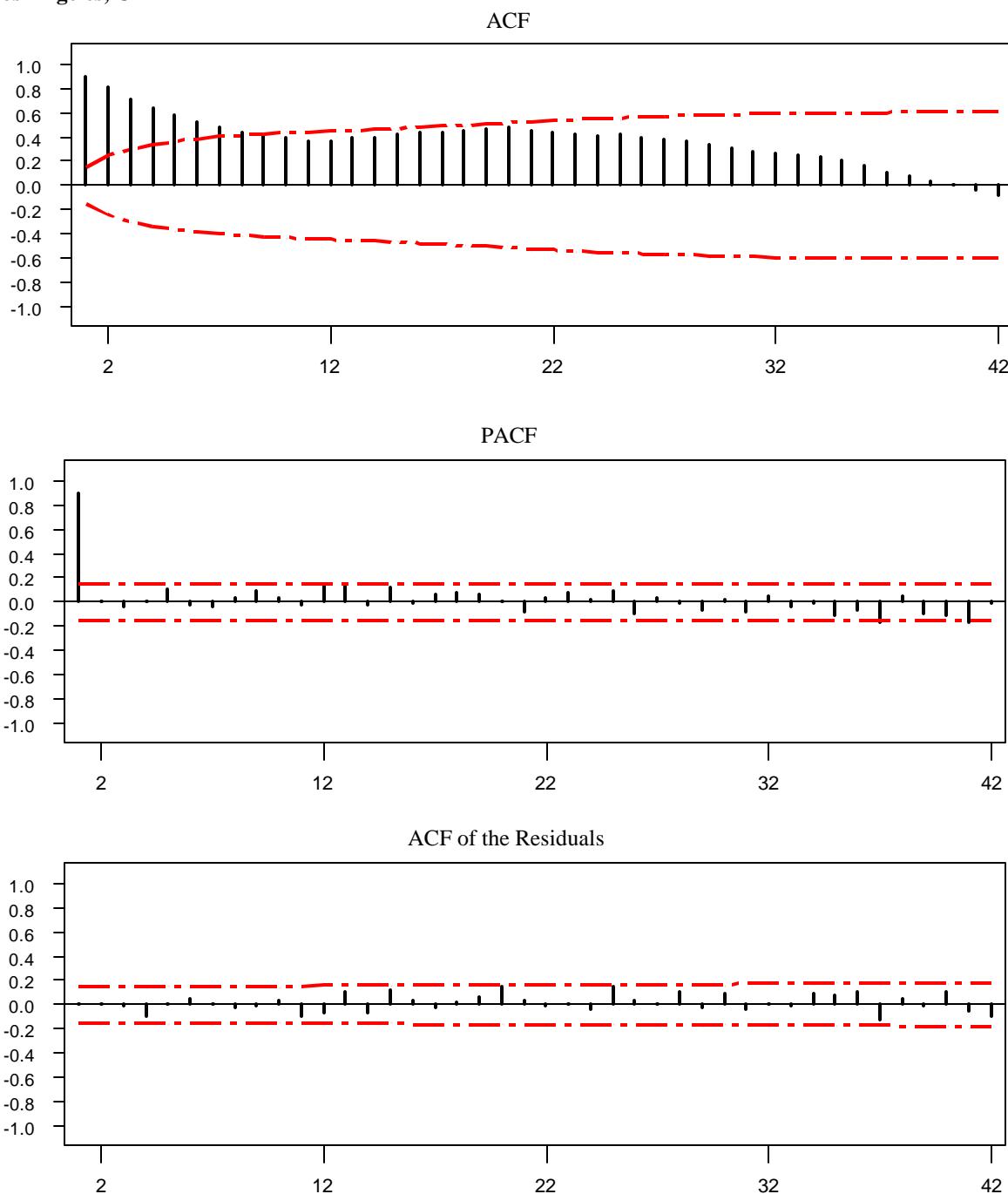


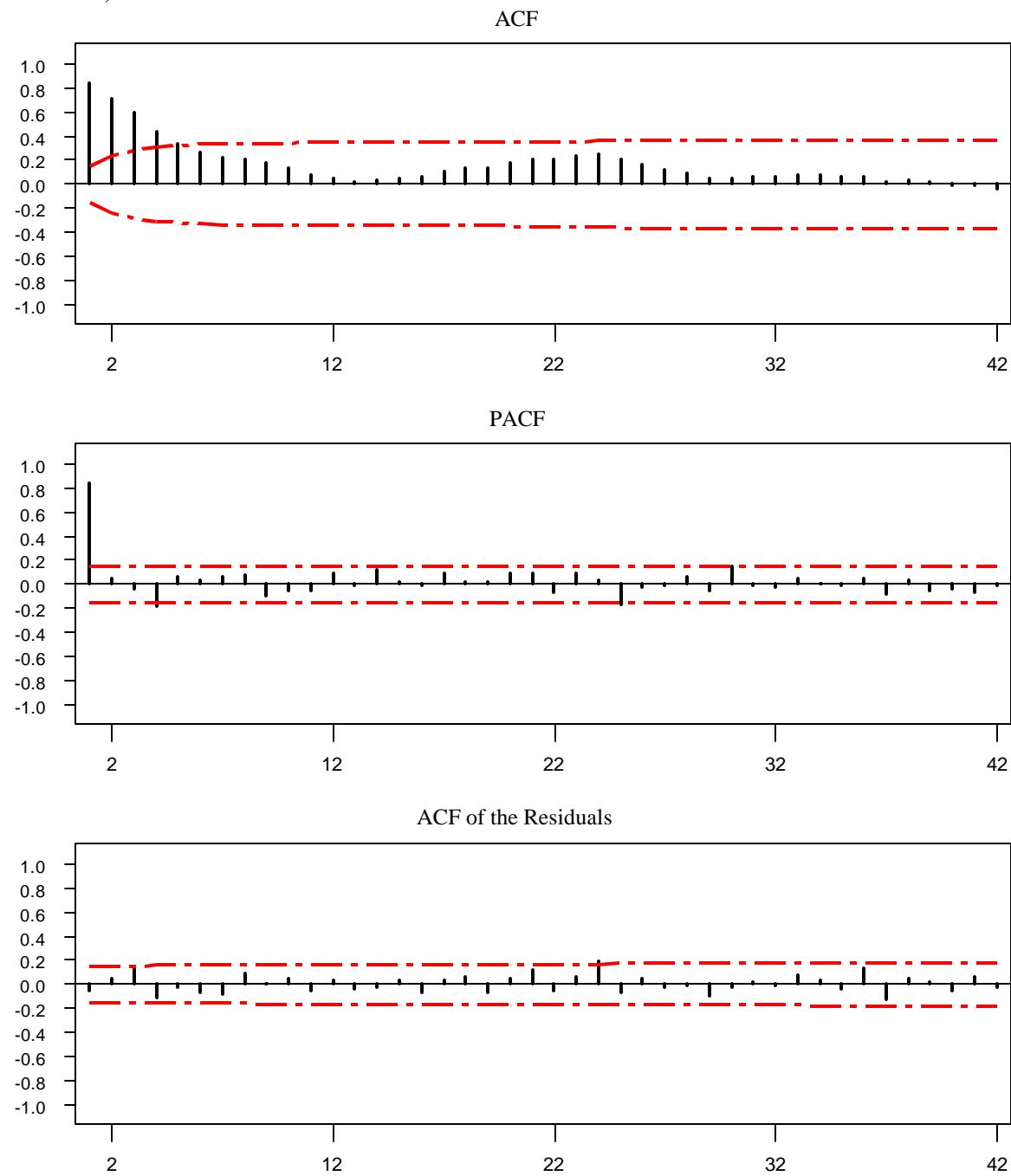
PACF

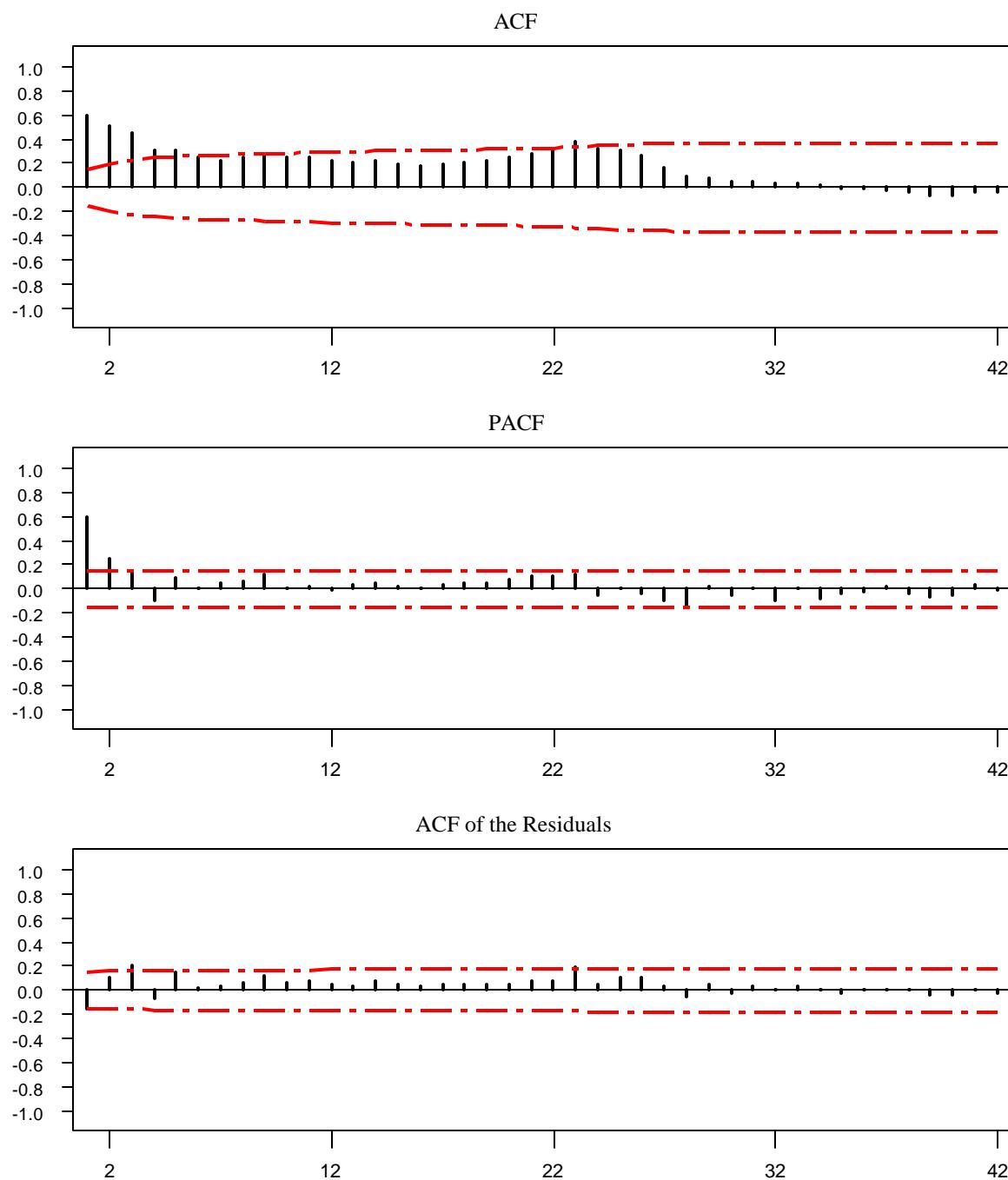


ACF of the Residuals



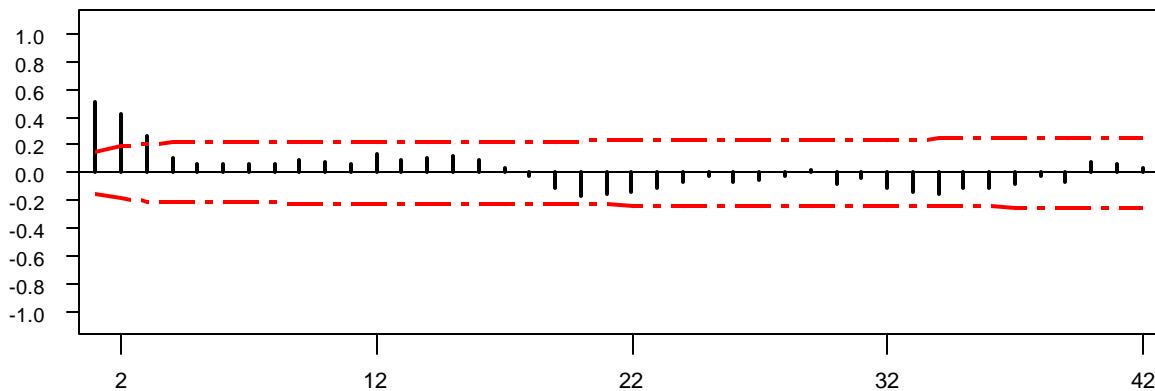
**Los Angeles, CA**

**New York , NY**

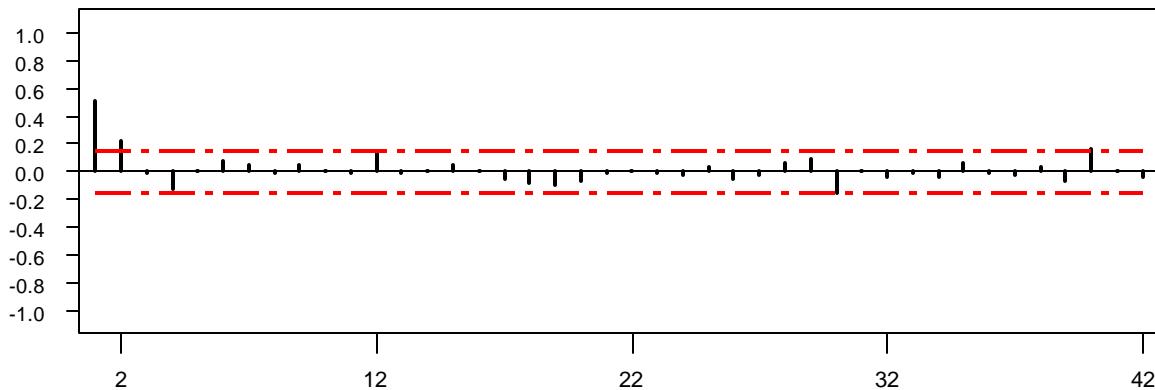
**San Fransisco, CA**

**West Palm Beach, FL**

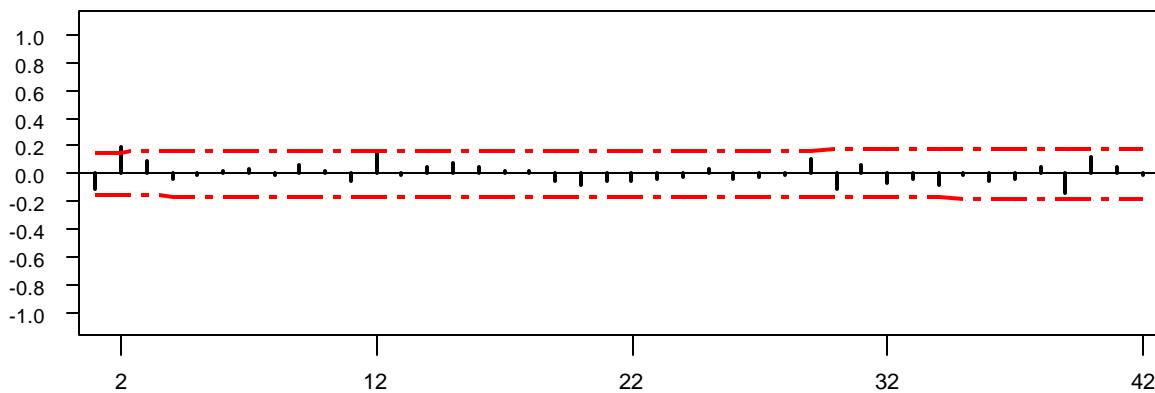
ACF

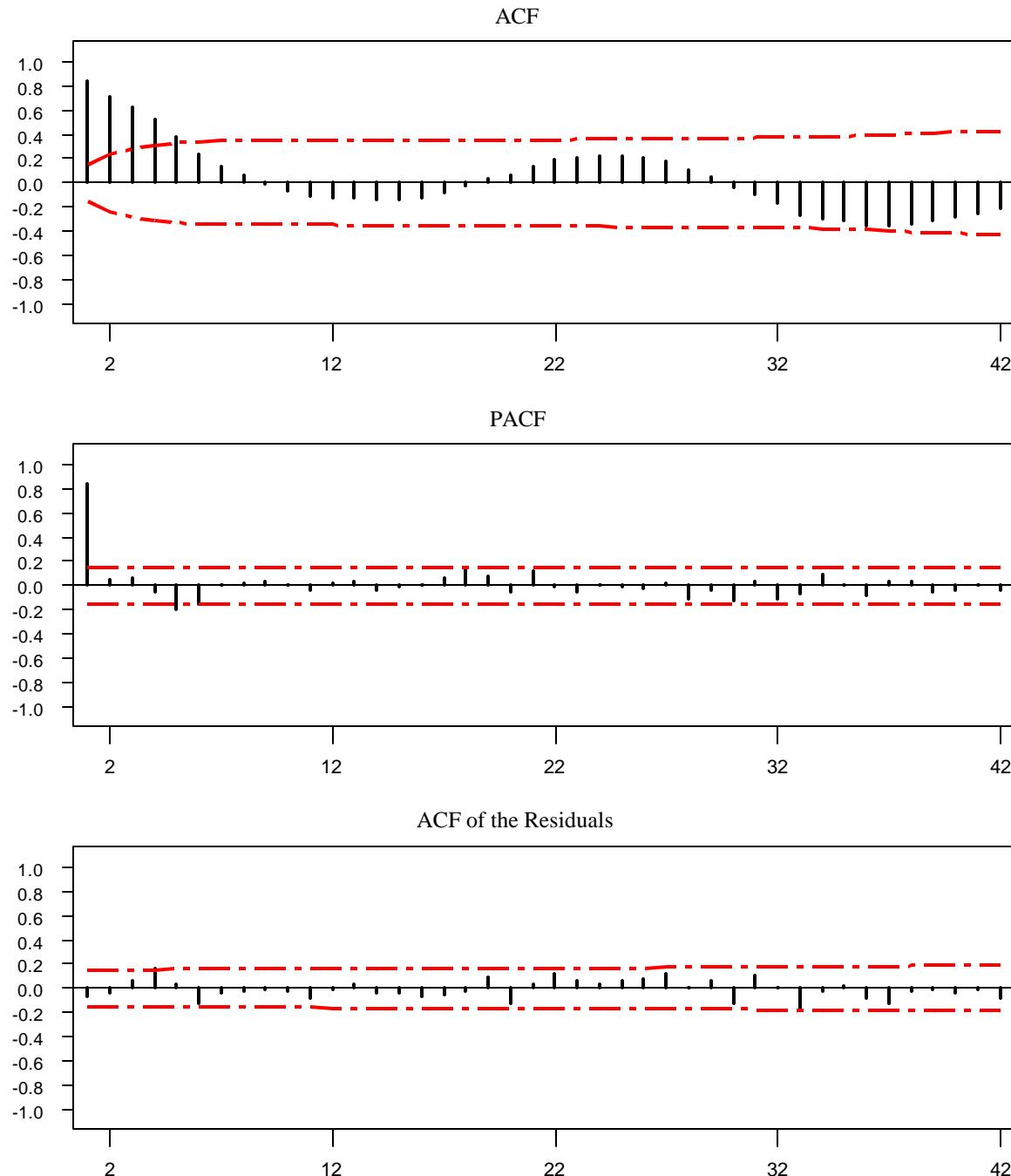


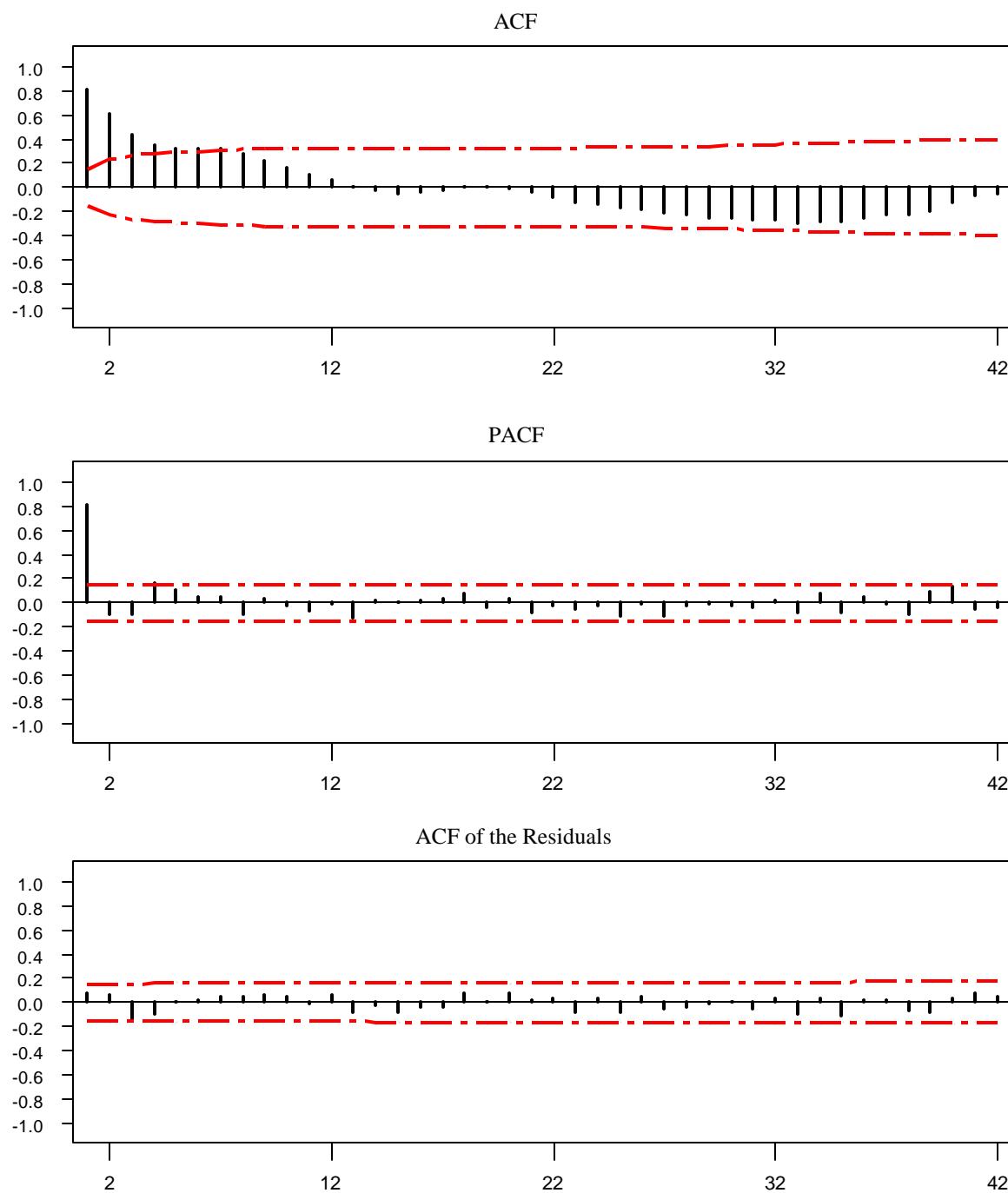
PACF

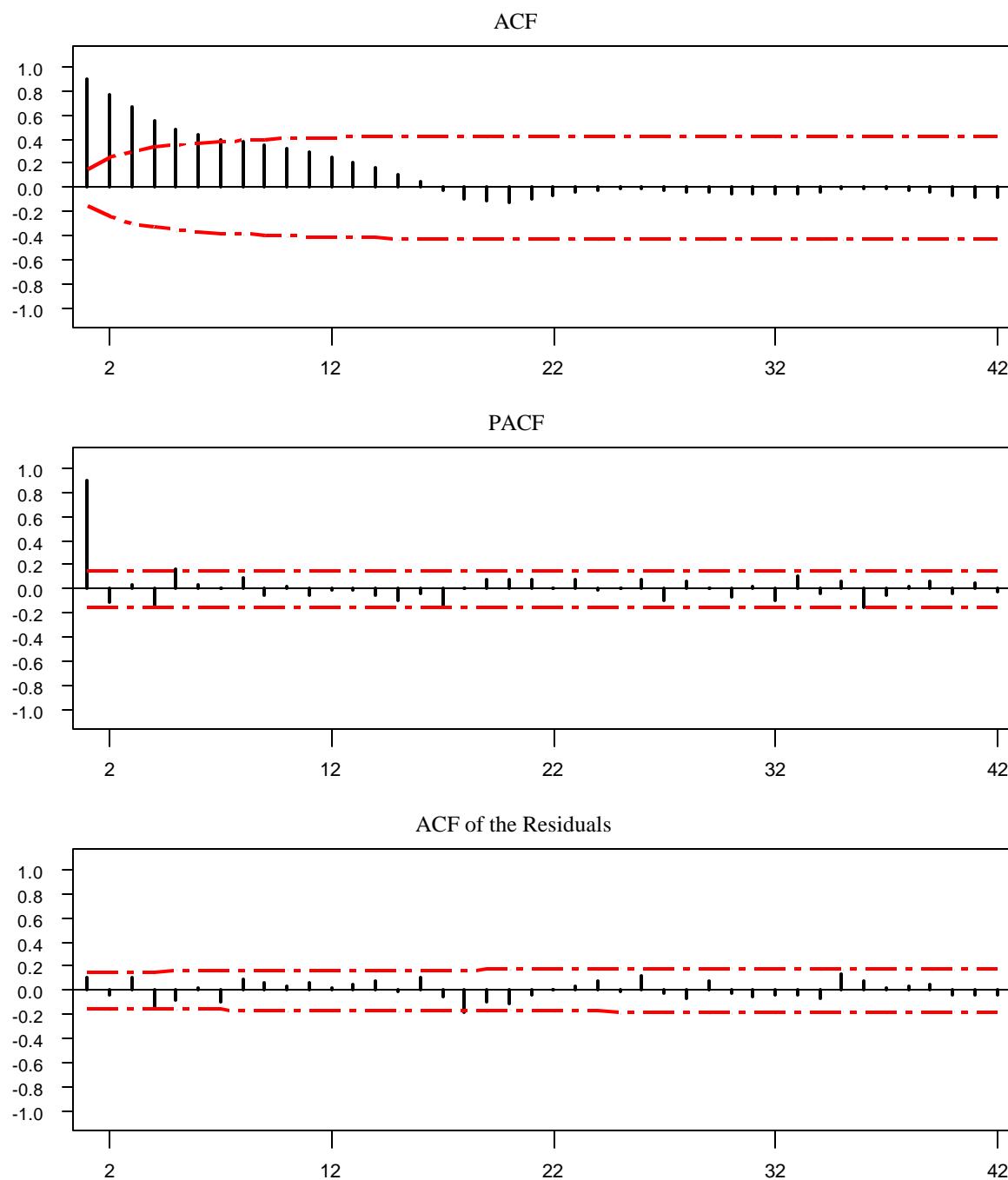


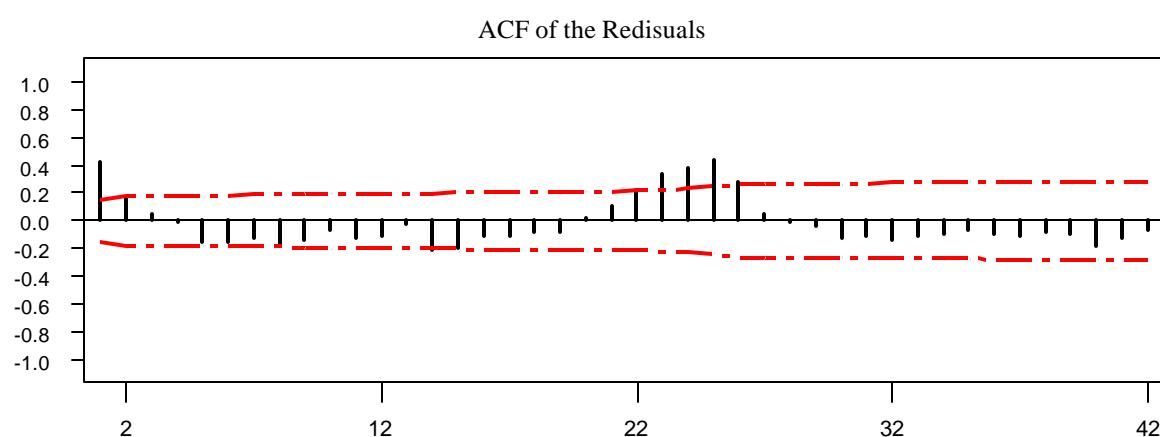
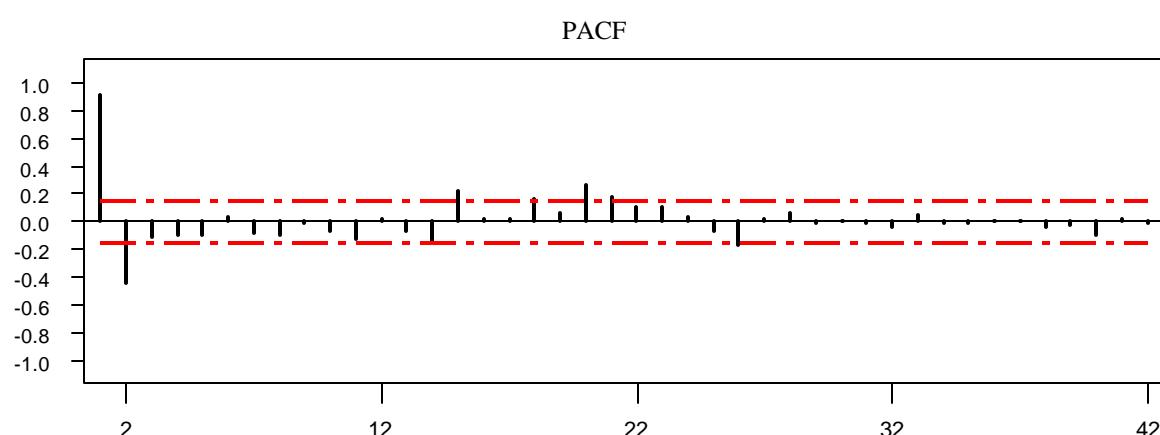
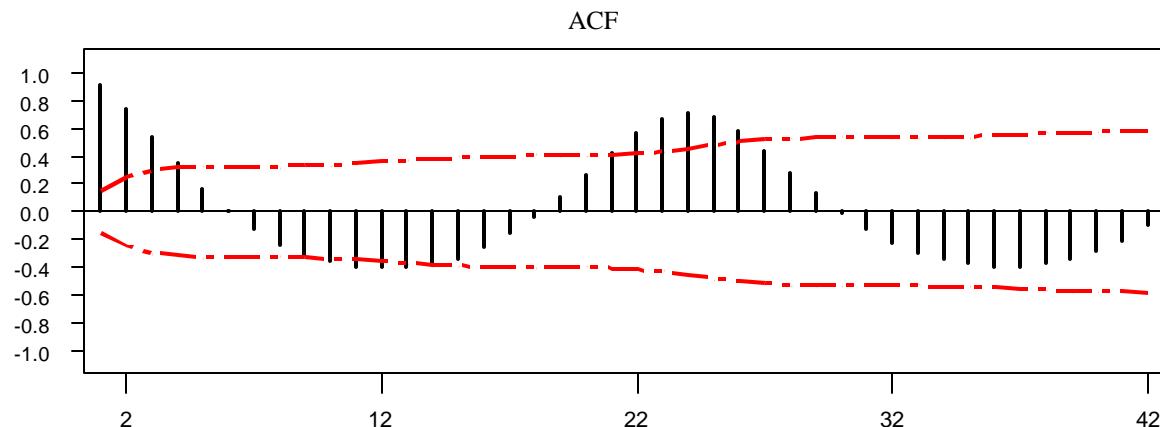
ACF of the Residuals

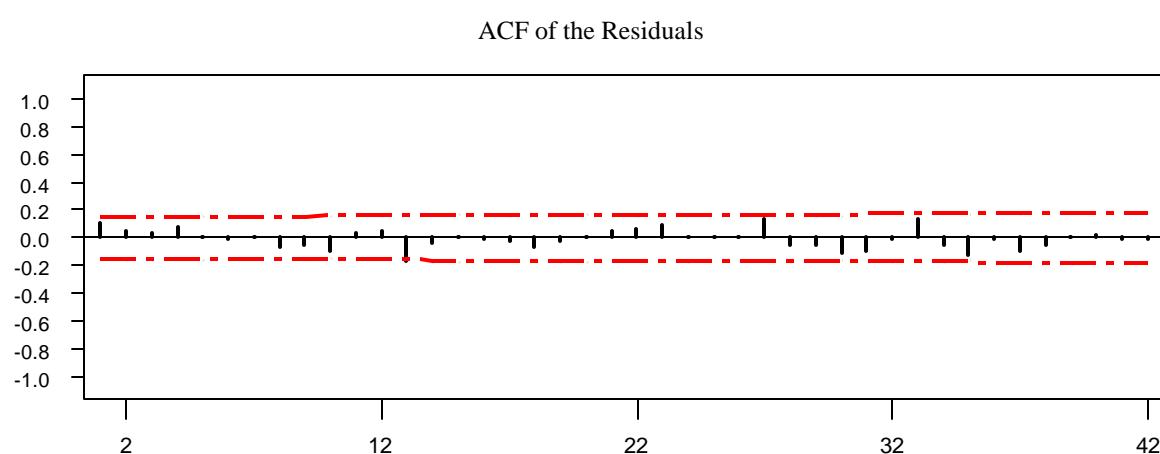
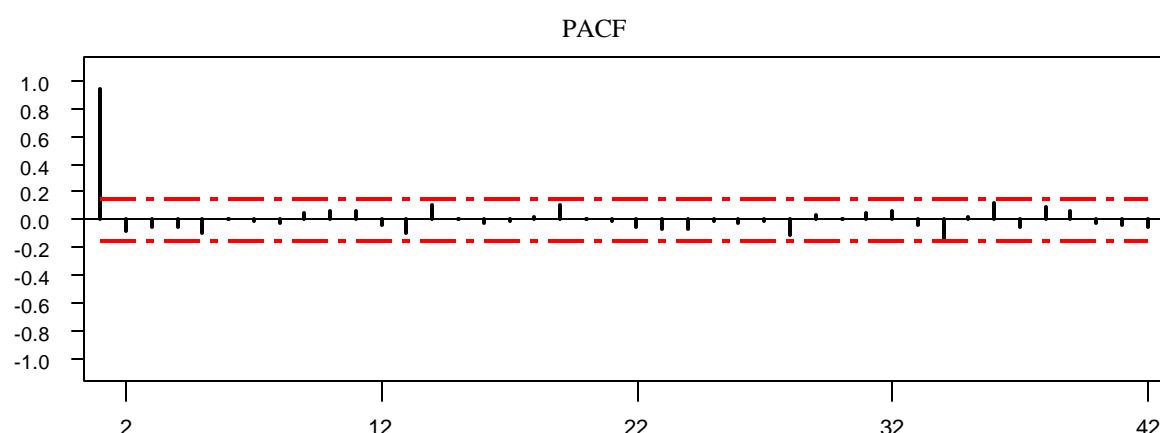
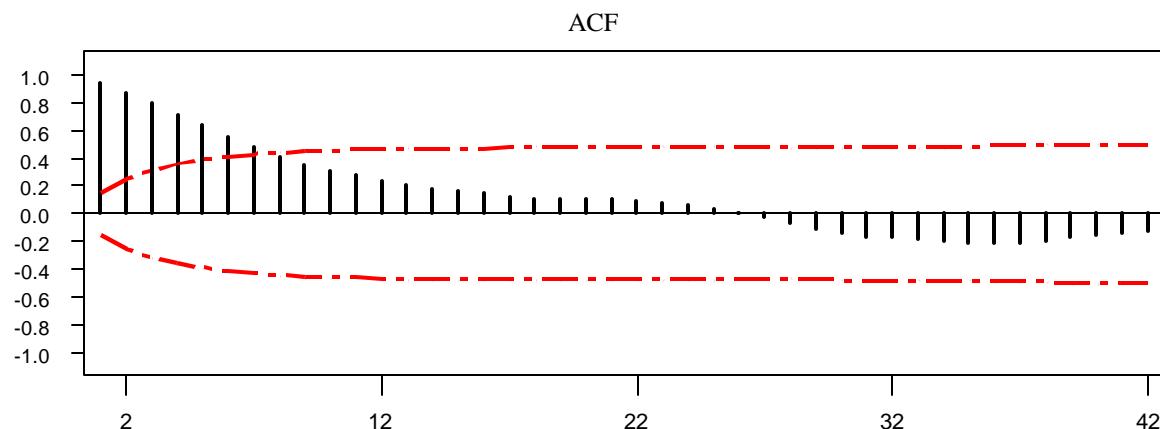


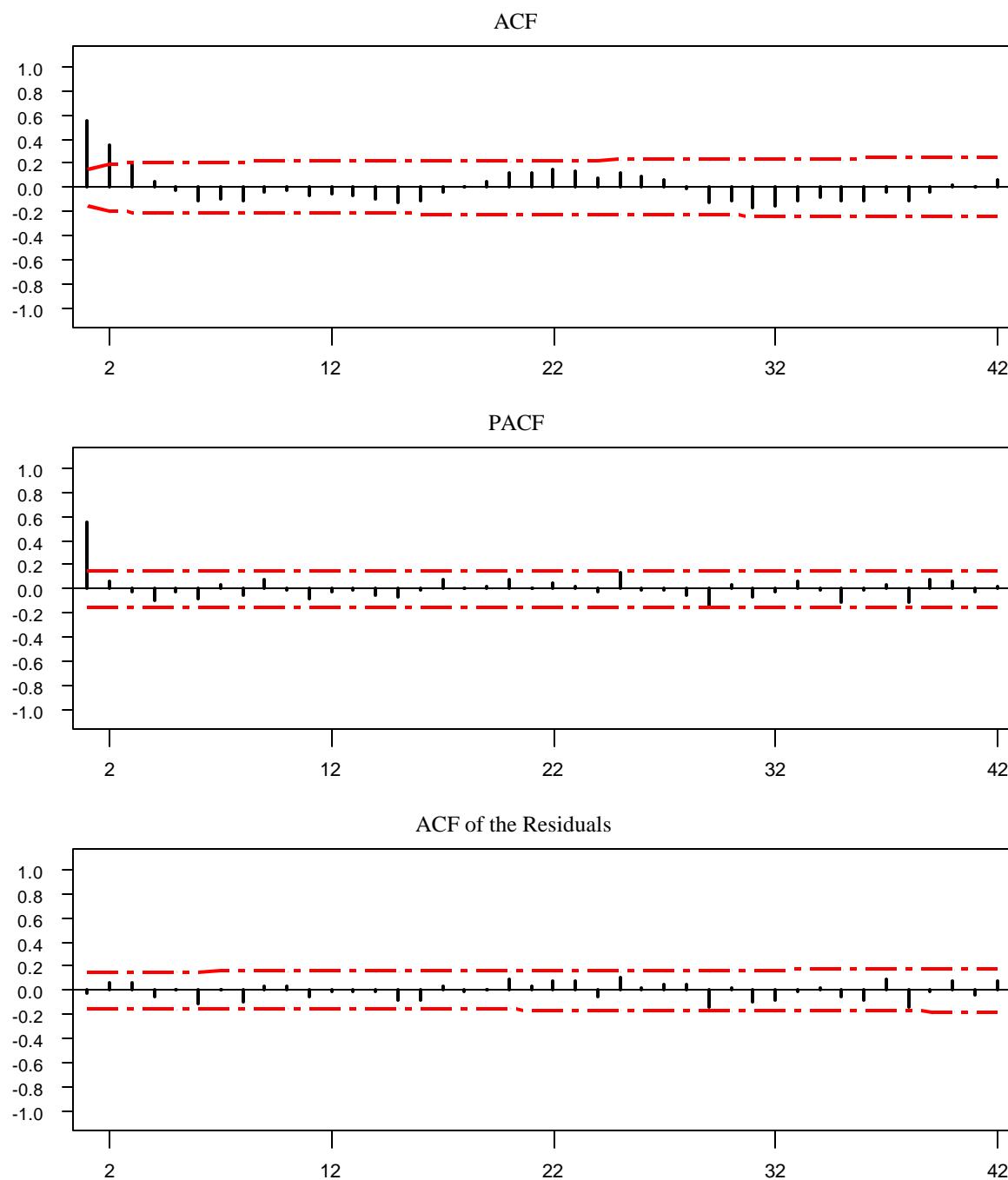
**Coincident Humidity Ratio****Albuquerque, NM**

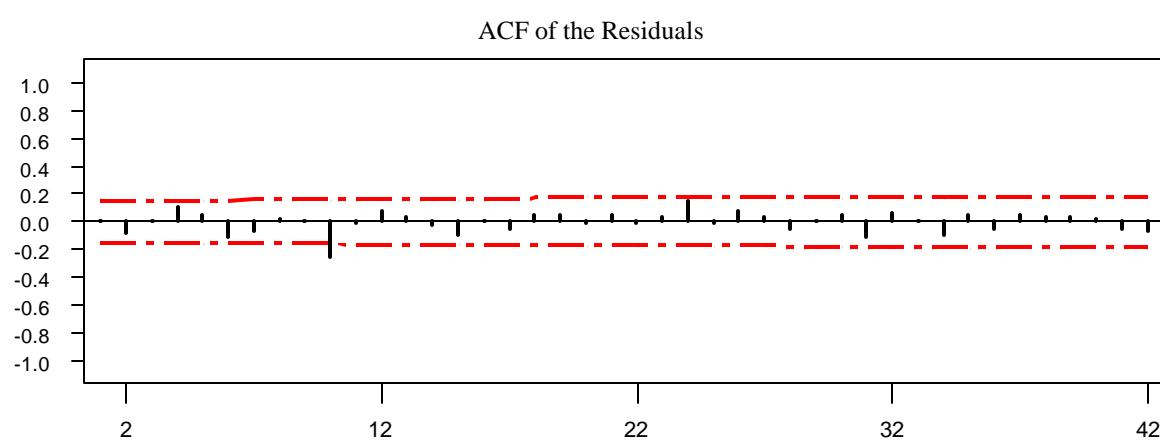
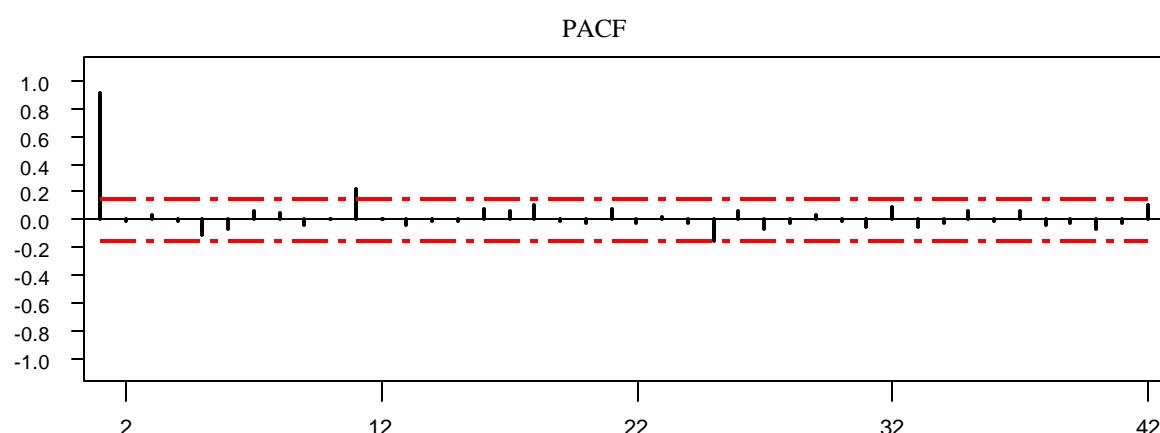
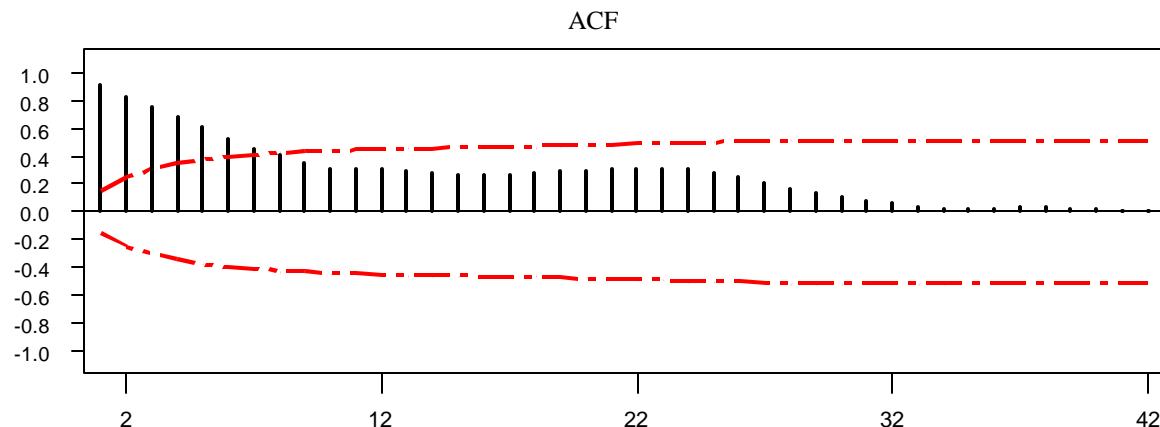
**Atlanta, GA**

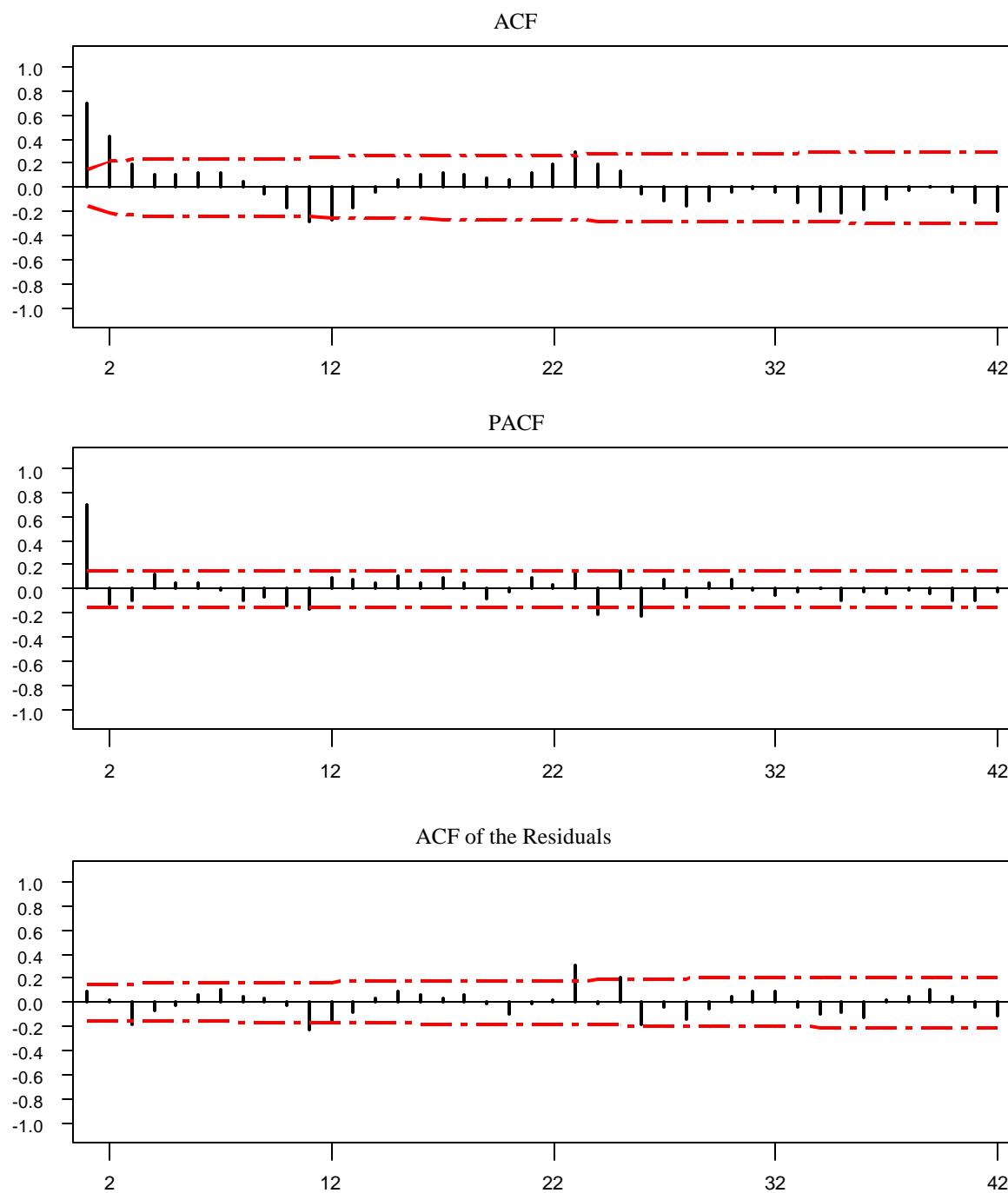
**Baltimore, MD**

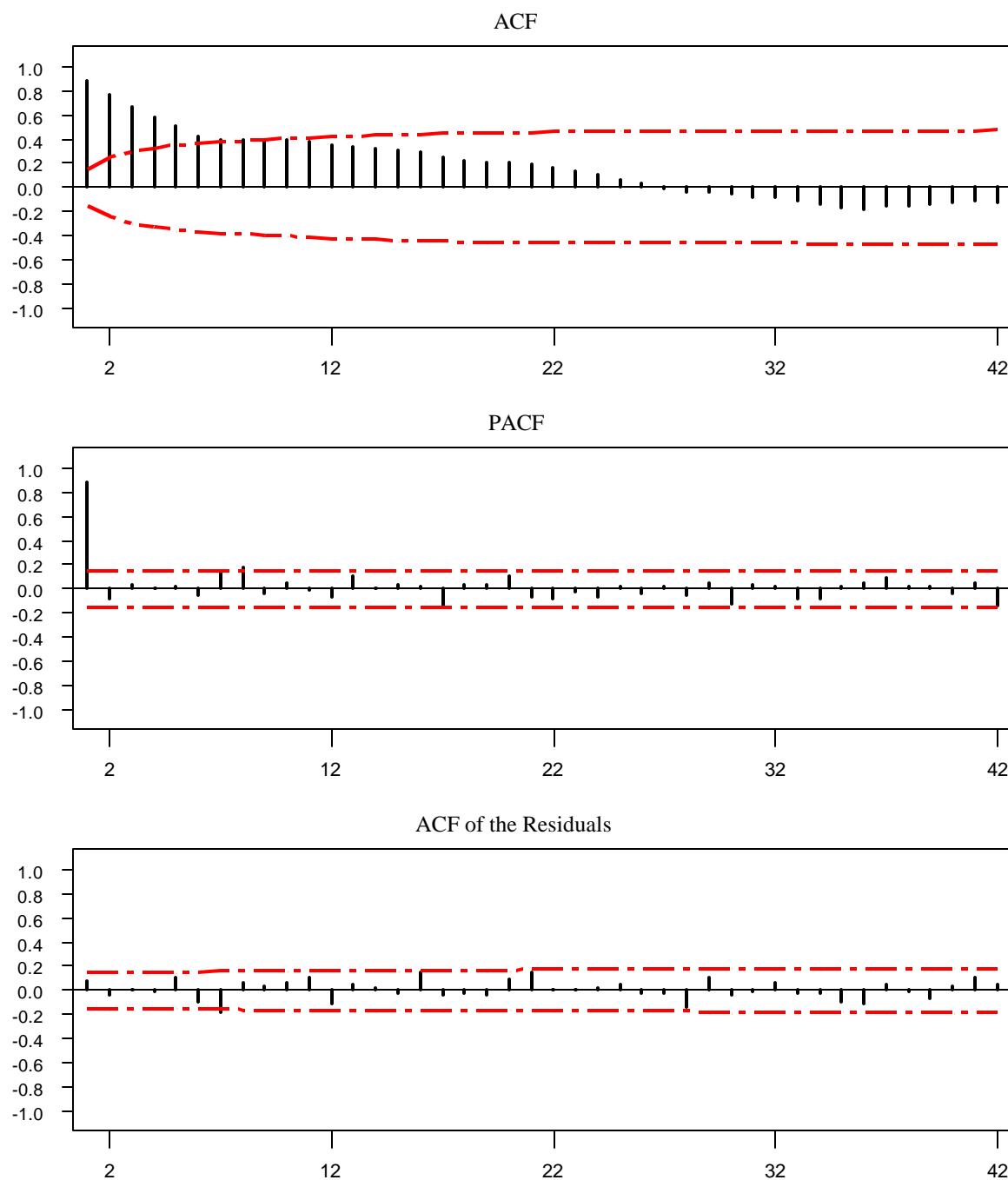
**Houston, TX**

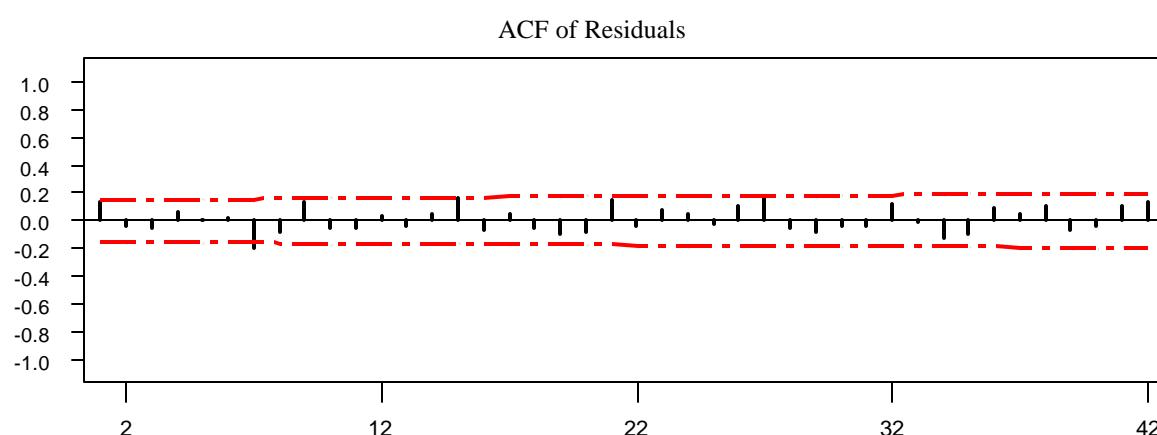
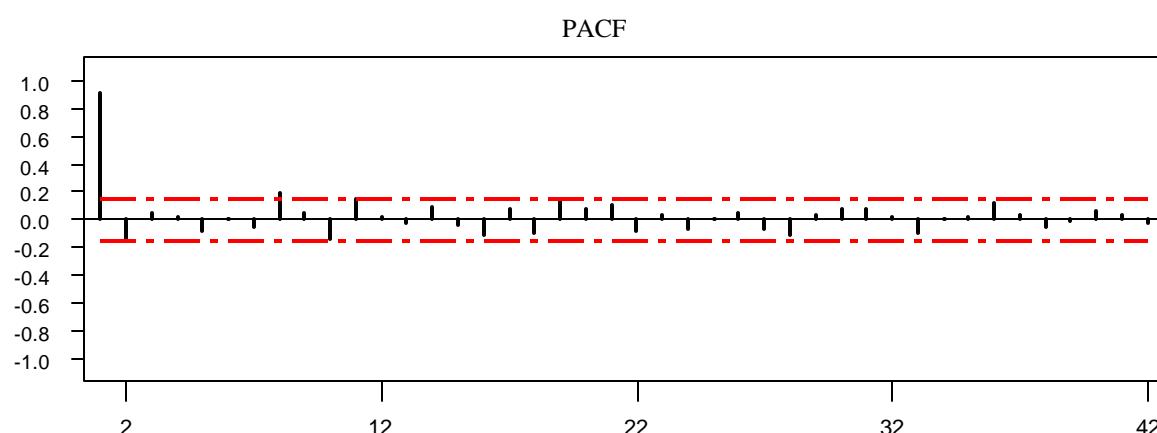
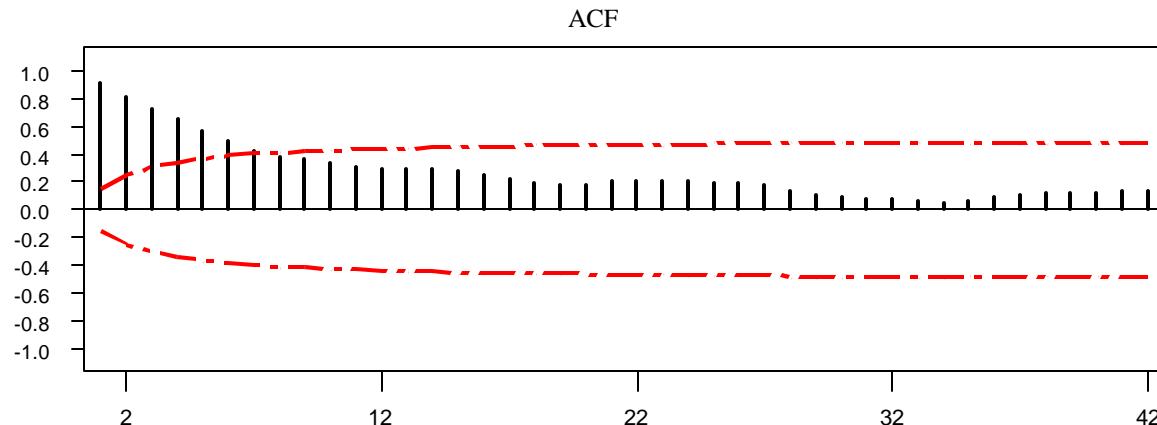
**Madison, WI**

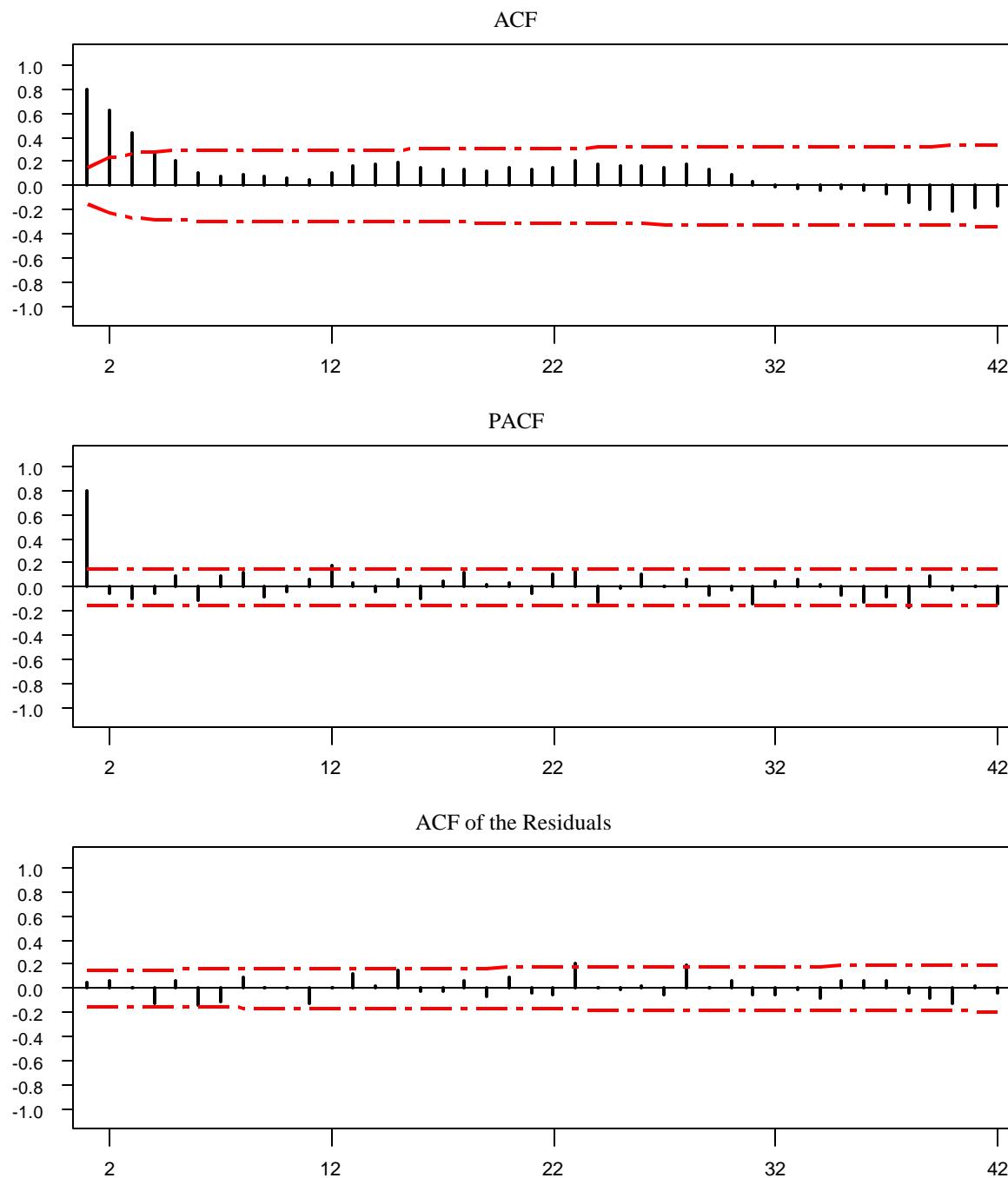
**Miami, FL**

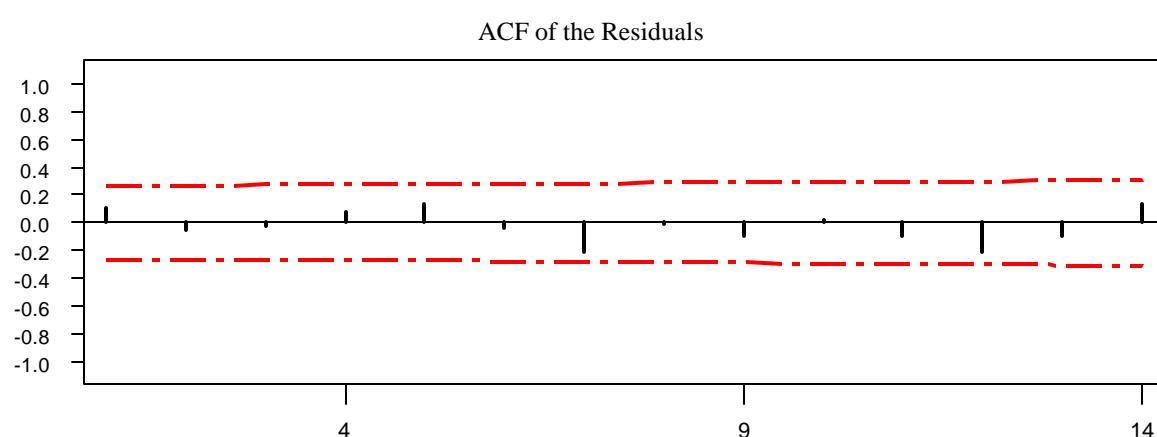
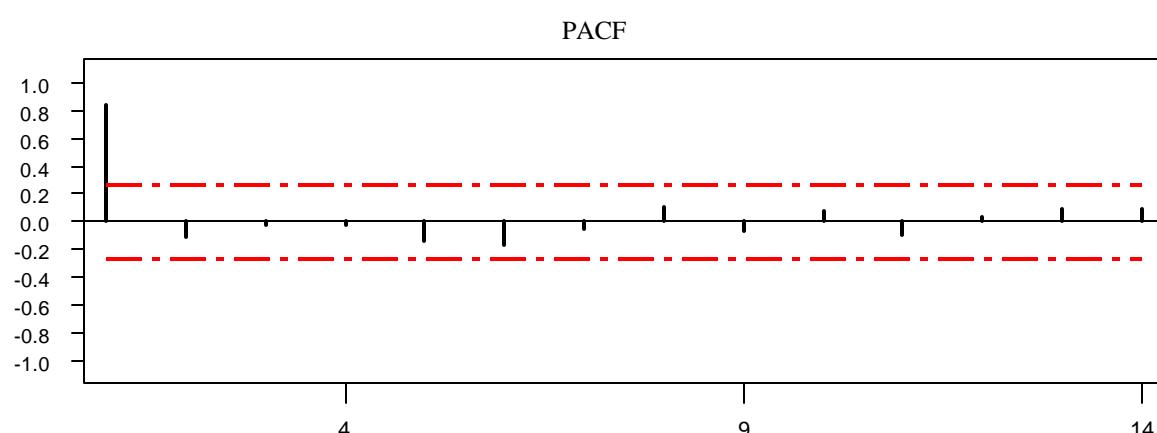
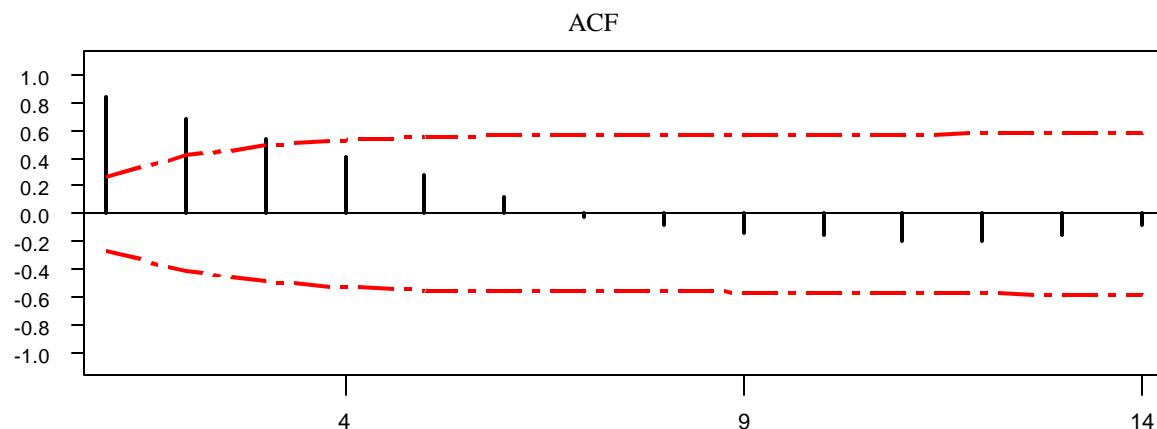
**Seattle, WA**

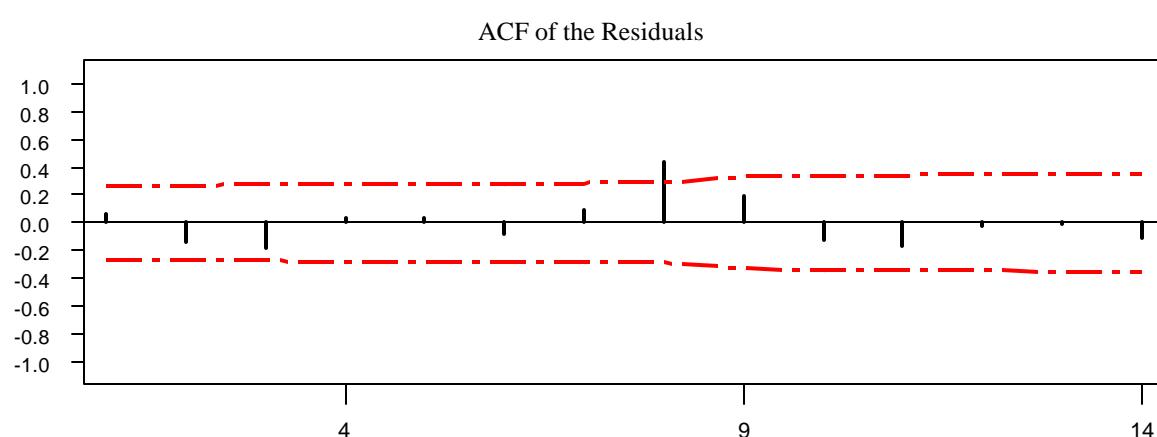
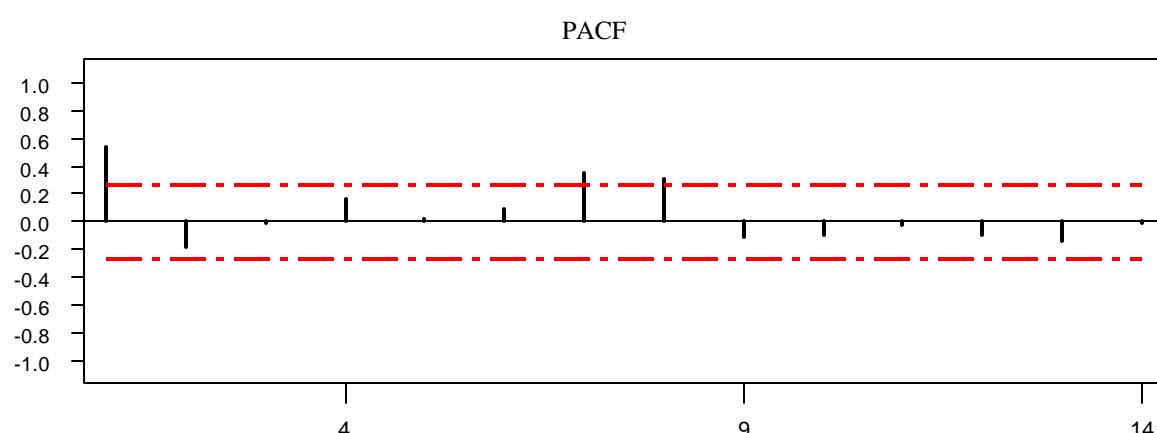
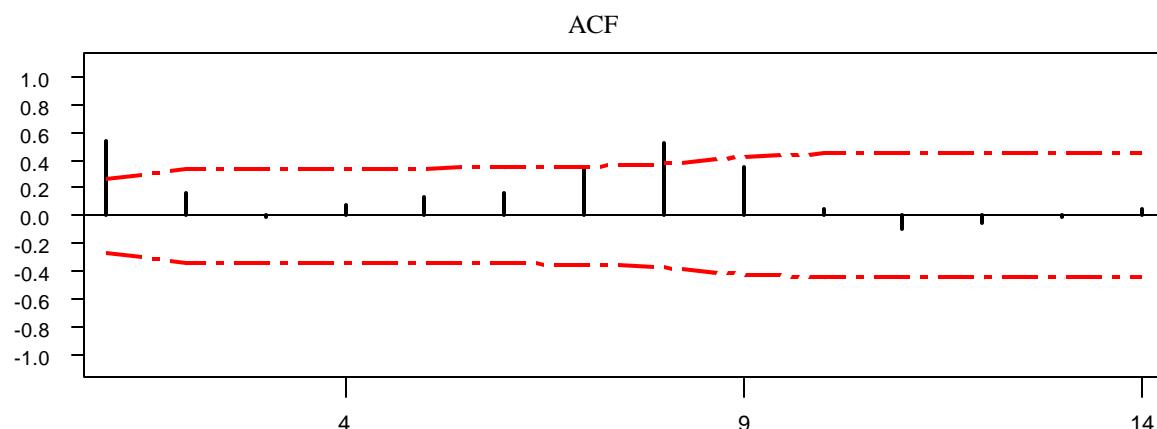
**Charleston, SC**

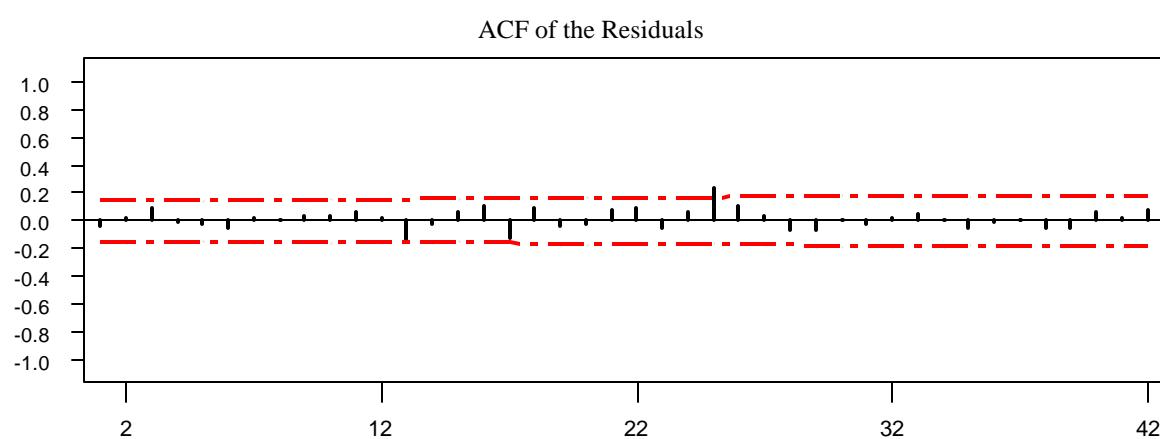
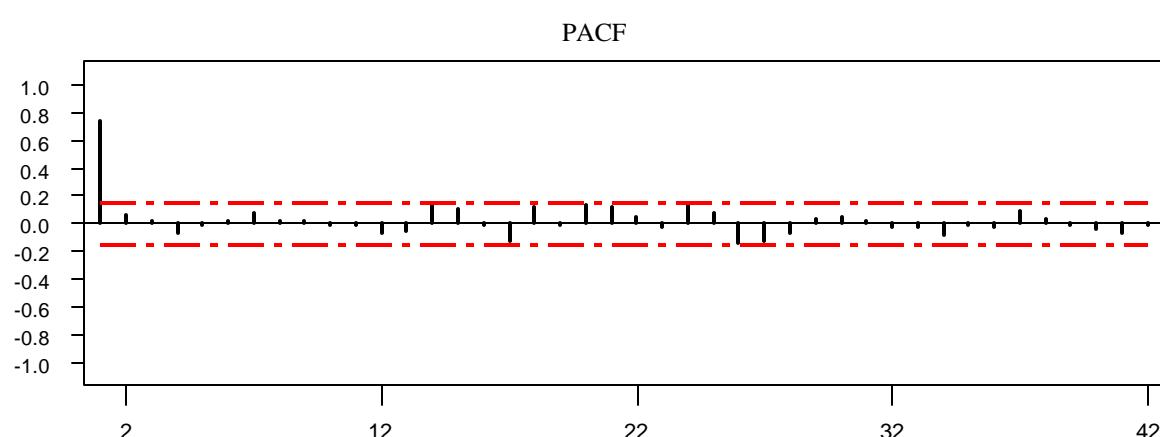
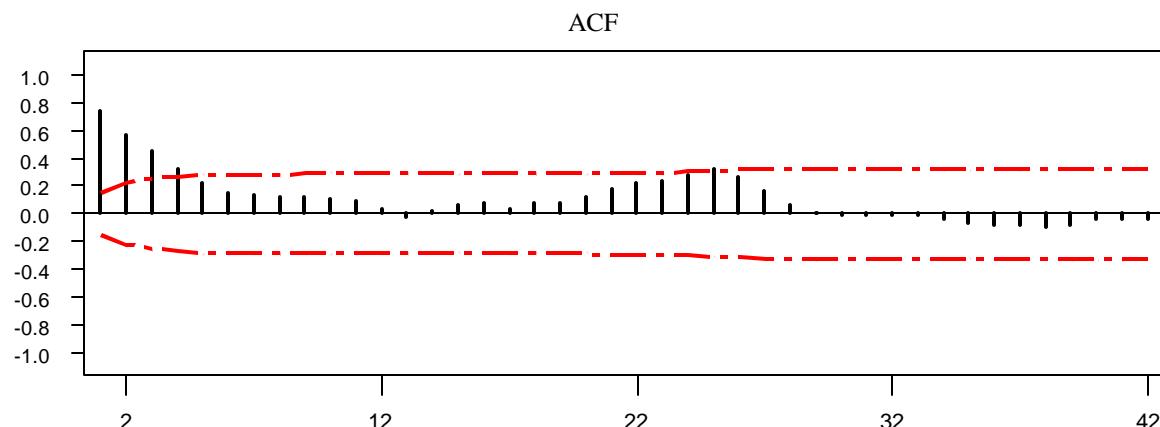
**Chicago, IL**

**Kansas, MO**

**Los Angeles, CA**

**New York, NY**

**San Francisco, CA**

**West Palm Beach, FL**

## **Appendix E**

### Computer Program Listings

---

Program Extr11 - Calculate average for each data window and create extreme summary sheet

Program Extr2x – Extract extreme sequence using using summary sheet

Sub-Program Psychro – Calculate humidity ratio from SAMSON data

```

program extr11
!-----
!      Utility Program #11 - Find sequence averages
!-----
implicit none
integer :: seqlen,numseq,i,badW,badDB,badWB,lastday,badWnd
integer :: year,month,day,hour,G,RH,StaPress,badG,j,k
integer :: maxDByear(1:7),maxDBday(1:7),maxWByear(1:7)
integer :: maxWBday(1:7),maxWyear(1:7),maxWday(1:7)
integer :: minDByear(1:7),minDBday(1:7),minWByear(1:7)
integer :: minWBday(1:7),minWyear(1:7),minWday(1:7)
integer :: minGyear(1:7),maxGyear(1:7),minGday(1:7),maxGday(1:7)
integer :: minWndyear(1:7),maxWndyear(1:7),minWnnday(1:7)
integer :: maxWnnday(1:7),goodG
character :: infile*20,outfile*20,ext*3,datatype*20
real :: DBtemp,DPtemp,WndSpd,avgseqW,avgseqDB,WBtemp,humratio,h
real :: avgseqWB,maxDB(1:7),maxWB(1:7),maxW(1:7),minDB(1:7)
real :: minWB(1:7),minW(1:7),minDB_W(1:7),maxDB_W(1:7)
real :: minW_DB(1:7),maxW_DB(1:7),minWB_DB(1:7),maxWB_DB(1:7)
real :: start_time,end_time,avgseqG,maxG(1:7),minG(1:7)
real :: maxG_DB(1:7),minG_DB(1:7),ExtraRad,daytotG
real :: minKt(1:7,1:7),maxKt(1:7,1:7),avgseqWnd,maxWnd(1:7)
real :: minWnd(1:7),minDB_Kt(1:7,1:7),maxDB_Kt(1:7,1:7)
real :: maxDB_G(1:7),minDB_G(1:7),Kt(1:7),Ho

!-----
!      Open files, Initialize variables
!-----
call cpu_time(start_time)

maxDB      = -999.0
minDB      = 999.0
avgseqDB   = 0.0
badDB      = 0

maxWB      = -999.0
minWB      = 999.0
avgseqWB   = 0.0
badWB      = 0

maxW       = -999.0
minW       = 999.0
avgseqW    = 0.0
badW       = 0

maxG       = -999.0
minG       = 9999.0
avgseqG   = 0.0
badG       = 0
goodG      = 0
j          = 1

maxWnd     = -999.0
minWnd     = 9999.0
avgseqWnd = 0.0

```

```

badWnd      = 0

open (3,file='files',status='old')
do
  read (3,2,end=50,err=50) infile
2   format (a10,x)

  if (infile == ' ') then
    goto 50
  end if

  datfile = infile(1:6)//'.out'
  open (4,file=datfile,status='unknown')

  print*, 'Processing File: ',infile
  do numseq=1,7
    select case (numseq)
    case (1)
      ext = '024'
    case (2)
      ext = '048'
    case (3)
      ext = '072'
    case (4)
      ext = '096'
    case (5)
      ext = '120'
    case (6)
      ext = '144'
    case (7)
      ext = '168'
    end select

    outfile = infile(1:6)//'.'//ext
    print*, 'Sequence Number: ',numseq
    seqlen = 24*numseq

    ! May need to change if other months are used
    lastday = 31

!-----!
!      Main Procedure
!-----
      open (1,file=infile,status='old')
      open (2,file=outfile,status='unknown')
      do
        do i=1,seqlen
1         read (1,5,end=20,err=20) year,month,day,hour,G,DBtemp,
          .                                         DPtemp,RH,StaPress,WndSpd,WBtemp,
          .                                         humratio,h
5         format (4(x,i2),3x,i4,3x,2(x,f6.1),x,i3,x,i4,4(x,f6.1))

        if (DBtemp > 900.0) then
          badDB = badDB+1
        else

```

```

        avgseqDB = avgseqDB+(1.8*DBtemp+32.0)
end if

if (WBtemp > 900.0) then
    badWB = badWB+1
else
    avgseqWB = avgseqWB+(1.8*WBtemp+32.0)
end if

if (humratio > 900.0) then
    badW = badW+1
else
    avgseqW = avgseqW+humratio
end if

if (G == 9999) then
    badG = badG+1
else
    if (G /= 0) then
        avgseqG = avgseqG+0.317*G ! btu/ft^2
        daytotG = daytotG+0.317*G
        goodG = goodG+1
    end if
end if

! Calculate the daily Kt
if (hour == 24) then
    Ho = ExtraRad(infile,month,day)
    Kt(j) = daytotG/Ho
    daytotG = 0.0
    j = j+1
end if

if (Wndspd > 90.0) then
    badWnd = badWnd+1
else
    avgseqWnd = avgseqWnd+Wndspd/0.447 ! mph
end if

end do

if (badDB == seqlen) then
    avgseqDB = 9999.0
else
    avgseqDB = avgseqDB/(seqlen-badDB)
end if

if (badWB == seqlen) then
    avgseqWB = 9999.0
else
    avgseqWB = avgseqWB/(seqlen-badWB)
end if

if (badW == seqlen) then
    avgseqW = 9999.0

```

```

else
    avgseqW = avgseqW/(seqlen-badW)
end if

    if (badG == seqlen) then
        avgseqG = 9999.0
    else
        avgseqG = avgseqG/(goodG-badG) ! btu/day-ft^2
    end if

    if (badWnd == seqlen) then
        avgseqWnd = 99.0
    else
        avgseqWnd = avgseqWnd/(seqlen-badWnd)
    end if

! Find max/min dry bulb sequence and coincident W and Kt
if (avgseqDB > maxDB(numseq) .and. avgseqDB /= 9999.0) then
    maxDB(numseq)      = avgseqDB
    maxDB_W(numseq)    = avgseqW
    do k=1,numseq
        maxDB_Kt(numseq,k) = Kt(k)
    end do
    maxDB_G(numseq)    = avgseqG
    maxDBYear(numseq)  = year
    maxDBday(numseq)   = day
end if
if (avgseqDB < minDB(numseq)) then
    minDB(numseq)      = avgseqDB
    minDB_W(numseq)    = avgseqW
    do k=1,numseq
        minDB_Kt(numseq,k) = Kt(k)
    end do
    minDB_G(numseq)    = avgseqG
    minDBYear(numseq)  = year
    minDBday(numseq)   = day
end if

! Find min/max wet bulb sequence and coincident dry bulb
if (avgseqWB > maxWB(numseq) .and. avgseqWB /= 9999.0) then
    maxWB(numseq)      = avgseqWB
    maxWB_DB(numseq)   = avgseqDB
    maxWBYear(numseq)  = year
    maxWBday(numseq)   = day
end if
if (avgseqWB < minWB(numseq)) then
    minWB(numseq)      = avgseqWB
    minWB_DB(numseq)   = avgseqDB
    minWBYear(numseq)  = year
    minWBday(numseq)   = day
end if

! Find max/min humidity ratio sequence and coincident dry bulb
if (avgseqW > maxW(numseq) .and. avgseqW /= 9999.0) then
    maxW(numseq)       = avgseqW

```

```

maxW_DB(numseq)      = avgseqDB
maxWyear(numseq)     = year
    maxWday(numseq)   = day
end if
if (avgseqW < minW(numseq)) then
    minW(numseq)      = avgseqW
    minW_DB(numseq)   = avgseqDB
    minWyear(numseq)  = year
    minWday(numseq)   = day
end if

! Find max/min solar sequence and coincident dry bulb
if (avgseqG > maxG(numseq) .and. avgseqG /= 9999.0) then
    maxG(numseq)      = avgseqG
    maxG_DB(numseq)   = avgseqDB
    maxGyear(numseq)  = year
    maxGday(numseq)   = day
    do k=1,numseq
        maxKt(numseq,k) = Kt(k)
    end do
end if
if (avgseqG < minG(numseq)) then
    minG(numseq)      = avgseqG
    minG_DB(numseq)   = avgseqDB
    minGyear(numseq)  = year
    minGday(numseq)   = day
    do k=1,numseq
        minKt(numseq,k) = Kt(k)
    end do
end if

! Find max/min wind sequence
if (avgseqWnd > maxWnd(numseq) .and. avgseqWnd /= 99.0) then
    maxWnd(numseq)      = avgseqWnd
    maxWndyear(numseq)  = year
    maxWndday(numseq)   = day
end if
if (avgseqWnd < minWnd(numseq)) then
    minWnd(numseq)      = avgseqWnd
    minWndyear(numseq)  = year
    minWndday(numseq)   = day
end if

write (2,15) year,day,avgseqDB,avgseqWB,avgseqW,avgseqG,
            avgseqWnd,(Kt(i),i=1,numseq)
format (2(x,i2),5(x,f6.1),7(x,f6.4))

avgseqDB = 0.0
badDB    = 0

avgseqWB = 0.0
badWB    = 0

avgseqW  = 0.0
badW     = 0

```

```

        avgseqG  = 0.0
        daytotG  = 0.0
        badG     = 0
        goodG    = 0
        j         = 1

        avgseqWnd = 0.0
        badWnd   = 0

        if (day /= lastday) then
            do i=1,24*(numseq-1)
                backspace (1)
            end do
        end if

        end do

20      close (1)
        close (2)

        end do

! Max dry bulb/coincident W
do i=1,7
    write (4,21) infile,i,maxDByear(i),maxDBday(i),maxDB(i),
.           maxDB_W(i)
. end do
write (4,45)

! Min dry bulb/coincident W
do i=1,7
    write (4,22) infile,i,minDByear(i),minDBday(i),minDB(i),
.           minDB_W(i)
. end do
write (4,45)

! Max W/coincident dry bulb
do i=1,7
    write (4,25) infile,i,maxWyear(i),maxWday(i),maxW(i),
.           maxW_DB(i)
. end do
write (4,45)

! Min W/coincident dry bulb
do i=1,7
    write (4,26) infile,i,minWyear(i),minWday(i),minW(i),
.           minW_DB(i)
. end do
write (4,45)

! Max G/coincident dry bulb
do i=1,7
    write (4,27) infile,i,maxGyear(i),maxGday(i),maxG(i),
.           maxG_DB(i),(maxKt(i,k),k=1,numseq-1)
.
```

```

end do
write(4,45)

! Min G/coincident dry bulb
do i=1,7
  write (4,28) infile,i,minGyear(i),minGday(i),minG(i),
.           minG_DB(i),(minKt(i,k),k=1,numseq-1)
end do
write (4,45)

! Max DB/coincident G
do i=1,7
  write (4,29) infile,i,maxDByear(i),maxDBday(i),maxDB(i),
.           maxDB_G(i),(maxDB_Kt(i,k),k=1,numseq-1)
end do
write (4,45)

! Min DB/coincident G
do i=1,7
  write (4,30) infile,i,minDByear(i),minDBday(i),minDB(i),
.           minDB_G(i),(minDB_Kt(i,k),k=1,numseq-1)
end do
write (4,45)

! Max wet bulb/coincident dry bulb
do i=1,7
  write (4,23) infile,i,maxWByear(i),maxWBday(i),maxWB(i),
.           maxWB_DB(i)
end do
write (4,45)

! Min wet bulb/coincident dry bulb
do i=1,7
  write (4,24) infile,i,minWByear(i),minWBday(i),minWB(i),
.           minWB_DB(i)
end do
write(4,45)
! Max Wind
do i=1,7
  write (4,31) infile,i,maxWndyear(i),maxWndday(i),maxWnd(i)
end do
write (4,45)

! Min Wind
do i=1,7
  write (4,32) infile,i,minWndyear(i),minWndday(i),minWnd(i)
end do

21   format (x,a20,i1,x,' DB/MHR : ',2(x,i2),2(x,f6.1))
22   format (x,a20,i1,x,' DB/MHR : ',2(x,i2),2(x,f6.1))
23   format (x,a20,i1,x,' WB/MDB : ',2(x,i2),2(x,f6.1))
24   format (x,a20,i1,x,' WB/MDB : ',2(x,i2),2(x,f6.1))
25   format (x,a20,i1,x,' HR/MDB : ',2(x,i2),2(x,f6.1))
26   format (x,a20,i1,x,' HR/MDB : ',2(x,i2),2(x,f6.1))

```

```

27      format (x,a20,i1,x,' G/MDB : ',2(x,i2),x,f6.1,x,f6.1,7(x,f3.2))
28      format (x,a20,i1,x,' G/MDB : ',2(x,i2),x,f6.1,x,f6.1,7(x,f3.2))
29      format (x,a20,i1,x,' DB/MG : ',2(x,i2),x,f6.1,x,f6.1,7(x,f3.2))

30      format (x,a20,i1,x,' DB/MG : ',2(x,i2),x,f6.1,x,f6.1,7(x,f3.2))
31      format (x,a20,i1,x,' Wind   : ',2(x,i2),x,f6.1)
32      format (x,a20,i1,x,' Wind   : ',2(x,i2),x,f6.1)
45      format ('')
           close (4)

! Reinitialize the arrays
maxDB      = -999.0
minDB      = 999.0
avgseqDB  = 0.0
badDB      = 0

maxWB      = -999.0
minWB      = 999.0
avgseqWB  = 0.0
badWB      = 0

maxW       = -999.0
minW       = 999.0
avgseqW   = 0.0
badW       = 0

maxG       = -999.0
minG       = 9999.0
avgseqG   = 0.0
daytotG   = 0.0
badG       = 0
goodG      = 0
j          = 1

maxWnd     = -999.0
minWnd     = 9999.0
avgseqWnd = 0.0
badWnd     = 0

end do

50      close (3)

call cpu_time(end_time)
print*, 'Run Time :',(end_time-start_time)/60.0,' minutes'

end program extr11

function ExtraRad(infile,month,day) result(Ho)
!-----
!      Calculate the extraterrestrial radiation on a horizontal
!      surface for day. Used to compute the daily Kt
!-----
implicit none

```

```

integer :: i,month,day,numseq,day_number
real:: delta_rad,omega_s_rad,phi_rad,delta_deg,omega_s_deg
real:: phi_deg,pi,Ho
character :: infile*10,city*3

Ho      = 0.0
pi     = 4.0*atan(1.0)
city   = infile(1:3)

select case (city)
  case ('alb')
    phi_deg = 35.1
  case ('atl')
    phi_deg = 33.7
  case ('bal')
    phi_deg = 39.2
  case ('cha')
    phi_deg = 32.9
  case ('chi')
    phi_deg = 41.8
  case ('hou')
    phi_deg = 30.0
  case ('kan')
    phi_deg = 39.3
  case ('los')
    phi_deg = 33.9
  case ('mad')
    phi_deg = 43.1
  case ('mia')
    phi_deg = 25.8
  case ('new')
    phi_deg = 40.8
  case ('san')
    phi_deg = 37.6
  case ('sea')
    phi_deg = 47.5
  case ('wes')
    phi_deg = 26.7
  case default
    print*, 'City not found.'
end select

select case (month)
  case (1)
    day_number = day
  case (3)
    day_number = 59+day
  case (7)
    day_number = 181+day
  case (10)
    day_number = 273+day
end select

! radians
delta_rad = 0.4093*sin(2.0*pi*(284.0+float(day_number))/365.0)

```

```
omega_s_rad = acos(-tan(pi/180.0*phi_deg)*tan(delta_rad))
phi_rad      = pi/180.0*phi_deg

! btu/ft^2
Ho = (88.06e-6)*(24.0*3600.0*1367.0/pi)*
.   (1.0+0.033*cos(2.0*pi*float(day_number)/365.0))* 
.   (cos(phi_rad)*cos(delta_rad)*sin(omega_s_rad)+ 
.     omega_s_rad*sin(phi_rad)*sin(delta_rad))

end function ExtraRad
```

```

program extr2x

!-----  

!      Utility Program #2x - Pick off period (year, month or day)  

!      where extreme occurred using the file  

!      that contains the raw SAMSON data with  

!      the wb temp, humidity ratio and enthalpy  

!      and calculates the hourly kt.  

!-----  

! Define Variables  

!-----  

implicit none  

integer :: i,index,period,seqlen  

integer :: year1,day1,hour,G,RH,StaPress  

integer :: year2,month2,day2  

character :: infile*10,outfile*12,seqtype*6,extfile*10  

character :: minmax*1,length*1  

real :: DBtemp,DPtemp,WndSpd,WBtemp,W,h,kt,Io,ExtraRad  

!-----  

! Get the location, month, sequence length and type  

!-----  

open (1,file='files2x',status='old')  

do  

  read (1,2,end=20,err=20) infile,length,seqtype,minmax  

2    format (a10,x,a1,x,a6,x,a1)  

  if (infile == ' ') then  

    goto 20  

  end if  

  read (length,*) seqlen  

  select case (seqtype)  

  case ('DB/MHR')  

    if (minmax == 'H') then  

      index = (0*8)+seqlen  

    else  

      index = (1*8)+seqlen  

    end if  

  case ('HR/MDB')  

    if (minmax == 'H') then  

      index = (2*8)+seqlen  

    else  

      index = (3*8)+seqlen  

    end if  

  case ('G_/MDB')  

    if (minmax == 'H') then  

      index = (4*8)+seqlen  

    else  

      index = (5*8)+seqlen  

    end if  

  case ('DB/_MG')  

    if (minmax == 'H') then  

      index = (6*8)+seqlen

```

```

        else
            index = (7*8)+seqlen
        end if
    case ('WB/MDB')
        if (minmax == 'H') then
            index = (8*8)+seqlen
        else
            index = (9*8)+seqlen
        end if
    case ('Wind')
        if (minmax == 'H') then
            index = (10*8)+seqlen
        else
            index = (11*8)+seqlen
        end if
    case default
        print*, 'Sequence type not found.'
    end select

!-----
!      Get year and day of end of sequence
!-----
extfile = infile(1:5)//'x.out'
open (4,file=extfile,status='old')
do i=1,index
    read(4,3) year1,day1
    format (34x,i2,x,i2)
end do
close (4)

day1      = day1-(seqlen-1)
period    = 24*seqlen
outfile = infile(1:5)//seqtype(1:2)//seqtype(5:6)//'.' //length//minmax
open (2,file=infile,status='old')
open (3,file=outfile,status='unknown')
print*, 'Processing File: ',infile

!-----
!      Main Procedure
!-----
do
    read (2,5,end=20,err=20) year2,month2,day2,hour,G,DBtemp,
                           DPtemp,RH,StaPress,WndSpd,WBtemp,W,h
5      format (4(x,i2),3x,i4,3x,2(x,f6.1),x,i3,x,i4,4(x,f6.1))
!-----
!      Match the period
!-----
        if (year1 .eq. year2 .and. day1 .eq. day2) then
!-----
!      Get data for the period
!-----
        do i=1,period

            if (G > 0) then

```

```

      Io = ExtraRad(infile,month2,day2,hour)
          kt = 3600.0*G/Io
      else
          kt = 0.0
      end if

          if (kt > 1.0 .or. kt < 0.0) then
          kt = 0.0
          end if

      write (3,6) year2,month2,day2,hour,G,DBtemp,
.           DPtemp,RH,StaPress,WndSpd,WBtemp,W,h,kt
6       format (4(x,i2),3x,i4,3x,2(x,f6.1),x,i3,x,i4,4(x,f6.1),
.           x,f6.3)

      read (2,5,end=20,err=20)year2,month2,day2,hour,G,DBtemp,
.           DPtemp,RH,StaPress,WndSpd,
.           WBtemp,W,h
      end do
      exit
      end if
  end do

  close (2)
  close (3)

end do

20  close (1)

end program extr2x

function ExtraRad(infile,month,day,hour) result(Io)
!-----
!     Calculate the extraterrestrial radiation on a horizontal
!     surface for an hour period. Used to compute the hourly kt.
!-----
implicit none
integer :: month,day,hour,day_number
real :: delta_rad,phi_rad,delta_deg
real :: phi_deg,pi,Io,long_deg,std_mer,hour1,hour2,omegal_rad
real :: omega2_rad,SolarCorr,HourAng,omega_s
character :: infile*10,city*3

Io      = 0.0
pi      = 4.0*atan(1.0)
city    = infile(1:3)

select case (city)
  case ('alb')
    phi_deg  = 35.1
    long_deg = 106.6
    std_mer  = 105.0
  case ('atl')
    phi_deg  = 33.7

```

```

long_deg = 84.4
      std_mer = 75.0
case ('bal')
  phi_deg = 39.2
    long_deg = 76.7
    std_mer = 75.0
case ('cha')
  phi_deg = 32.9
    long_deg = 80.0
    std_mer = 75.0
case ('chi')
  phi_deg = 41.8
    long_deg = 87.8
    std_mer = 90.0
case ('hou')
  phi_deg = 30.0
    long_deg = 95.3
    std_mer = 90.0
case ('kan')
  phi_deg = 39.3
    long_deg = 94.6
    std_mer = 90.0
case ('los')
  phi_deg = 33.9
    long_deg = 118.4
    std_mer = 120.0
case ('mad')
  phi_deg = 43.1
    long_deg = 89.3
    std_mer = 90.0
case ('mia')
  phi_deg = 25.8
    long_deg = 80.3
    std_mer = 75.0
case ('new')
  phi_deg = 40.8
    long_deg = 74.0
    std_mer = 75.0
case ('san')
  phi_deg = 37.6
    long_deg = 122.4
    std_mer = 120.0
case ('sea')
  phi_deg = 47.5
    long_deg = 122.3
    std_mer = 120.0
case ('wes')
  phi_deg = 26.7
    long_deg = 80.1
    std_mer = 75.0
case default
  print*, 'City not found.'
end select

select case (month)

```

```

    case (1)
        day_number = day
    case (3)
        day_number = 59+day
    case (7)
        day_number = 181+day
    case (10)
        day_number = 273+day
    end select

    ! Convert local time to solar time
    hour2 = float(hour)+4.0*(std_mer-long_deg)/60.0+
.          SolarCorr(day_number)
    hour1 = float(hour-1)+4.0*(std_mer-long_deg)/60.0+
.          SolarCorr(day_number)

    ! Convert to hour angle
    omega2_rad = HourAng(hour2)*pi/180.0
    omegal_rad = HourAng(hour1)*pi/180.0

    ! radians
    delta_rad = 0.4093*sin(2.0*pi*(284.0+float(day_number))/365.0)
    phi_rad = pi/180.0*phi_deg
    omega_s = acos(-tan(phi_rad)*tan(delta_rad))

    ! Make sure hour2 is < sunset angle
    if (omega2_rad > omega_s) then
        omega2_rad = omega_s
    end if

    ! J/m^2
    Io = (12.0*3600.0*1367.0/pi)*
.      (1.0+0.033*cos(2.0*pi*float(day_number)/365.0))**
.      (cos(phi_rad)*cos(delta_rad)*
.      (sin(omega2_rad)-sin(omegal_rad))+*
.      ((omega2_rad-omegal_rad)*sin(phi_rad)*sin(delta_rad)))

    !print*,Io/1.e6

    end function ExtraRad

    function SolarCorr(day_number) result(E)
!-----
!      Convert local time to solar time
!-----
    implicit none
    integer :: day_number
    real:: B,E,pi

    pi = 4.0*atan(1.0)
    B = float(day_number-1)*2.0*pi/365.0
    E = 229.2*(0.000075+0.001868*cos(B)-0.032077*sin(B)-
.             0.014615*cos(2.0*B)-0.04089*sin(2.0*B))
    E = E/60.0 ! convert to hours

```

```
end function SolarCorr

function HourAng(hour) result(omega)
!----- Convert hour to hour angle
!----- implicit none
real :: hour,omega

if (hour <= 12) then
    omega = -15.0*(12.0-hour)
else
    omega = 15.0*(hour-12.0)
end if

end function HourAng
```

```

subroutine psychro(input,output)
!
!   input[1]  dry bulb temp [F]
!           [2]  dew point temp [F]
!           [3]  station pressure [millibars]
!
!   output[1] wb_temp [F]
!           [2] W, humidity ratio
!           [3] h, enthalpy [btu/lb]
!           [4] RH, relative humidity [%]
!-----
implicit none
real*8 wb_temp,db_temp,enthalpy,W_act,RelHum,RH
real*8 stn_press,wet_bulb,dp_temp,W,h
real*8 input(3),output(4)

db_temp    = input(1)
dp_temp    = input(2)
stn_press = input(3)*0.1d0/6.895d0 ! convert from mBar to psia

!get the wet bulb [F]
wb_temp = wet_bulb(db_temp,dp_temp,stn_press)
output(1) = wb_temp

!get the humidity ratio
W_act = W(db_temp,wb_temp,stn_press)
output(2) = W_act

!get the enthalpy [btu/lb]
h = enthalpy(db_temp,W_act)
output(3) = h

!get the relative humidity
RH = RelHum(db_temp,W_act,stn_press)
output(4) = RH
end subroutine psychro

!-----
! FUNCTION p_sat
!
!   inputs  : db_temp [deg F]
!
!   outputs : p_ws      [psia]
!-----
function p_sat(temp) result(p_ws)

implicit none
real*8 temp,p_ws,temp_abs

temp_abs = temp+459.67d0

if (temp_abs < 491.67d0) then
  p_ws = exp((-1.0214165e+04)/temp_abs          +
             (-4.8932428e+00)                  +
             (-5.3765794e-03)*temp_abs       +

```

```

.
.          ( 1.9202377e-07)*temp_abs**2  +
.          ( 3.5575832e-10)*temp_abs**3  +
.          (-9.0344688e-14)*temp_abs**4  +
.          ( 4.1635019e+00)*log(temp_abs) )
else
    p_ws = exp((-1.0440397e+04)/temp_abs      +
.              (-1.1294650e+01)                  +
.              (-2.7022355e-02)*temp_abs      +
.              ( 1.2890360e-05)*temp_abs**2  +
.              (-2.4780681e-09)*temp_abs**3  +
.              ( 6.5459673e+00)*log(temp_abs) )
end if

end function p_sat

!-----
! FUNCTION W_sat
!
!   inputs  : stn_press [psia]
!             p_ws [psia]
!
!   outputs : W_s
!-----
function W_sat(p_ws,stn_press) result(W_s)
implicit none
real*8 p_ws,stn_press,W_s

W_s = (18.d0/29.d0)*p_ws/(stn_press-p_ws)

end function W_sat

!-----
! FUNCTION wet_bulb
!
!   inputs  : db_temp [F]
!             dp_temp [F]
!             stn_press [psia]
!
!   outputs : wb_temp [F]
!-----
function wet_bulb(db_temp,dp_temp,stn_press) result(wb_temp)
implicit none
integer i
real*8 db_temp,dp_temp,stn_press,p_ws_dp,W_dp,p_sat,W_sat
real*8 wb_temp,wb_temp_lo,wb_temp_hi,wb_temp_guess,W_guess,W

! get the water saturation pressure at the dew point
p_ws_dp = p_sat(dp_temp)

! get the humidity ratio at saturation at the dew point
W_dp = W_sat(p_ws_dp,stn_press)

! provide initial guess values
wb_temp_lo = dp_temp
wb_temp_hi = db_temp

```

```

wb_temp_guess = wb_temp_lo+(wb_temp_hi-wb_temp_lo)/2.d0

! iterate to find the wet bulb temp
i = 0
do while (wb_temp_hi-wb_temp_lo > 0.001)
    W_guess = W(db_temp,wb_temp_guess,stn_press)
    if (W_guess > W_dp) then
        wb_temp_hi      = wb_temp_guess
        wb_temp_guess   = wb_temp_lo+(wb_temp_hi-wb_temp_lo)/2.d0
    else
        wb_temp_lo      = wb_temp_guess
        wb_temp_guess   = wb_temp_lo+(wb_temp_hi-wb_temp_lo)/2.d0
    end if
    i = i+1
    if (i > 100) then
        print*, 'Number of Iterations exceeds 100'
        exit
    end if
end do

wb_temp = wb_temp_guess

end function wet_bulb

!-----
! FUNCTION W - Calculate the humidity ratio using
!
!   inputs  : db_temp [F]
!             wb_temp [F]
!             stn_press [psia]
!
!   outputs : W
!-----
function W(db_temp,wb_temp,stn_press) result(W_act)
implicit none
real*8 db_temp,wb_temp,stn_press,p_ws_wb,W_s_star,W_act
real*8 p_sat,w_sat,num,den

! saturation press at the wet bulb temp
p_ws_wb = p_sat(wb_temp)

! humidity ratio at the wet bulb temp
W_s_star = W_sat(p_ws_wb,stn_press)

! humidity ratio at actual dry and wet bulb temps
num = (1093.d0-0.556d0*wb_temp)*W_s_star-0.24d0*(db_temp-wb_temp)
den = 1093.d0+0.444d0*db_temp-wb_temp
W_act=num/den

end function W

```

```
!-----  
! FUNCTION enthalpy - Calculate the enthalpy  
!  
!   inputs  : db_temp [F]  
!             W  
!  
!   outputs : h    [btu/lb]  
!-----  
function enthalpy(db_temp,W) result(h)  
implicit none  
real*8 h,db_temp,W  
  
h = 0.24d0*db_temp+W*(1061.d0+0.444d0*db_temp)  
  
end function enthalpy  
  
!-----  
! FUNCTION RH - Calculate the relative humidity  
!  
!   inputs  :  
!  
!  
!   outputs :  
!-----  
function RelHum(db_temp,W_act,stn_press) result(RH)  
implicit none  
real*8 RH,p_ws,db_temp,W_act,W_sat,stn_press,W_s,mu,p_sat  
  
p_ws = p_sat(db_temp)  
W_s = W_sat(p_ws,stn_press)  
mu = W_act/W_s  
RH = 100.d0*(mu/(1.d0-(1.d0-mu)*(p_ws/stn_press)))  
  
end function RelHum
```

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