

SOLAR RADIATION DATA ANALYSIS

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This thesis reevaluates three fundamental concepts concerning the mathematical modeling of solar energy:

- 1) calculating solar radiation on a tilted surface from horizontal data;
- 2) analyzing the distribution of solar energy within a month; and
- 3) calculating the "utilizable energy" within a month.

One year of radiation data collected by Universities in San Antonio, Texas and in Albany, New York provided the basis for this study. Total solar insolation data were measured every minute and recorded on magnetic tape, for eight surface orientations. Normal incident beam radiation, various spectral ranges, and ambient conditions were also measured and recorded.

Modeling tilted surface radiation from horizontal data requires the calculation of a diffuse to total radiation fraction. The largest error in estimating monthly-average daily diffuse fractions from Erbs' [5] hourly diffuse fraction correlation was 10%. Typical errors were approximately 4%. Comparing individual hourly values from Erbs' correlation to data showed typical monthly RMS errors around 0.18, with a maximum RMS error of 0.32.

The isotropic hourly model, Hay [8] anisotropic hourly model, and hourly data values of tilted to horizontal surface radiation values were compared. For south-facing surfaces at a slope equal to the latitude, the isotropic model underestimated actual values by as much as 10%. In comparison, the Hay model provided better estimates of the radiation ratio for 23 of the 24 months studied. The worst performance was an underestimation by 6%. For all south-facing surfaces, the largest isotropic model errors occurred during winter months, with underestimations as large as 18%.

The distribution of solar energy within a month can be described by a "clearness frequency distribution". The minute clearness frequency distributions for hourly periods within a month show more variability in insolation levels than the presently used long-term hourly distributions. Variability in hourly distributions with the same monthly-average hourly clearness index indicates the potential need for modeling distributions with more than one independent parameter.

Monthly-average hourly and daily utilizability values calculated from hour data and Clark's [2] hourly correlation were compared to minute data values. An RMS error of 0.02 or less indicated a pair of approximately identical utilizability curves. Hour data values calculated for surface slopes equal to the latitude exceeded this RMS error for half of the months studied. Typically, surfaces receiving large amounts of normal incident beam radiation show the largest dif-

ferences between hour and minute data values. Three versions of Clark's correlation were compared to the minute data values, to check for errors resulting from: the monthly-average hourly isotropic radiation ratio model; the symmetrical day insolation assumption; and a correlation modeled from long-term data versus a short-term data base. The largest source of error in Clark's correlation was typically from the isotropic radiation ratio model, using Erb's monthly-average daily diffuse fraction correlation.

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I wish to dedicate this work to the most important person in my life, Jesus Christ. Without His guidance and strength, I would have been lost. Also, without His creative world, there would not have been a topic to do my thesis on.

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NOMENCLATURE

This list contains the major parameters used in this study. Others are defined locally.

a	Utilizability correlation parameter (Eq. 4.4)
A	Hay's anisotropic index
f	Cumulative frequency of occurrence
G	Instantaneous insolation
G_{sc}	Solar constant
H	Total daily inolation on a horizontal surface
H_d	Daily diffuse insolation on a horizontal surface
H_T	Total daily insolation on a tilted surface
H_o	Daily extraterrestrial radiation on a horizontal surface
I	Total hourly insolation on a horizontal surface
I_c	Critical hourly insolation level
I_d	Hourly diffuse radiation on a horizontal surface
I_{NIP}	Hourly normal incident beam radiation
I_o	Hourly extraterrestrial radiation on a horizontal surface
I_T	Total hourly insolation on a tilted surface
J	Number of critical levels used in utilizability calculation
k_T	Hourly clearness index
K_T	Daily clearness index
r_d	Ratio of hourly diffuse radiation to daily diffuse radiation

r_t	Ratio of hourly total radiation to daily total radiation
R	Ratio of total hourly insolation on a tilted surface to that on a horizontal surface
\tilde{R}	Ratio of monthly-average hourly insolation on a tilted surface to that on a horizontal surface
\overline{R}	Ratio of monthly-average daily insolation on a tilted surface to that on a horizontal surface
R_b	Ratio of hourly beam radiation on a tilted surface to that on a horizontal surface
X_c	Critical insolation ratio
X_m	Minimum critical insolation ratio at which utilizability equals 0
β	Collector slope
γ	Azimuth angle
δ	Declination
θ	Angle of incidence
θ_z	Solar zenith angle
ρ	Ground reflectance
ϕ	(1) Latitude (2) Monthly-average hourly utilizability
$\overline{\phi}$	Monthly-average daily utilizability
ω	Hour angle
ω_s	Sunset hour angle
An overbar ' $\overline{\quad}$ ' indicates monthly-average	

INTRODUCTION

Energy received from the sun permeates all aspects of our lives. It affects the weather and our resulting conversations, provides energy for plants, provided the stored energy in fossil fuels, can be used to heat or cool buildings, contributes to building cooling loads, and can even generate electricity. Clearly, solar energy contributes to our lives regardless of our philosophy on "alternative energy sources".

This thesis reexamines solar insolation models which are used in solar process design applications and system evaluations. Chapter 1 discusses the two year data base, while the remaining chapters discuss the three major topics investigated: Chapter 2 - estimating tilted surface radiation from horizontal data; Chapter 3 - analyzing the insolation profile during a month; and Chapter 4 - estimating the energy above a given threshold level. Because of the short-term data base, conclusions concerning long-term model performances - accuracy over a 10 year or longer period - could not be made. However, a Recommendation section has been included to indicate areas for future research.

Calculating radiation on a tilted surface from horizontal data requires methodologies for handling beam, diffuse, and ground reflected radiation. For hourly models, methods for predicting beam and ground reflected components are well defined. However, predicting the diffuse radiation component is an area still receiving much

attention. Chapter 2 investigates two areas concerning diffuse radiation: 1) the fraction of diffuse radiation to total radiation; and 2) the isotropic versus Hay's [8] anisotropic distribution model. Hay's hourly anisotropic model breaks diffuse radiation into an isotropic component and a circumsolar component, based on the ratio of terrestrial to extraterrestrial normal incident beam radiation. The tilted surfaces studied include the following orientations: slope equal to latitude; south-facing vertical; east and west-facing vertical; and north-facing vertical.

Insolation levels can be defined in terms of a "clearness index", or the ratio of terrestrial to extraterrestrial total radiation. The cumulative daily distribution of clearness indexes within a month form patterns that are fairly similar for a given monthly-average clearness index. The comparison of minute data distributions for hourly periods, hour data distributions, and existing long-term distributions is discussed in Chapter 3. Daily distributions calculated from hour data are also compared to existing long-term distributions.

The ratio of total solar energy above a given threshold or "critical" level to total solar energy is called "utilizability". This concept is useful for analyzing active solar systems, where the critical level is the energy required to make-up collector losses and the energy exceeding this level is the net gain of the system. For passive systems, the energy below the critical level is useful and the energy above the critical level has to be discarded to prevent

overheating. In this context, utilizability is referred as "unutilizability".

Chapter 4 discusses the comparison of monthly-average hourly and daily utilizability values calculated from minute data, hour data, and Clark's [2] monthly-average hourly correlation. The monthly-average hourly utilizability comparison is for noon to 1 p.m. Clark's correlation was derived from a combined 61 year horizontal radiation data base from 3 locations. To develop the correlation for south-facing surfaces, Clark calculated tilted surface radiation values from the hourly isotropic radiation ratio model and Erbs' [6] hourly diffuse fraction correlation. Using the monthly-average hourly isotropic radiation model and Erbs' monthly-average daily diffuse fraction correlation, Clark's correlation is dependent only on the monthly-average daily clearness index for a given surface orientation and location.

All time referenced in this thesis represents true solar time, and not local standard time for the area investigated. Both San Antonio and Albany are located in the northern hemisphere, and therefore "south-facing surfaces" also imply surfaces facing the sun during mid-day hours. Similarly, north-facing surfaces imply surfaces receiving no direct sunlight during mid-day hours.

1. RESEARCH DATA SOURCE

1.1 Overview

This study utilized two years of existing meteorological data from San Antonio, Texas and Albany, New York. The data were collected as part of the Solar Energy Meteorological Research and Training Site Program (SEMRTS), conducted on behalf of the U.S. Department of Energy. Readings were taken on a minute-by-minute time scale for 20 different instruments and recorded on magnetic tapes. Global or Total radiation instruments included: Horizontal; Tilt = Latitude, Latitude + 10°, and Latitude - 10° south-facing orientations; and vertical surfaces facing North, South, East, and West. Other radiation instruments included: Normal Incident (Direct Beam); Diffuse; Infra-Red; Ultra-Violet; and various other spectral ranges. Also recorded were ambient and dewpoint temperatures, along with wind speed and direction.

The data tapes were arranged in a form of the Researchers Cooperator Format [27]. A file contained a month of data, and a record held 60 minutes of data for one instrument. Each record consisted of a 27-character header, and sixty 9-character minute data groups. As a means of quality control, each measured data point was compared to theoretical limits and various continuity checks through programs in the data acquisition systems. Therefore, a minute data group included a seven digit data value, and a two digit flag indi-

cating the validation of that data value. Table 1.1 shows an example of a minute data record, with an explanation of the record header.

Four types of validation flags were observed in these tapes:

"11" = measured data, unvalidated;

"12" = measured data, considered valid;

"13" = measured data, considered bad;

"99" = missing data.

The "valid data" criteria is described in an Inter-Office Memorandum [16] from the Solar Energy Research Institute (SERI), which administered the data collection. Only the "11" and "12" flagged data values were accepted for the work presented here. Generally, the "11" flags were only found during night hours, where the radiation instrument readings would be due to background "noise" or miscalibration. Typical instrument accuracy is $\pm 5\%$ [5].

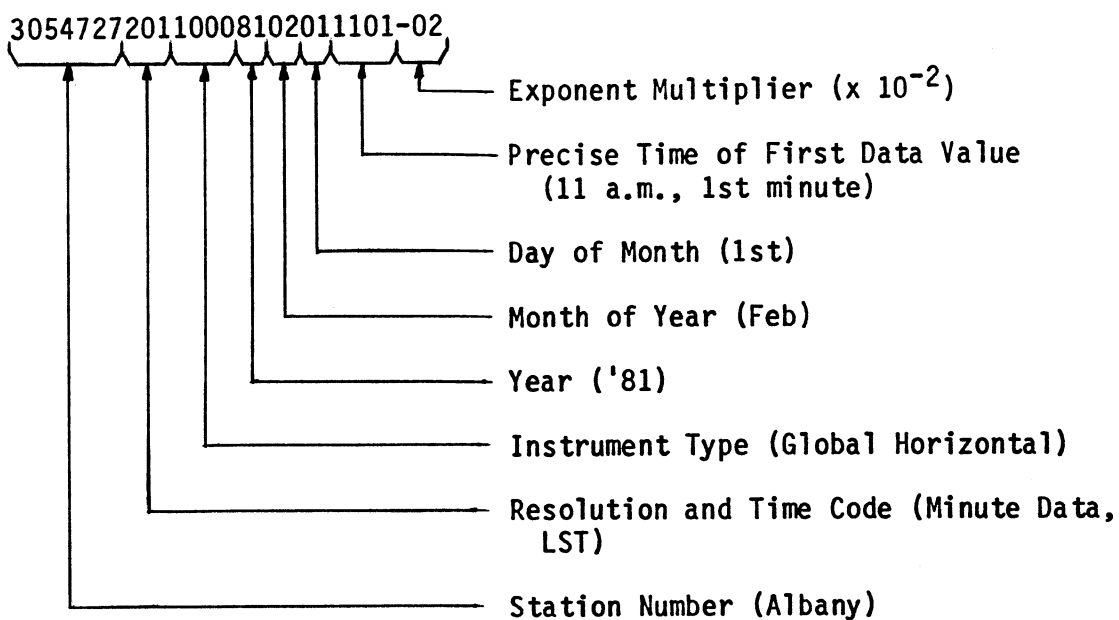
The last three characters in the header represented an exponent multiplier to convert the integer data values to real numbers. The units were the same as for the SOLMET data tapes [32], i.e. KJ/m^2 for irradiation instruments.

To compare minute data results to the more common hour data results, hour data tapes were made from the minute data. To be consistent with the minute tapes, a file contained a month of data, and a record held 24 hours of data for one instrument. Each record consisted of a 27-character header, and twenty-four 9-character hour data groups. Once again, each data group contained a seven digit data value, and a two digit flag. In making the hour tapes, the data

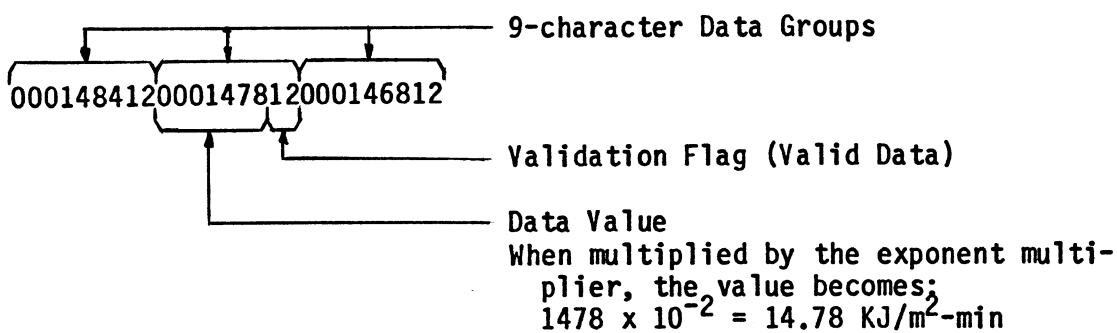
TABLE 1.1
Minute Data Record Example

The numbers below are from a data record from the Albany Minute Tape.

Header:



Data Groups:



was also converted from Local Standard Time (LST) to True Solar Time (TST).

To compensate for "bad" or missing data, all sums were normalized to a sixty-minute value. A new two-digit flag was then written for each hour data point, indicating the number of "good" minute data values used in generating the hourly sum. Hours with completely missing data were filled with 9's and given a "00" flag.

1.2 San Antonio, Texas Data

The San Antonio, Texas data was taken by Trinity University in San Antonio, between April 1981 and March 1982. The tilted radiation instrumentation included: 20° south, 30° south, and 40° south. Table 1.2 shows a summary of the radiation data available for this study.

Besides beam and diffuse radiation, tilted pyranometers also receive radiation reflected from the ground, proportional to the local albedo or ground reflectivity. Typical albedo values are around 0.2, but may be as high as 0.7 for fresh snow. To reduce this variability in ground reflectance, Trinity University used flat black plates to produce artificial horizons for the tilted pyranometers [31]. This resulted in a low, year round value, estimated to be 0.05.

The diffuse radiation was measured by a pyranometer with a shadow band. The accuracy of this method versus other methods of obtaining diffuse data has been an ongoing debate [16]. Since the shadow band blocks out more radiation than just the beam, correction methods must be applied to the data [4,20]. Hogan and Loxsom [14]

TABLE 1.2
SAN ANTONIO, TX DATA

Data collected by Trinity University

Latitude = 29.5°

Longitude = 98.5°

Radiation Data Available for This Study

<u>Instrument I.D. Number</u>	<u>Variable Measured[*] and Orientation</u>	<u>Instrument [31]</u>
1000	Global, Horizontal	Eppley PSP ^{**}
1260	Global, 20 South	"
1360	Global, 30 South	"
1460	Global, 40 South	"
1920	Global, 90 North	"
1940	Global, 90 East	"
1960	Global, 90 South	"
1980	Global, 90 West	"
2010	Direct Normal Beam	Eppley NIP ^{***}
3000	Diffuse, Horizontal	Eppley PSP w/Shadow Band

* Global instruments were filtered with a 0.295-2.80 μm pass band

** PSP = Precision Spectral Pyranometer

*** NIP = Normal Incident Pyrheliometer

showed that diffuse values from the corrected shadow band method are more accurate than calculated values from global horizontal and normal incident radiation data. However, in a more recent study using a larger data base, Huang [15] found the value of diffuse radiation calculated from normal incident and global radiation data to be more accurate than the shadow band measurements. For this work, the diffuse radiation measurements were ignored in favor of calculated values from the global and normal incident data.

In converting the minute data from LST to TST, the equation of time conversion factor [5] was calculated for the first day of each month only. This will cause a slight error for the following days in those months where the equation of time changes rapidly over the month. The worst cases are December and September, where the change in the equation of time conversion factor is 13 minutes and 11 minutes, respectively. This error is considered minor for mid-day calculations. In all cases, local standard time in San Antonio leads the true solar time.

1.3 Albany, New York Data

The Albany, New York data was taken by State University of New York at Albany, between August 1980 and July 1981. The tilted radiation instrumentation included: 33° south, 43° south, and 53° south. Through the use of shielding baffles, the ground reflectivity for their instrumentation was reduced to 0.00 [30]. Table 1.3 shows a summary of the radiation data available for this study.

TABLE 1.3
ALBANY, NY DATA

Data collected by State University of New York at Albany

Latitude = 42.7°

Longitude = 73.8°

Radiation Data Available for This Study

<u>Instrument I.D. Number</u>	<u>Variable Measured and Orientation</u>	<u>Instrument [31]</u>
1000	Global, Horizontal	Eppley PSP [*]
1460	Global, 33 South	"
1560	Global, 43 South	"
1660	Global, 53 South	"
1920	Global, 90 North	"
1940	Global, 90 East	"
1960	Global, 90 South	"
1980	Global, 90 West	"
2010	Direct Normal Beam	Eppley NIP ^{**}
3000	Diffuse, Horizontal	Eppley PSP w/Shading Disk
3001	Diffuse, Horizontal	Eppley PSP w/Shadow Band
3002	Diffuse, Horizontal	Calculated from Instrument 1000 and 2010

* PSP = Precision Spectral Pyranometer

** NIP = Normal Incident Pyrhelimeter

Three sets of diffuse radiation data were recorded: data measured by a pyranometer with shadow band; pyranometer with shading disc; and calculated values from global and normal incident data. A spot check of all three methods showed the corrected shadow band values to be the largest, while the shading disc and calculated values were approximately equal to each other. To be consistent with the San Antonio data analysis, the calculated data values were used for diffuse radiation.

For the Albany hour tape, the equation of time conversion factor to change the data from LST to TST was calculated for every day of each month. This eliminated the minor source of error mentioned for the San Antonio hour tape. The difference in LST and TST varied from local time leading the solar time, to solar time leading the local time. For programming reasons, local and solar times were considered equal for any differences less than 2 minutes.

2. RADIATION ON TILTED SURFACES

2.1 General Discussion

Long-term horizontal radiation data are available for most parts of the country. The most unexplicit are maps showing trends of average daily radiation for a given month [23]. For specific locations, the weather service frequently document the long-term monthly-average daily horizontal radiation [2]. The SOLMET program utilized 23 years of data to provide an hourly profile of horizontal radiation values over a "typical" year, for 26 U.S. locations [32]. The data were "rehabilitated" to account for instrument error from degradation, and other long and short term errors. The SOLMET program also included estimates of hourly horizontal radiation profiles for an additional 222 locations, based on related meteorological data.

In comparison, long-term data for tilted surfaces are scarce. Since most solar energy designs incorporate tilted surfaces, "radiation ratio" mathematical models are used to convert horizontal data into the corresponding tilted values. A "radiation ratio" is the ratio of radiation on the tilted surface, to the radiation on a horizontal surface. This ratio can then multiplied by the known horizontal radiation to obtain the desired radiation on the tilted surface.

Typical models find the radiation ratio on a tilted surface for hourly periods R , monthly-average hourly periods \tilde{R} , and monthly-average daily periods \bar{R} . The accuracy of these radiation ratios depends on the methodology for handling the beam, diffuse, and re-

flected components of solar irradiation. Presently, the major issue concerning the radiation ratio is the handling of diffuse radiation. Within this diffuse radiation discussion, two questions have arisen:

- 1) What is the percentage of diffuse to total insulation, and
- 2) Assuming this percentage is known, what is the distribution of diffuse radiation from the various parts of the sky?

For the following section it will be assumed that the percentage of diffuse radiation is known.

2.2 Isotropic Model Description

The simplest radiation ratio models incorporate an isotropic diffuse radiation assumption, first suggested by Hottel and Woertz [13]. This approach assumes diffuse radiation is uniformly distributed from all parts of the sky, regardless of weather conditions.

2.2.1 Hourly Isotropic Model

The hourly isotropic model calculates the radiation ratio for a specific hour. To define this ratio, the components required to calculate the radiation on a tilted surface will first be shown.

The diffuse radiation on a tilted surface is the diffuse radiation on a horizontal surface times the "sky-view factor" - the portion of the sky "in view" of the tilted surface. Defining β as the surface slope, the sky-view factor is $(1 + \cos \beta)/2$. Therefore, the diffuse component can be written as:

$$\text{Diffuse} = I_d (1 + \cos \beta)/2 , \quad (2.1)$$

where I_d is the diffuse radiation.

The ground reflected radiation also incorporates an isotropic assumption. Defining ρ as the ground reflectivity, the reflected component is:

$$\text{Reflected} = \rho I (1 - \cos \beta)/2 . \quad (2.2)$$

where $(1 - \cos \beta)/2$ is the ground-view factor for the tilted surface.

The beam component is found by multiplying the beam radiation on a horizontal surface, I_b , by the ratio of beam radiation on the tilted surface to the horizontal surface, R_b . On an instantaneous basis, this beam ratio is a function only of geometry, as shown in Eq. (2.3).

$$R_b = \frac{G_{bT}}{G_b} = \frac{G_{bn} \cos(\theta)}{G_{bn} \cos(\theta_z)} = \frac{\cos(\theta)}{\cos(\theta_z)} \quad (2.3)$$

where equations for $\cos(\theta)$ and $\cos(\theta_z)$ can be found in Duffie and Beckman [5].

For a given period of time, the beam ratio numerator and denominator need to be integrated with respect to time. Since beam radiation is attenuated by the earth's atmosphere, the amount of atmosphere or beam "path-length," becomes important. As the position of the sun changes throughout a day, the path-length changes, making the beam ratio a function of the atmospheric transmittance.

For hourly periods, Hottel and Woertz [13] suggested treating R_b as a constant, with the middle of the hour being used for the calculation. This is a reasonable approximation for mid-day hours, since the change in beam path-length is minimal, and a fair approximation for hours close to sunrise and sunset, where the change in beam path-length is more pronounced.

Horizontal beam radiation is the difference between global horizontal radiation and horizontal diffuse radiation: $I_b = (I - I_d)$. Calculating the beam radiation in this manner allows use of any one of the numerous diffuse radiation models, opposed to the limited number of beam radiation sources. These diffuse radiation models will be discussed latter in more detail. Using the horizontal and diffuse radiation terms, the beam component can be written as:

$$\text{Beam} = (I - I_d)R_b \quad (2.4)$$

Combining all three radiation components, the radiation on a tilted surface is:

$$I_T = I_d \left(\frac{1 + \cos \beta}{2} \right) + (I - I_d)R_b + \rho I \left(\frac{1 - \cos \beta}{2} \right) \quad (2.5)$$

Dividing Eq. (2.5) by the global horizontal radiation produces the hourly isotropic radiation model:

$$R = \frac{I_d}{I} \left(\frac{1 + \cos \beta}{2} \right) + \left(1 - \frac{I_d}{I} \right) R_b + \rho \left(\frac{1 - \cos \beta}{2} \right) \quad (2.6)$$

The hourly radiation model is useful for detailed analysis of a solar process. An example of this application is TRNSYS [37] - a transient system simulation program - which models time dependent solar operations. This program is useful for estimating both short and long-term performances.

2.2.2 Monthly-Average Hourly Isotropic Model

The monthly-average hourly radiation ratio is the ratio of the monthly-average hourly tilted radiation to the monthly-average hourly horizontal radiation.

$$\tilde{R} = \frac{\bar{I}_T}{\bar{I}} \quad (2.7)$$

It is used as an "average" hourly radiation ratio over a given month. The model is derived by integrating Eq. (2.5) over a month, and then dividing by \bar{I} . The hourly diffuse fraction becomes a monthly-average hourly diffuse fraction, \bar{I}_d/\bar{I} , while the other terms remain the same due to their dependence only on geometry. The monthly-average hourly isotropic model is therefore:

$$\tilde{R} = \frac{\bar{I}_d}{\bar{I}} \left(\frac{1 + \cos \beta}{2} \right) + \left(1 - \frac{\bar{I}_d}{\bar{I}} \right) R_b + \rho \left(\frac{1 - \cos \beta}{2} \right) \quad (2.8)$$

The monthly-average hourly radiation model is useful for "quick" simulations of a solar process. An example of this application is FCHART [36], a long-term performance design program used for modeling solar heating systems. FCHART produces fairly accurate long-term

results, but without the expense of running a detailed simulation program such as TRNSYS.

2.2.3 Monthly-Average Daily Isotropic Model

The monthly-average daily radiation ratio is the ratio of the monthly-average daily radiation on a tilted surface to a horizontal surface.

$$\bar{R} = \frac{\bar{H}_T}{\bar{H}} \quad (2.9)$$

The model is derived by integrating the monthly-average hourly tilted surface radiation over all daylight hours in a month. Therefore, the diffuse fraction term becomes the monthly-average daily diffuse fraction, \bar{H}_d/\bar{H} . The beam ratio becomes the ratio of the monthly-average daily beam radiation on the tilted surface to that on a horizontal surface, \bar{H}_{bT}/\bar{H}_b . As discussed in Section 2.2.1, this is a function of the atmospheric transmittance. To obtain an estimated value, Liu and Jordan [21] suggested neglecting the effect of the atmosphere. In this case, \bar{R}_b is the ratio of the monthly-average daily extraterrestrial radiation on the tilted surface to that on a horizontal surface. This assumption is correct only for south-facing surfaces during the solar equinox [22].

Using \bar{H}_d/\bar{H} and \bar{R}_b , the monthly-average daily radiation ratio can be written as:

$$\bar{R} = \frac{\bar{H}_d}{\bar{H}} \left(\frac{1 + \cos \beta}{2} \right) + \left(1 - \frac{\bar{H}_d}{\bar{H}} \right) \bar{R}_b + \rho \left(\frac{1 - \cos \beta}{2} \right) \quad (2.10)$$

The monthly-average daily radiation model is useful for approximate calculations of solar irradiation on a tilted surface. These approximations can then be used in an economic analysis to determine if a solar process has economic potential, before the expense of a detailed design is made.

2.3 Diffuse Fraction Calculation

The three radiation ratio models shown are all functions of their respective diffuse fractions. As mentioned in Chapter 1, the method for obtaining diffuse insolation data is still being discussed. This raises the question, what methodology for obtaining the diffuse fraction should be used?

The hourly diffuse fraction I_d/I , can be obtained in several ways. Diffuse data can be measured by a pyranometer with a shadow band; pyranometer with a shading disc; or calculated from global and beam data. Using global horizontal radiation and normal incident beam radiation I_{NIP} data, the diffuse radiation on a horizontal surface is:

$$I_d = I - I_{NIP} \cos (\theta_z) . \quad (2.11)$$

The diffuse fraction can then be found by dividing Eq. (2.11), or the actual measured diffuse insulation, by the horizontal radiation.

However, diffuse data of any kind is generally not available for most locations. To overcome this data deficiency, many correlations have been developed from available diffuse data, to estimate the dif-

fuse fraction. Most of these correlations [6] are functions of the "clearness index" - the ratio of global terrestrial to global extra-terrestrial radiation on a horizontal surface. This clearness index will be discussed in more detail in Chapter 3.

Diffuse fraction correlations are limited to the accuracy of their data base. Modeling the diffuse fraction around one independent parameter has also been questioned. In a study utilizing almost three years of global and direct radiation data from 33 U.S. sites, Garrison [7] found the diffuse fraction to actually be a function of five independent parameters: global solar irradiance; solar elevation (beam path-length); surface albedo; atmospheric precipitable water; and atmospheric turbidity. However, a diffuse fraction correlation as a function of these five parameters has yet to be developed. Also, except for global solar irradiance, these parameters are generally not available.

The monthly-average hourly and daily diffuse fractions can also be found from data when it is available. Monthly-average values can be calculated by summing the daily contributions to the diffuse and global components. The ratio of the sums becomes the monthly-average short-term value. For long-term values, an average can be taken of the monthly-average diffuse fractions.

However, due to the lack of data, correlations must once again be relied upon for most locations [5]. These monthly-average diffuse fraction models have been developed by correlating the results of monthly-average diffuse fractions calculated from a data base, to the

monthly-average clearness index. Another approach for monthly-average daily diffuse fractions was first shown by Liu and Jordan [21]. They developed a correlation between the monthly-average diffuse fraction and monthly-average clearness index, by relating the daily components of the diffuse fraction to the long-term average distribution of the daily clearness index. This approach was also the method used by Erbs [6] to develop his diffuse fraction correlations, which will be discussed in more detail in Section 2.6.

As mentioned in the beginning of Chapter 2, part of the diffuse radiation discussion is the calculation of the diffuse to global radiation ratio. All of the correlations developed do work fairly well for calculating this ratio, for their given data base. However, judging on the limited diffuse data, the findings by Garrison [7], and the diversity of models developed, the diffuse fraction question has yet to be completely answered.

The following section on anisotropic radiation models assumes the diffuse to global fraction is known. Based on this "known" break-up, the issue in question is: what is the distribution of diffuse radiation from the various parts of the sky?

2.4 Anisotropic Model Descriptions

In 1966, Norris [25] compared the isotropic model, an anisotropic model, and one year's worth of data from Highest, Australia. The anisotropic model was developed by Morse and Czarnecki [24], and assumed that a major portion of the diffuse radiation emanates from the area surrounding the sun. This "circumsolar" diffuse radiation can

then be treated as beam radiation in the isotropic model. The data base included total and diffuse radiation on both horizontal and 60° tilted surfaces. Norris concluded that both models were actually incorrect, and that real data should be taken in the location of interest. However, when averaged over a month, he felt that the distribution of diffuse radiation is isotropic.

During the last 10 years, this question has been reevaluated. Many reports conclude that the pure isotropic assumption is inappropriate [9,14,19,26]. Hay [10] concluded that the degree of anisotropic diffuse radiation varied from complete beam in the absence of atmospheric scattering, to complete isotropy under thick overcast clouds. Because of this recent work, new models for predicting the radiation ratio have been developed. Most incorporate various coefficients to modify the isotropic model, while a few take drastically new approaches. The following sections provide a short overview of some of the more notable anisotropic work recently done.

2.4.1 Klucher's Model

Klucher [19] used a data base of 6 months and 3 orientations (Horizontal, 37° and 60° south-facing) for comparison to the isotropic model, and to Temps and Coulson's [33] anisotropic-clear-sky model. The Temp and Coulson model considers anisotropic effects from both "horizon brightening" and circumsolar diffuse radiation under clear sky conditions. Both models had advantages under cloudy and clear weather conditions respectively, but neither were satisfactory for all cases. Consequently, Klucher developed an anisotropic cor-

rection factor for diffuse radiation on a tilted surface, to account for the degree of clearness. His model reduces to the isotropic case under heavy overcast conditions, but otherwise incorporates a fraction of the Temps and Coulson model.

2.4.2 Hay's Model

Hay [8] found the isotropic hourly model leads to significant short and long term errors compared to actual data. Taking an approach similar to Robinson [29] and to Revfeim [28], he broke the diffuse radiation into isotropic and circumsolar components. However, he allowed the ratio of isotropic to anisotropic diffuse radiation to vary, depending on an anisotropy index [9]. His original model for this index was partially a function of the optical air mass. Later, he modified this to be the ratio of normal incident beam radiation to the extraterrestrial normal incident radiation [8]. Under conditions of heavy overcast, the normal incident radiation approaches zero, returning the radiation ratio model to the isotropic case.

The evaluation of his model utilized 6 years of data for three south-facing surfaces from both Vancouver, British Columbia and Toronto, Ontario. Data from vertical north, east, and west facing surfaces were also used from Vancouver.

2.4.3 Herzog Models

Herzog [11] used existing minute data from the SEMRTS program, to develop correction factors for the hourly isotropic model and the monthly-average daily isotropic model. His models were developed for

south facing tilted surfaces and vertical surfaces facing north, south, east, and west. The data base included: San Antonio, Texas (27 months, 7 tilts); Albany, New York (55 months, 7 tilts); and Atlanta, Georgia (46 months, 1 tilt).

For the hour model, Herzog empirically developed an anisotropic to isotropic diffuse insolation ratio to account for circumsolar and horizon brightening diffuse radiation. In the same manner as Klucher and Hay, this ratio is used as a correction factor in the diffuse radiation component of the isotropic model. It is a function of the hourly clearness index, angle dependent parameters, and time of year. Three different hourly correction factors were developed to account for differences in radiation characteristics during the winter, equinox, and summer seasons.

Using his hourly results and probability theory of the clearness frequency distribution (see Chapter 3), Herzog also developed a correction factor for the isotropic monthly-average daily radiation ratio model. Two versions of the correction factor were developed based on zero and nonzero values of the monthly-average daily beam fraction, as defined by Klein and Theilacker [18].

2.4.4 Perez Model

Perez et al. [26] took a different approach to calculating the diffuse radiation component on a surface. They developed a "geometrical sky hemisphere description" to help parameterize the various characteristics of diffuse radiation. This resulted in a matrix equation with three independent variables used to calculate the radi-

ation ratio. The model was then compared to data for seasonally representative months from data from Trappes, France; Carpentras, France; San Antonio, Texas; and Albany, New York.

At present, the matrix variables are not written as continuous functions, but are defined by one of over 200 "sky condition categories". Consequently, this model is inconvenient to implement at this point in time.

2.5 Past Comparisons of Radiation Ratio Models

All of the anisotropic models presented have advantages and disadvantages. All of them were developed from relatively short term data, which may limit their universal application. Also, most have been developed only for hourly radiation ratio models, which limits their use to detailed analysis. Herzog did develop a monthly-averaged daily model, but no monthly-averaged hourly models were found, as required for use in Clark's utilizability correlation (see Chapter 4). Klucher's model was developed only from south-facing orientations, and Herzog's hourly model has three different forms depending on the time of year. Perez's model can not be used without knowing the matrix elements for the desired locations.

The four anisotropic hourly models discussed do have one major strength in common: under the conditions tested by their authors, the respective anisotropic model usually provided closer results to tilted surface insolation levels, than the isotropic model. The comparative study done by Norris [25] was the only contrary report found. When evaluated over a monthly period, he found the hourly

isotropic model was better than the anisotropic model developed by Morse and Czarnecki [24].

Many studies have been made of these anisotropic models. Hogan and Loxsom [14] made an independent comparison of the isotropic, Hay, and Klucher models, to three winter months of SEMRTS data from San Antonio, Texas. Their comparison was for 20°, 30°, 40° south-facing surfaces, and vertical north, south, east, and west surfaces. They concluded:

- 1) none of the models can accurately predict insolation on vertical surfaces; and
- 2) the Klucher model produced the most consistently correct results for these data.

Studies using larger data bases have found different results. Huang [15] used 27 months of SEMRTS data from San Antonio, Texas at the same orientations as Hogan and Loxsom. Once again, the isotropic, Hay, and Klucher models were compared. However, Huang found the Hay model to be the most accurate during the winter for all tilts, and in the summer for small tilts. The isotropic model was best for one condition - vertical surfaces during summer months, while the Klucher model was best during the summer for tilts between 20 and 40 degrees. On an annual basis, Huang concluded that the Hay model was best, although it exceeded $\pm 5\%$ of the measured values for vertical surfaces.

Perez et al. [26] compared their model and the isotropic, Hay, and Klucher models to their data base, showing that their model was

best. They also pointed out that the Hay model underestimates on clear days for surfaces away from the sun, due to its lack of a horizon brightening consideration. In comparison, the Klucher model overestimates for surfaces not facing the sun.

Hay and McKay [8] made a comparison of eight models, including the isotropic, Klucher, Hay, and Perez models, to their Vancouver data base. They too discussed the positive and negative attributes of all of the models evaluated. Many of the models gave excellent results under certain conditions, but generated poorer results for the other cases. The exception was the Hay model, which consistently produced small short and long term errors for all slope orientations.

2.6 Radiation Ratio Analysis from Present Data

2.6.1 Diffuse Fraction Comparison

Existing diffuse fraction correlations were developed from limited data bases. Since the SEMRTS data included normal incident beam radiation - which can be used to calculate diffuse radiation, a comparison was made of correlation versus data derived monthly-average daily diffuse fractions. These diffuse fractions were calculated from: hourly data; Erbs' [6] hourly diffuse fraction model; and Erbs' [6] monthly-averaged daily diffuse fraction model. Comparing the monthly-average daily values was considered a fair method for evaluation of hourly diffuse fractions over typical ranges, i.e. all daylight hours, and monthly variations in radiation data. Erbs' monthly-average daily diffuse fraction was included as a check of a "quick" calculation method. As a measure of the individual hourly

errors between the data and Erbs' hourly diffuse fractions, the RMS error was also calculated.

A closer look at the normal incident beam (NIP) data revealed some problems. As discussed in Chapter 1, all data contained a two-digit flag indicating the quality of that data value. The NIP data were flagged as being missing or invalid for a large percentage of the hours within most months, especially for San Antonio. Some hours were found with only 1 to 20 minutes of valid NIP data while 60 valid minutes of global data were found. Since an explanation could not be envisioned as to why data would be randomly invalid within an hour, only hours with 60 valid minutes of both global and NIP data were used for the diffuse fraction comparison. Due to instrument accuracy problems and "pre-dawn" light, hours surrounding a sunrise or sunset were also neglected. These hours contain very little insolation and therefore introduce negligible error by neglecting them.

The decision to use only hour values with 60 valid minutes greatly limited the number of allowed NIP data, as shown by Table 2.1. The number of global horizontal hour values with 60 valid minutes is also shown by Table 2.1. Overall, the hours of valid San Antonio NIP data only represented 49% of the potential daylight hours during the year. The Albany NIP data were better at 68%. The worst month was October in San Antonio, where only 39 hours out of the potential 310 hours of complete daylight contained valid NIP data. Fortunately, the hours of valid horizontal data for San Antonio and

TABLE 2.1
Number of hours used in \bar{R} calculation.

Notes:

1. Only hours with 60 "good" minutes of data were used.
2. Only "complete" daylight hours were used. Part hours caused by a sunrise or sunset were neglected.

SAN ANTONIO, TX DATA

<u>Month</u>	<u>Daylight Hours in month</u>	<u>Hours of "Good" Horizontal data</u>	<u>Hours of "Good" NIP Data</u>
January	310	294	209
February	280	262	156
March	328	322	220
April	360	354	138
May	372	359	188
June	360	311	84
July	372	364	219
August	372	370	236
September	340	325	241
October	310	308	39
November	300	279	71
December	<u>302</u>	<u>302</u>	<u>178</u>
Total	4014	3850	1979
% of Daylight Hours		96%	49%

ALBANY, NY DATA

<u>Month</u>	<u>Daylight Hours in Month</u>	<u>Hours of "Good" Horizontal Data</u>	<u>Hours of "Good" NIP Data</u>
January	248	240	190
February	276	269	148
March	328	316	192
April	360	357	213
May	428	409	336
June	420	414	316
July	434	421	336
August	388	374	288
September	340	329	238
October	310	301	215
November	244	236	148
December	<u>248</u>	<u>230</u>	<u>134</u>
Total	4024	3896	2754
% of Daylight Hours		97%	68%

Albany were 96% and 97% respectively, of the potential daylight hours.

Erbs' hourly diffuse fraction is a function of the hourly clearness index k_T , where:

$$\begin{aligned}
 \text{For } k_T < 0.22 \quad \frac{I_d}{I} &= 1.0 - 0.09 k_T \\
 \text{For } 0.22 < k_T < 0.80 \quad \frac{I_d}{I} &= 0.9511 - 0.1604 k_T + 4.388 k_T^2 \\
 &\quad - 16.683 k_T^3 + 12.336 k_T^4 \\
 \text{For } k_T > 0.80 \quad \frac{I_d}{I} &= 0.165
 \end{aligned} \tag{2.12}$$

k_T was calculated for each valid hour, using global horizontal data and an analytical equation for the hourly horizontal extraterrestrial radiation, I_0 [5]:

$$\begin{aligned}
 I_0 = \frac{12 \times 3600}{\pi} G_{sc} & \left[1 + 0.033 \cos \left(\frac{360 n}{365} \right) \right] \left[\cos \phi \cos \delta (\sin \omega_2 \right. \\
 & \left. - \sin \omega_1) + \frac{2\pi(\omega_2 - \omega_1)}{360} \sin \phi \sin \delta \right]
 \end{aligned} \tag{2.13}$$

where G_{sc} = the solar constant, and n = day of the year.

The hourly diffuse fractions were multiplied by the actual global horizontal insolation, to obtain the horizontal diffuse radiation. The diffuse and global values were then separately summed for the month. The ratio of the total diffuse to total global insolation produced the monthly-average daily diffuse fraction. The data derived monthly-average daily diffuse fraction was similarly found, by

dividing the total valid diffuse value by the total valid global value.

Erbs' monthly-average daily diffuse fraction is a function of the monthly-average daily clearness index \bar{K}_T .

$$\frac{\bar{H}_d}{\bar{H}} = 1.317 - 3.023 \bar{K}_T + 3.372 \bar{K}_T^2 - 1.760 \bar{K}_T^3 \quad (2.14)$$

$$\text{for } 0.3 < \bar{K}_T < 0.8$$

The monthly-average daily clearness index was found by summing both the horizontal global data values and the calculated horizontal extraterrestrial values over all valid daylight hours in the month. The ratio of these sums produces the monthly-average daily clearness index.

Figures 2.1 and 2.2 show the results of the monthly-average daily diffuse fraction calculations for San Antonio and Albany, respectively. Figure 2.1 shows an equal number of overestimations as underestimations of the monthly-average daily diffuse fraction found by Erbs' hourly correlation. The worst errors are around 10% of the maximum diffuse fraction (The maximum diffuse fraction = 1.0). However, for seven of the months, the error in the predicted value of \bar{H}_d/\bar{H} is less than 3%. Considering instrumentation accuracy of $\pm 5\%$ [5], these values are excellent. As expected, the simpler monthly-average daily correlation had a larger error than the hourly correla-

MONTHLY-AVERAGE DAILY DIFFUSE FRACTION

San Antonio, TX

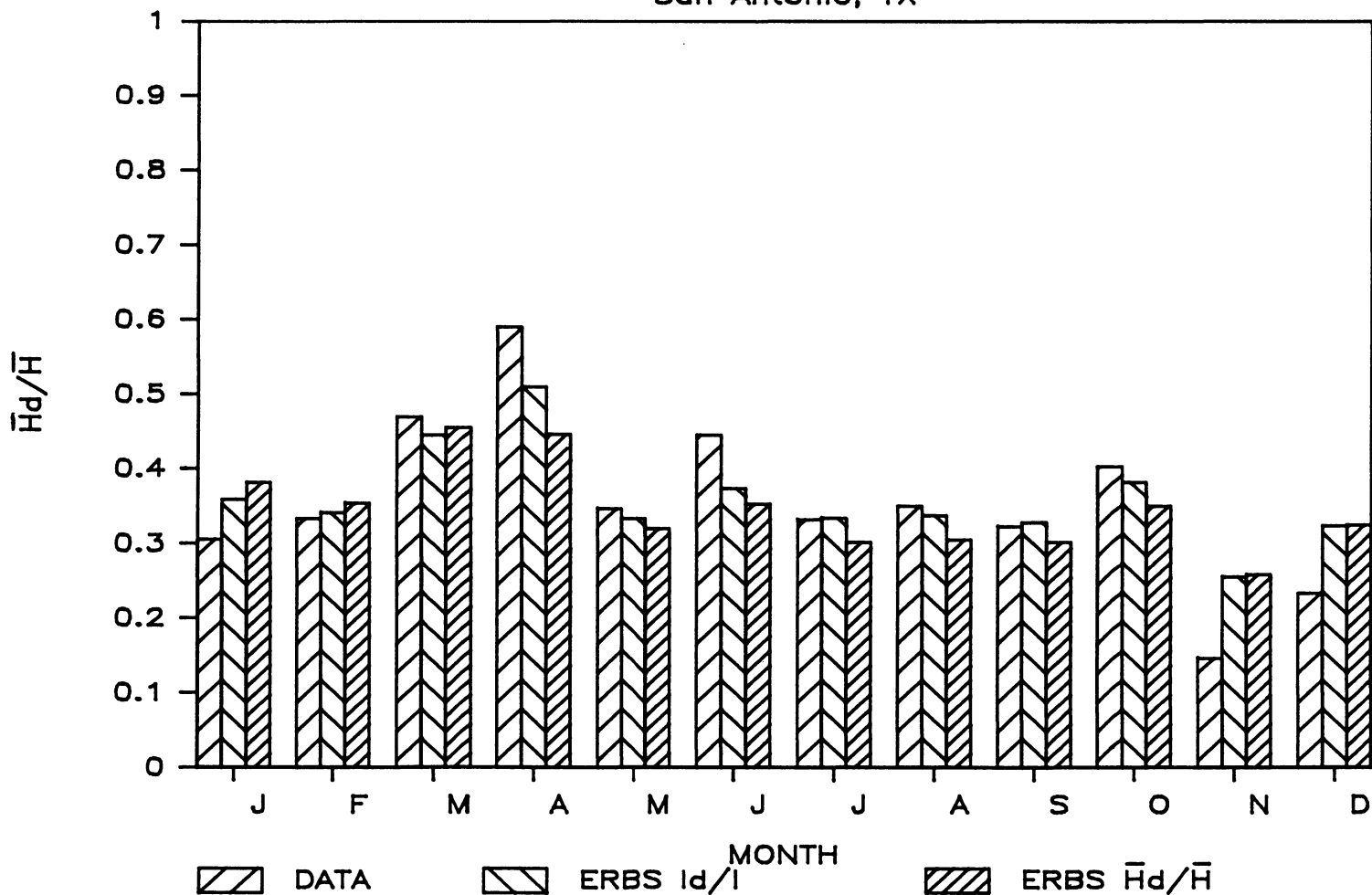


Figure 2.1: Monthly-Average Daily Diffuse Fractions for San Antonio, TX.

MONTHLY-AVERAGE DAILY DIFFUSE FRACTION

Albany, NY

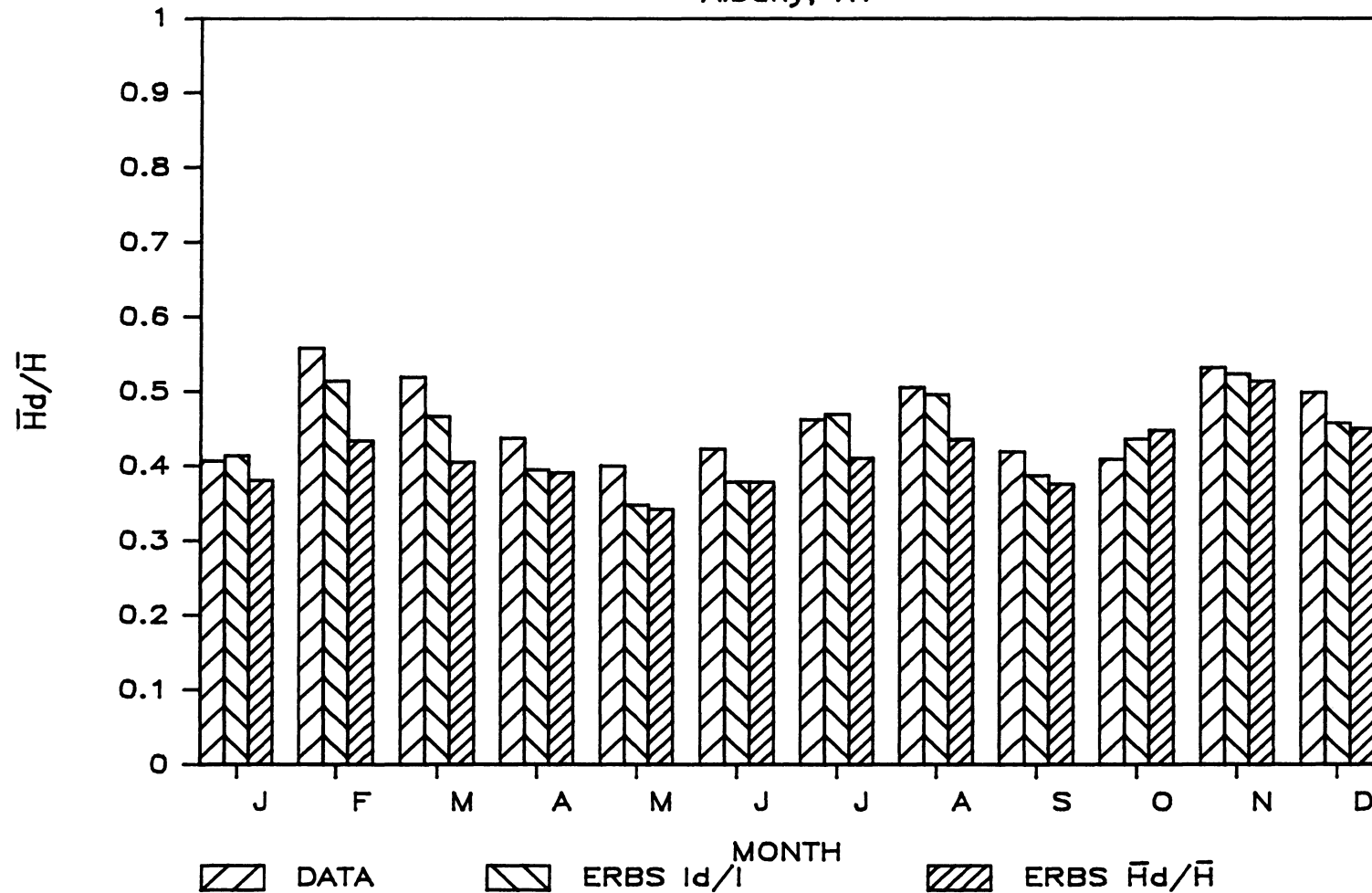


Figure 2.2: Monthly-Average Daily Diffuse Fractions for Albany, NY.

tion. The poorest case is an overestimation by 11% of the maximum fraction.

Figure 2.2 - Albany - shows smaller errors than found for San Antonio. In most cases, Erbs' hourly model underestimates the data value, usually by 4 to 5% of the maximum fraction. The few cases of overestimation are all less than 3%. Once again, Erbs' monthly-average daily correlation produces larger errors than the hourly model, the poorest being an underestimation by 12%.

Overall, the monthly-average daily diffuse fractions compare fairly well. However, as a measure of the differences between individual hourly diffuse fractions found from data and Erbs' hourly correlation, an RMS error was calculated. As applied here, the RMS error is defined as:

$$\text{RMS error} = \sqrt{\frac{\sum_{i=1}^n \left(\frac{I_d}{I} \text{data} - \frac{I_d}{I} \text{Erbs} \right)^2}{n - 1}} \quad (2.15)$$

By summing the squares of the individual errors, the RMS error places more weight on larger differences. Therefore, a large RMS error indicates poor agreement between data and correlation hourly diffuse fractions.

Table 2.2 shows the RMS error between Erbs' hourly diffuse fraction and the hourly diffuse fraction calculated from the data. The RMS error shows the individual hourly value comparison is not always favorable. The poorest comparison is in Albany, where the RMS error is 0.322. The poorest RMS error for San Antonio is 0.227. Also

TABLE 2.2
Comparison of Monthly-Average Daily Diffuse Fractions

Note: % Change = $\left[\left(\frac{\overline{H}_d}{\overline{H}} \right)_{\text{model}} - \left(\frac{\overline{H}_d}{\overline{H}} \right)_{\text{data}} \right] / 1.0 \times 100$.

San Antonio, TX

MONTH	% CHANGE	% CHANGE	RMS ERROR
	Erbs Hourly vs. Data	Erbs $\overline{H}_d/\overline{H}$ vs. Data	
January	5.3%	7.6%	0.177
February	0.8	2.1	0.134
March	-2.5	-1.4	0.103
April	-8.0	-14.	0.117
May	-1.3	-2.6	0.140
June	-7.1	-9.2	0.110
July	0.2	-3.0	0.119
August	-1.2	-4.5	0.139
September	0.5	-2.1	0.147
October	-2.1	-5.3	0.124
November	10.	11.	0.183
December	9.1	9.2	0.227

Albany, NY

MONTH	% CHANGE	% CHANGE	RMS ERROR
	Erbs Hourly vs. Data	Erbs $\overline{H}_d/\overline{H}$ vs. Data	
January	0.7%	-2.6%	0.113
February	-4.4	-12.	0.122
March	-5.2	-11.	0.124
April	-4.2	-4.6	0.223
May	-5.2	-5.8	0.322
June	-4.4	-4.4	0.286
July	0.7	-5.2	0.148
August	-1.0	-7.0	0.215
September	-3.2	-4.3	0.285
October	2.7	3.9	0.215
November	-0.8	-1.8	0.189
December	-4.1	-4.9	0.264

shown is a summary of the percent change between the correlations and the data values of $\overline{H}_d/\overline{H}$ (percent of maximum fraction).

Due to the limited data base, especially for San Antonio, only nonconclusive statements can be made. A comparison was made of the percent changes in $\overline{H}_d/\overline{H}$ to the percent of potential daylight hours utilized, but no correlation was found. Consequently, even though data were lacking, these deficiencies do not appear to affect the overall results. For the two years studied, the monthly-average daily diffuse fractions calculated by Erbs' correlations were usually fairly accurate. Erbs' hourly correlation usually gave the best results, while Erbs' monthly-average daily correlation typically gave slightly poorer results. However, large RMS errors indicate poor hourly agreement between Erbs' hourly correlation and data. Whether this hourly inaccuracy is due to "atypical" data, or inherent error in Erbs' correlations due to one parameter modeling, is unknown.

2.6.2 Model Selection

As discussed in the isotropic model section (Section 2.2), there are many needs for accurate models to calculate insolation levels on tilted surfaces. For detailed analysis, hourly models are the most widely used. At present, the TRNSYS [37] simulation program developed by the University of Wisconsin Solar Energy Laboratory, uses the hourly isotropic model for its calculation of hourly insolation levels on sloped surfaces. As a generic check for potential improvement in hourly radiation ratio calculations, radiation ratios calculated from the data were compared to results from one anisotropic

hourly model, and from the isotropic model. Also compared was the monthly-average hourly isotropic model, which is used in Clark's hourly utilizability correlation (See Chapter 4). These comparisons were made using hourly diffuse fractions calculated from both Erbs correlations and from the available NIP data.

Since this was a generic investigation, only one anisotropic model was evaluated. The Perez model was not considered since the matrix elements have not been generalized for various locations. The seasonal Herzog models involved a degree of complexity that was beyond the present interest in anisotropic models. Including seasonal variations in an anisotropic model should be considered only after being convinced of the need for an anisotropic model. This left the Klucher and Hay anisotropic models to choose from. From the reports studied, the Hay model seemed to have the best accuracy under most conditions. As a bonus, it was also the most algebraically simple. Therefore, Hay's anisotropic hourly model was selected as the best suited for this investigation.

2.6.3 Methodology for Comparison

Hourly radiation ratios were used to calculate the monthly-average daily radiation ratio. To accomplish this, the calculated hourly radiation ratios were multiplied by the actual horizontal radiation, giving the insolation levels on the tilted surfaces. The tilted and horizontal insolations were then summed for all daylight hours over every day of the month, to obtain monthly values. By dividing the total tilted insolation by the total horizontal insola-

tion, the monthly-average daily radiation ratio was obtained. This method is similar to the algorithm used by TRNSYS.

As in the diffuse fraction comparison (section 2.6.1), hours with a sunrise or sunset were neglected. Also, only hours composed of 60 "good" minutes of data were considered. To insure equal weighting of the radiation ratio numerator and denominator, the summations were skipped if either horizontal or tilted data were invalid. Due to different total hours with valid data for each tilted instrument, the tilted insolation and the horizontal insolation summations were made separately for each slope. Summations using data derived diffuse fractions also included a check for valid NIP values.

The monthly-average hourly model is based on the "average day" of the given month, as defined by Duffie and Beckman [5]. Therefore, summation of the hourly values was only required over the complete daylight hours of this day. Interest in this model developed from its use in Clark's Utilizability correlation.

Hay's modification to the hourly isotropic model can be written as:

$$R = \frac{I_d}{I} (1 - A) \left(\frac{1 + \cos \beta}{2} \right) + \left(1 - \frac{I_d}{I} (1 - A) \right) R_b + \rho \left(\frac{1 - \cos \beta}{2} \right) \quad (2.16)$$

where A is the anisotropic index. Hay defined his anisotropic index as the ratio of normal incident beam radiation to the normal extra-terrestrial incident radiation. Multiplying both terms by the cosine of the zenith angle converts the index from normal values to horizon-

tal values, or:

$$A = \frac{I_{NIP} \cos \theta_z}{I_o} \quad (2.17)$$

Since $I_{NIP} \cos(\theta_z)$ equals the beam radiation on a horizontal surface, this term can be rewritten as:

$$I_{NIP} \cos(\theta_z) = I - I_d . \quad (2.18)$$

Substituting Eq. (2.18) into (2.17) and multiplying the numerator and denominator by I , gives:

$$A = \frac{(I - I_d)}{I} \left(\frac{I}{I_o} \right) \quad (2.19)$$

Recognizing I/I_o as the hourly clearness index k_T , Hay's anisotropic index can be rewritten as:

$$A = \left(1 - \frac{I_d}{I} \right) k_T \quad (2.20)$$

This is now in a form that can use the hourly diffuse fraction.

The monthly-average hourly isotropic model shown in Eq. (2.8) requires a monthly-average hourly diffuse fraction. This hourly diffuse fraction can be calculated from Erbs' monthly-average daily diffuse fraction - Eq. (2.14), using the ratios r_d and r_t :

$$\frac{I_d}{I} = \left(\frac{r_d}{r_t}\right) \left(\frac{H_d}{H}\right) \quad (2.21)$$

where $r_d = \frac{\text{hourly diffuse radiation}}{\text{daily diffuse radiation}}$

and $r_t = \frac{\text{hourly total radiation}}{\text{daily total radiation}}$

The r_d/r_t ratio is a function of the hour angle ω , and the sunset hour angle ω_s [5]. Dividing out common terms, r_d/r_t can be written as:

$$\frac{r_d}{r_t} = \frac{1}{a + b \cos(\omega)} \quad (2.22)$$

where $a = 0.409 + 0.5016 \sin(\omega_s - 60),$

and $b = 0.6609 - 0.4769 \sin(\omega_s - 60).$

Equations (2.8), (2.14), and (2.21) provide a simple method to calculate \bar{R} from monthly-average hourly correlations, based only on \bar{K}_T and geometry. The horizontal radiation component of \bar{K}_T was calculated from actual data, over all valid hours of horizontal data.

2.6.4 Comparison of Monthly-Average Daily Radiation Ratios

Figures 2.3 through 2.22 show the results of the monthly-average daily radiation ratio calculations. These graphs and their discussions are broken into four groups: slope = latitude; slope = 90°S; slope = 90°E and slope = 90°W; and slope = 90°N orientations. Each

FIG. 2.3 \bar{R}'_s (I_d/I FROM ERBS' CORR.)

San Antonio, TX Slope = Lat.

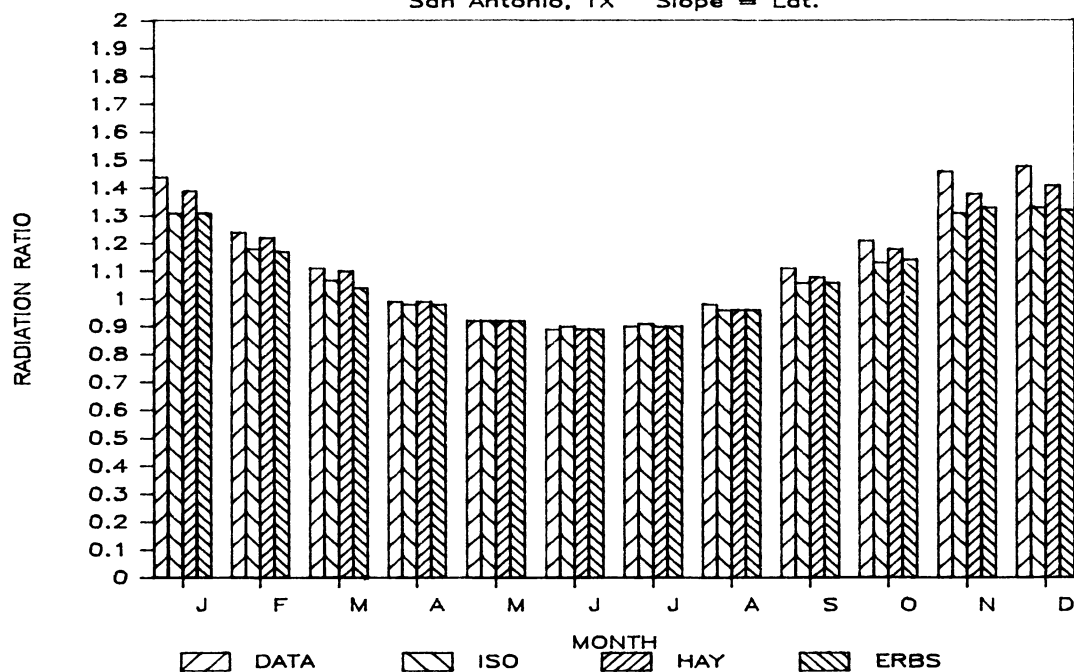


FIG. 2.4 \bar{R}'_s (I_d/I FROM NIP DATA)

San Antonio, TX Slope = Lat.

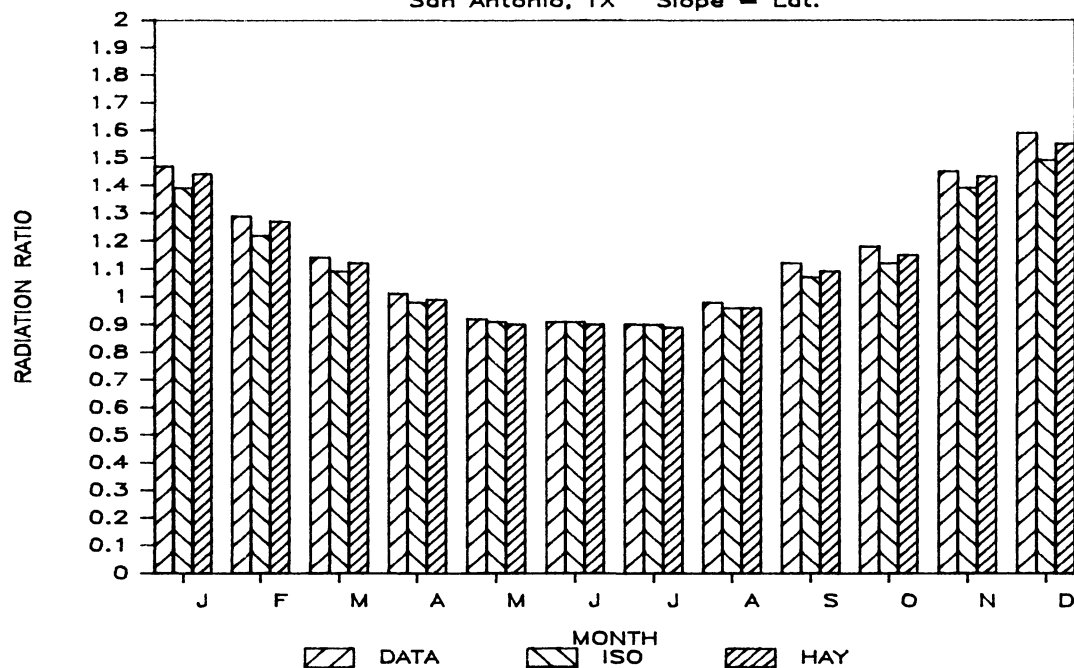


FIG. 2.5 \bar{R} 's (I_d/I FROM ERBS CORR.)

Albany, NY Slope = Lat.

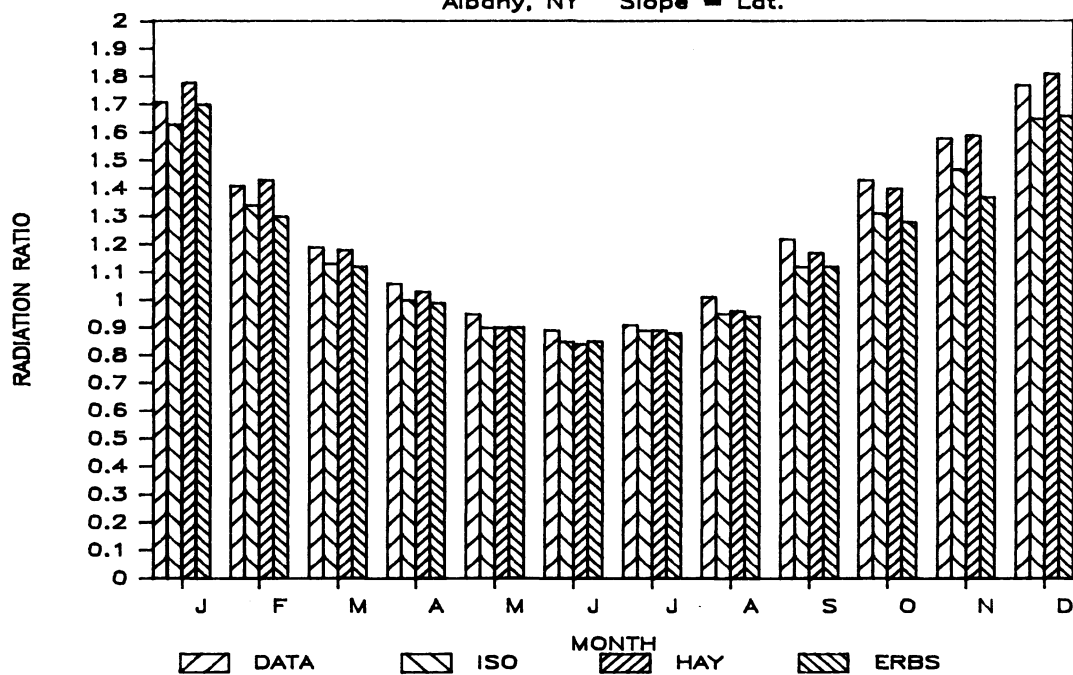


FIG. 2.6 \bar{R} 's (I_d/I FROM NIP DATA)

Albany, NY Slope = Lat.

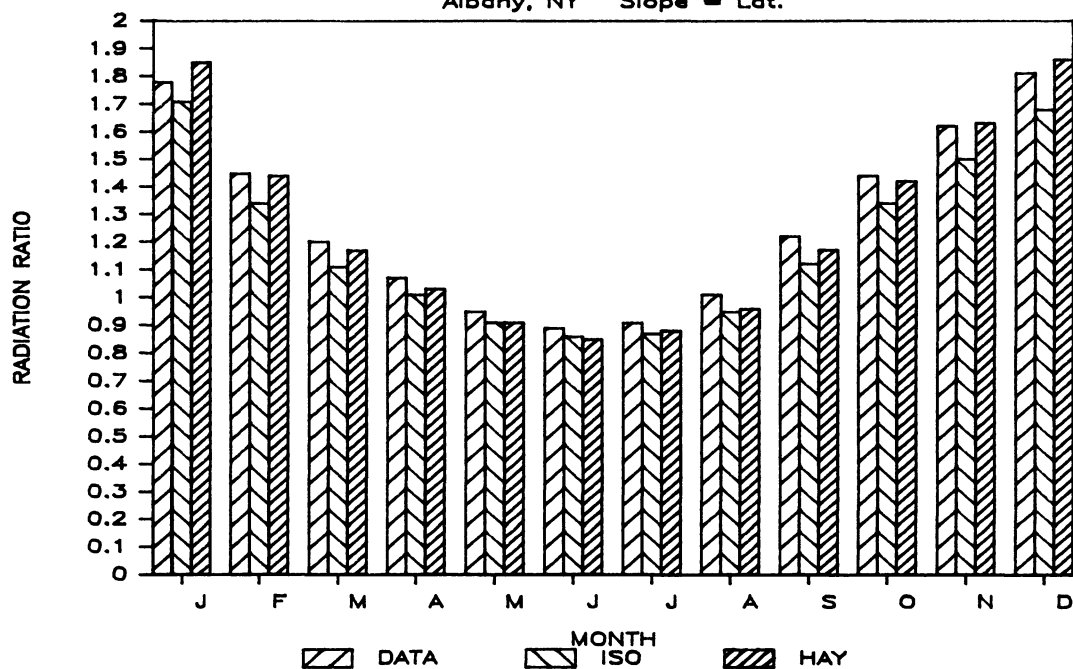
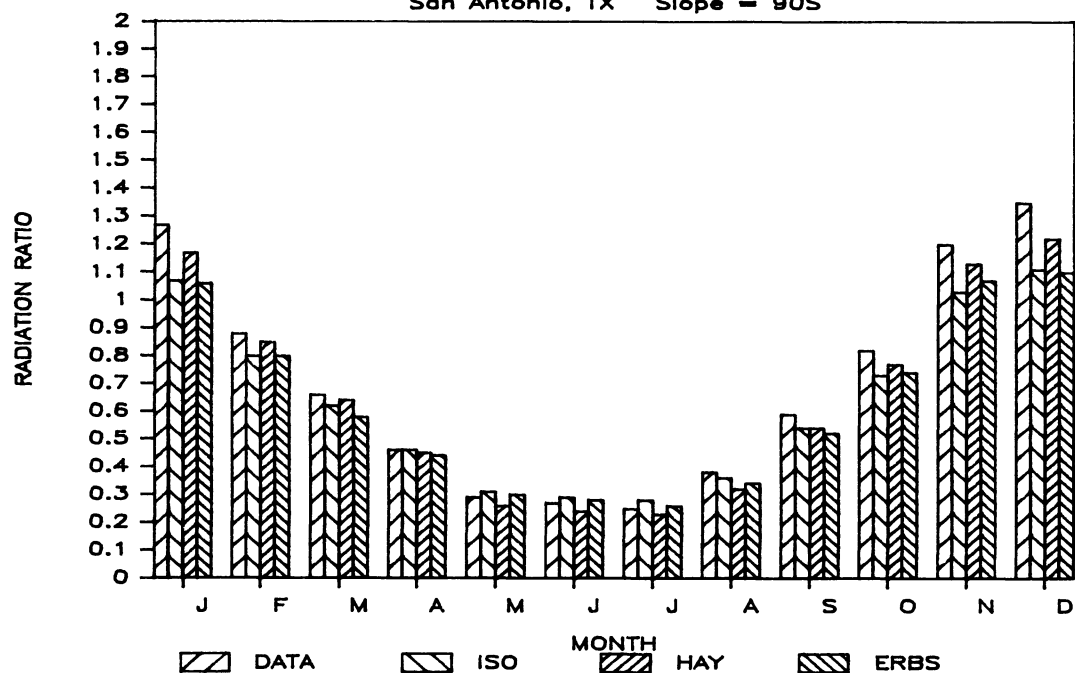


FIG. 2.7 \bar{R} 's (I_d/I FROM ERBS CORR.)

San Antonio, TX Slope = 90S

FIG. 2.8 \bar{R} 's (I_d/I FROM NIP DATA)

San Antonio, TX Slope = 90S

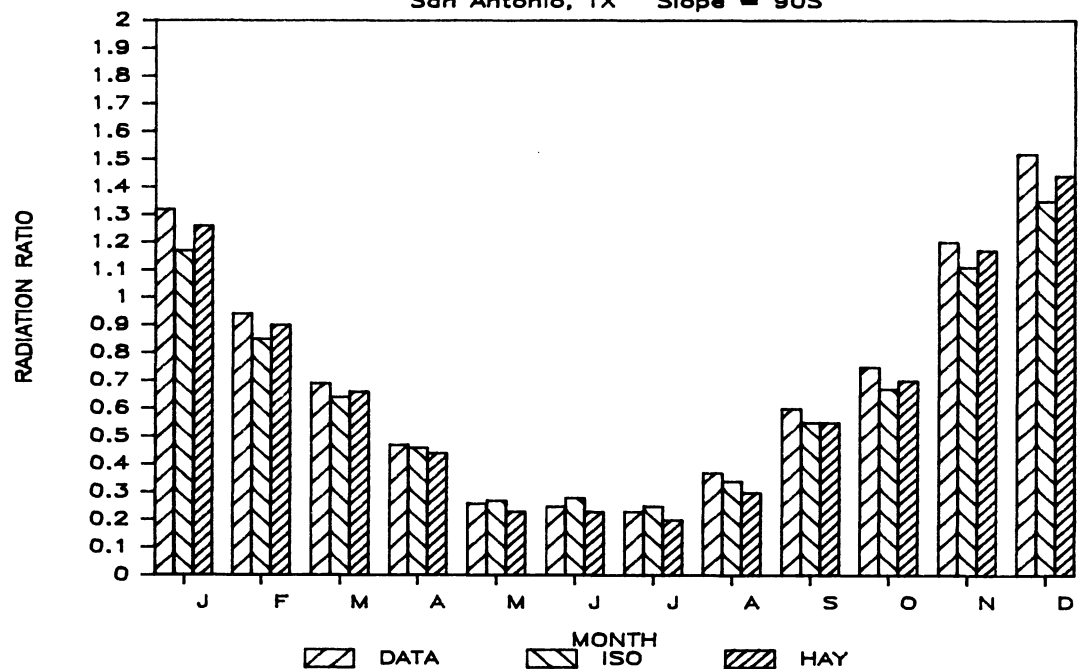


FIG. 2.9 \bar{R} 's (I_d/I FROM ERBS CORR.)

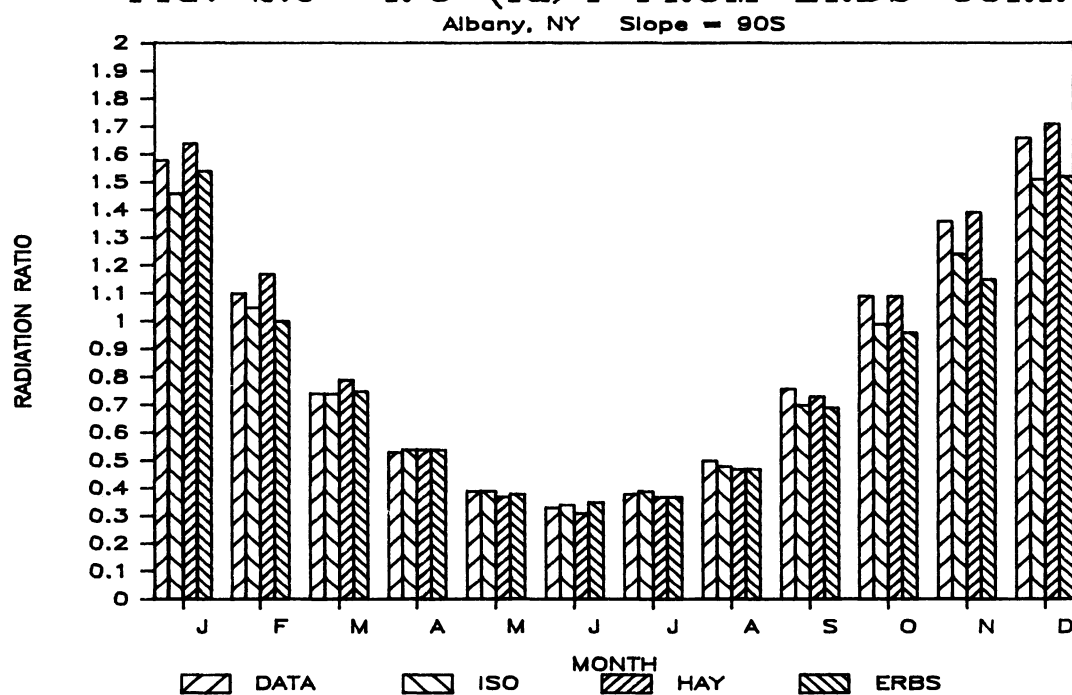


FIG. 2.10 \bar{R} 's (I_d/I FROM NIP DATA)

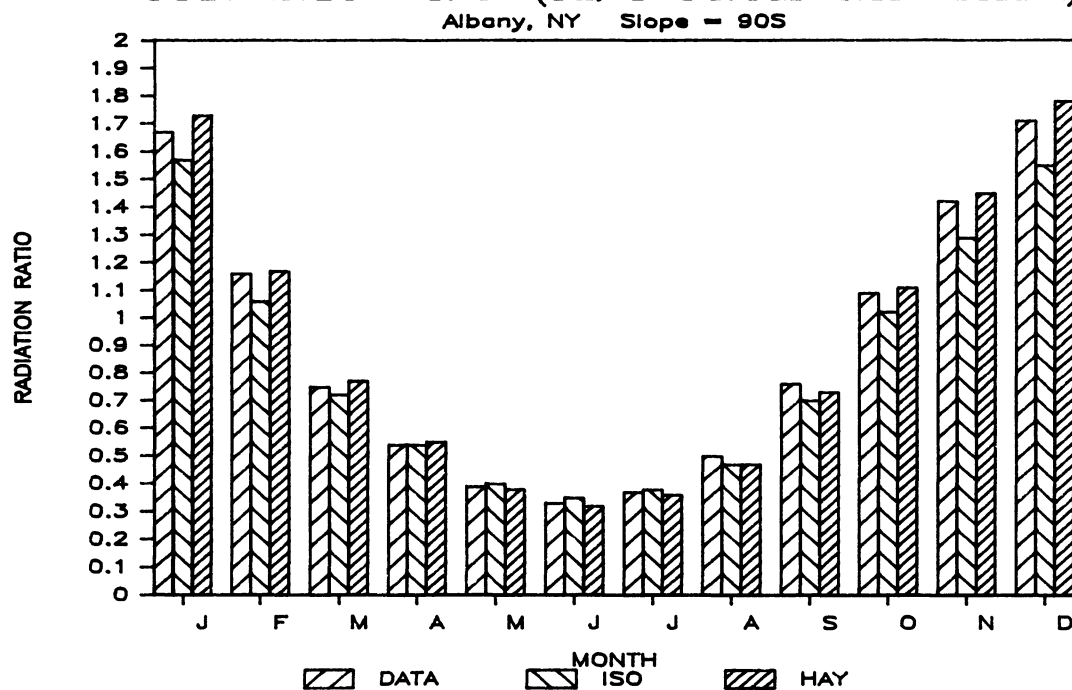
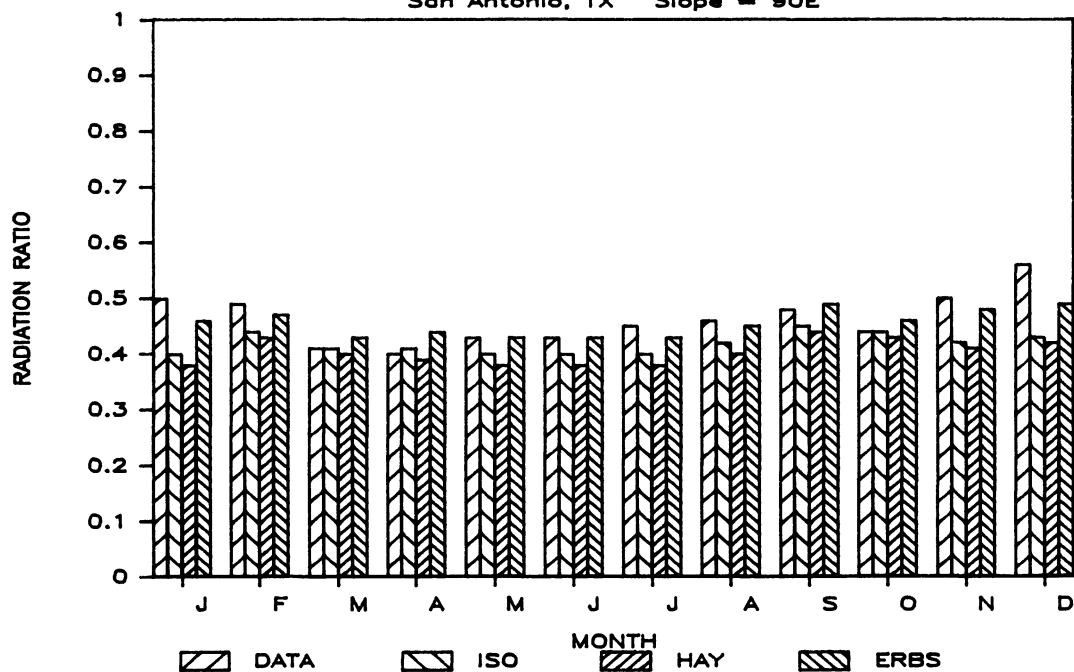


FIG. 2.11 \bar{R} 's (I_d/I FROM ERBS CORR.)

San Antonio, TX Slope = 90E

FIG. 2.12 \bar{R} 's (I_d/I FROM NIP DATA)

San Antonio, TX Slope = 90E

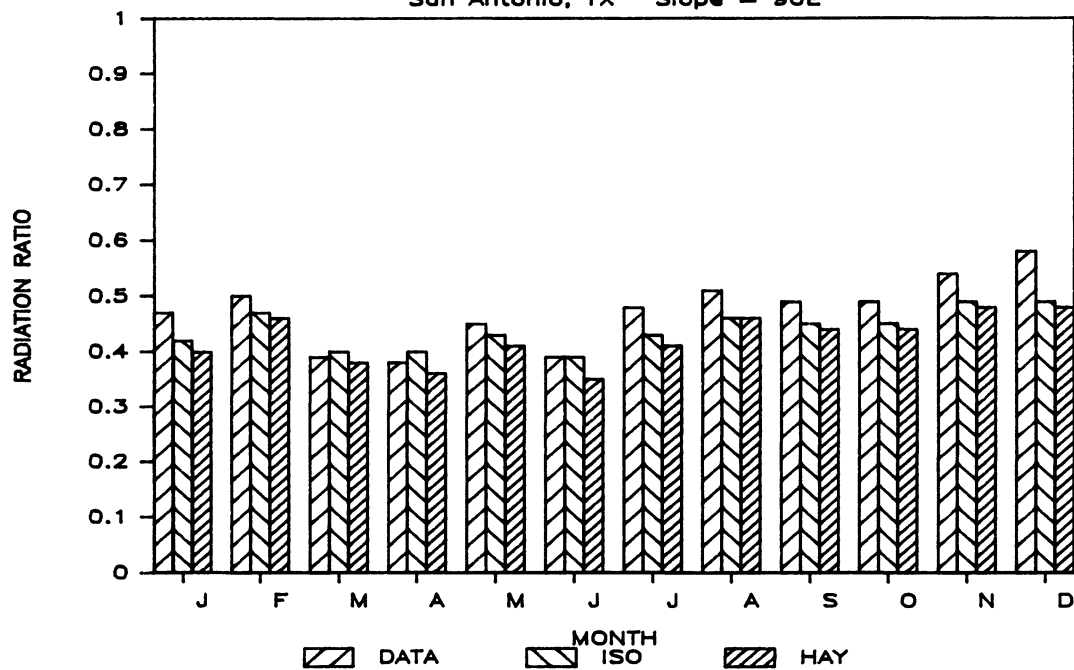


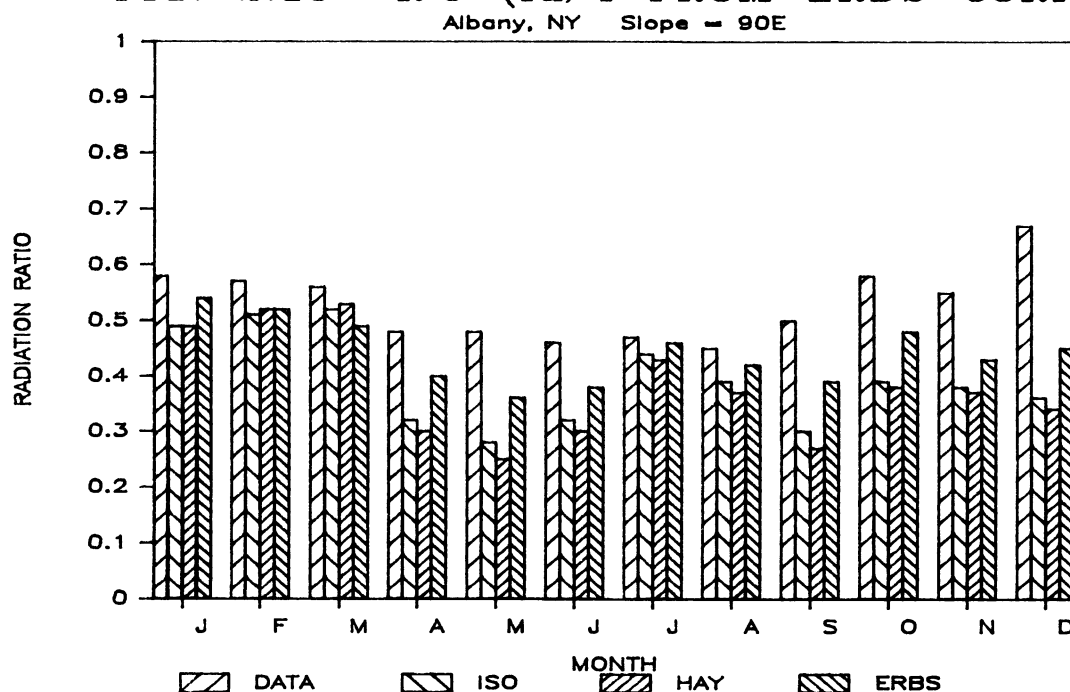
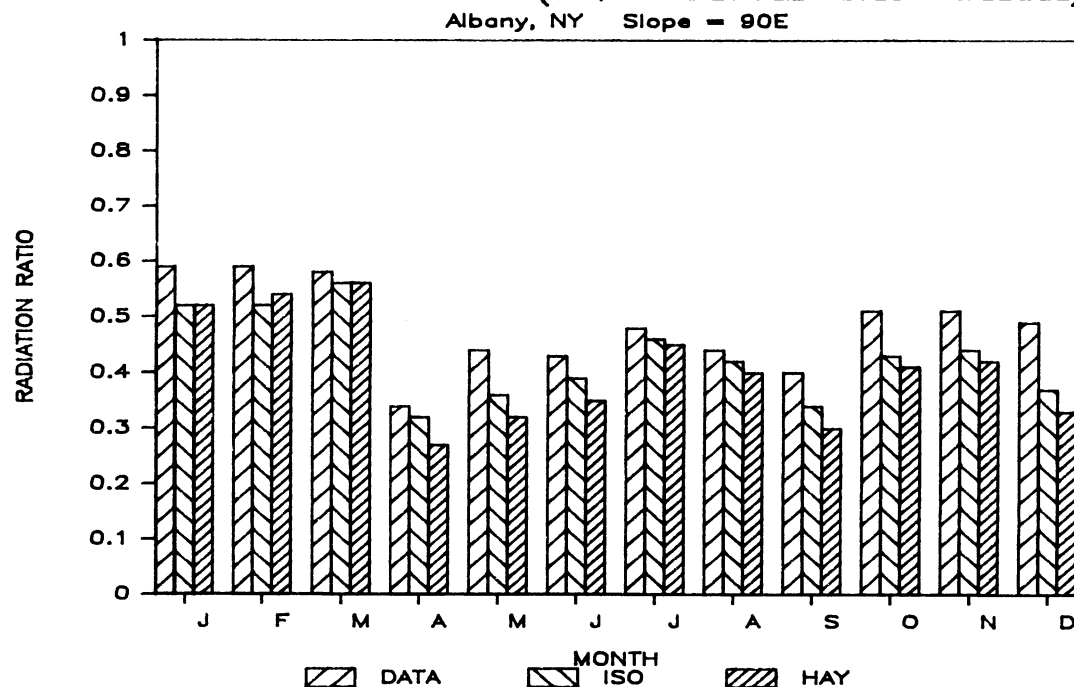
FIG. 2.13 \bar{R} 's (I_d/I FROM ERBS CORR.)FIG. 2.14 \bar{R} 's (I_d/I FROM NIP DATA)

FIG. 2.15 \bar{R} 's (I_d/I FROM ERBS CORR.)
San Antonio, TX Slope = 90W

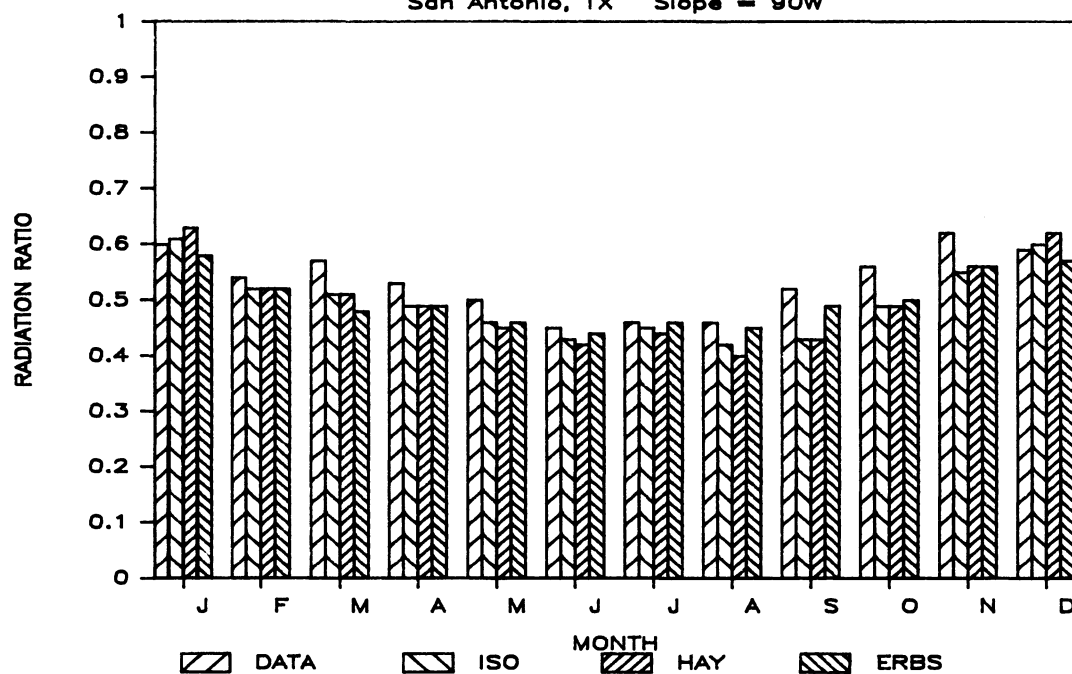


FIG. 2.16 \bar{R} 's (I_d/I FROM NIP DATA)
San Antonio, TX Slope = 90W

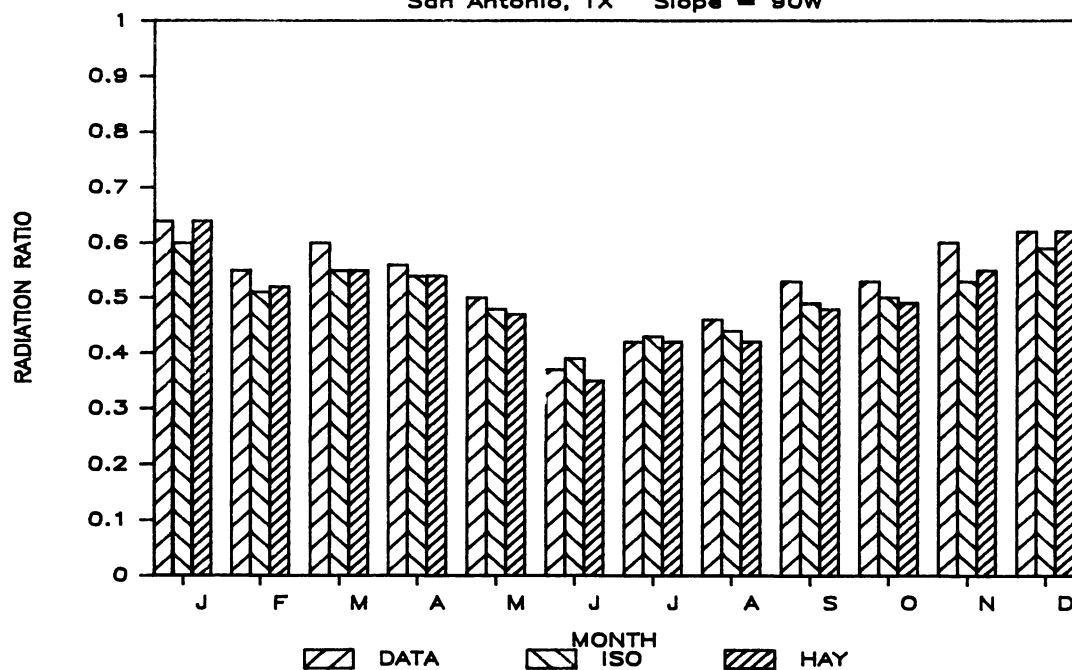
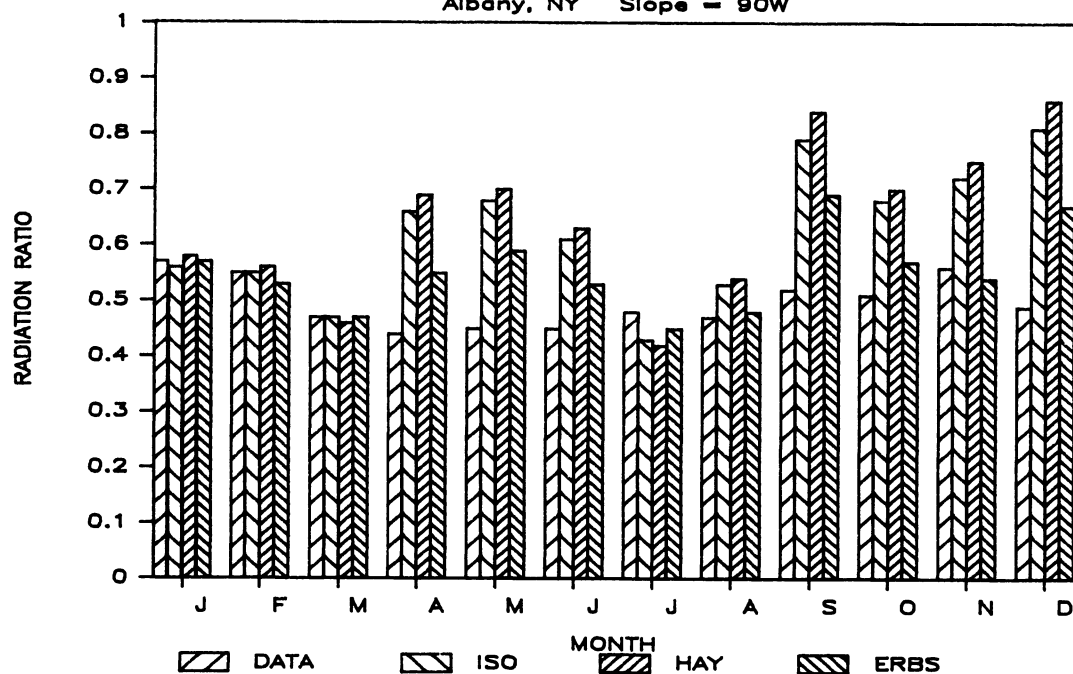


FIG. 2.17 \bar{R} 's (I_d/I FROM ERBS CORR.)

Albany, NY Slope = 90W

FIG. 2.18 \bar{R} 's (I_d/I FROM NIP DATA)

Albany, NY Slope = 90W

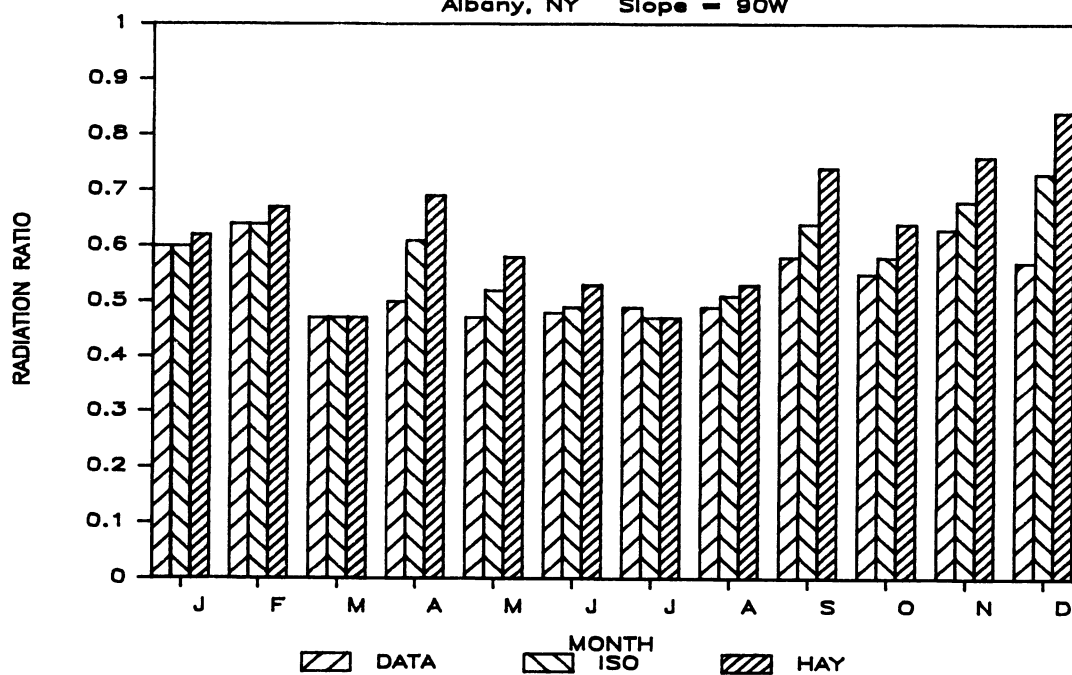


FIG. 2.19 \bar{R} 's (I_d/I FROM ERBS CORR.)

San Antonio, TX Slope = 90N

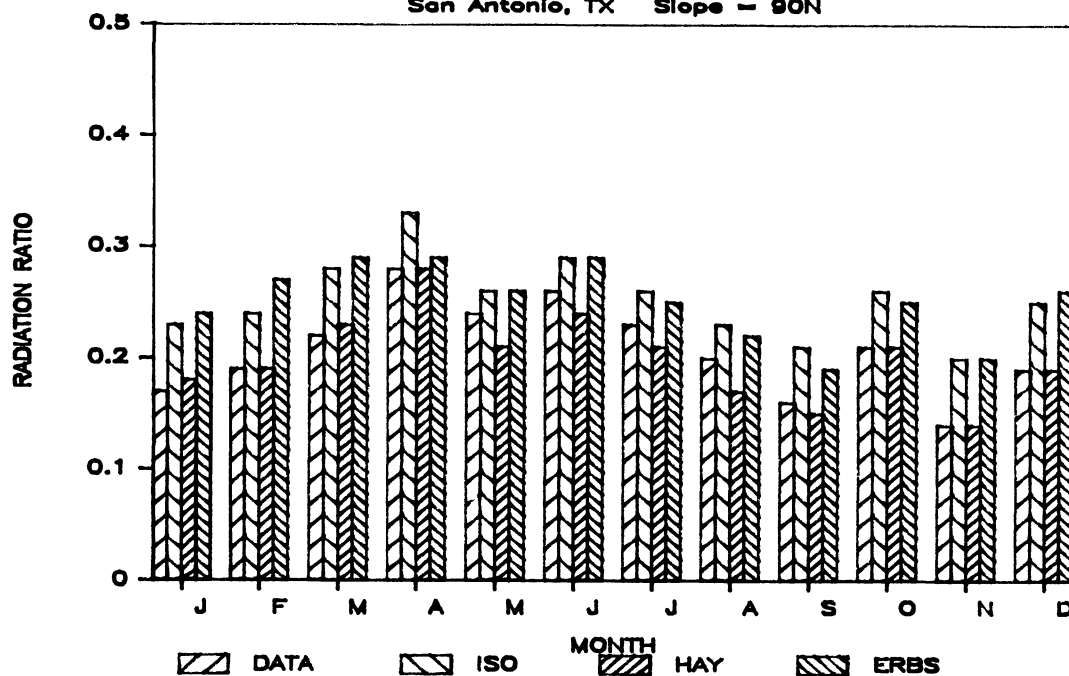


FIG. 2.20 \bar{R} 's (I_d/I FROM NIP DATA)

San Antonio, TX Slope = 90N

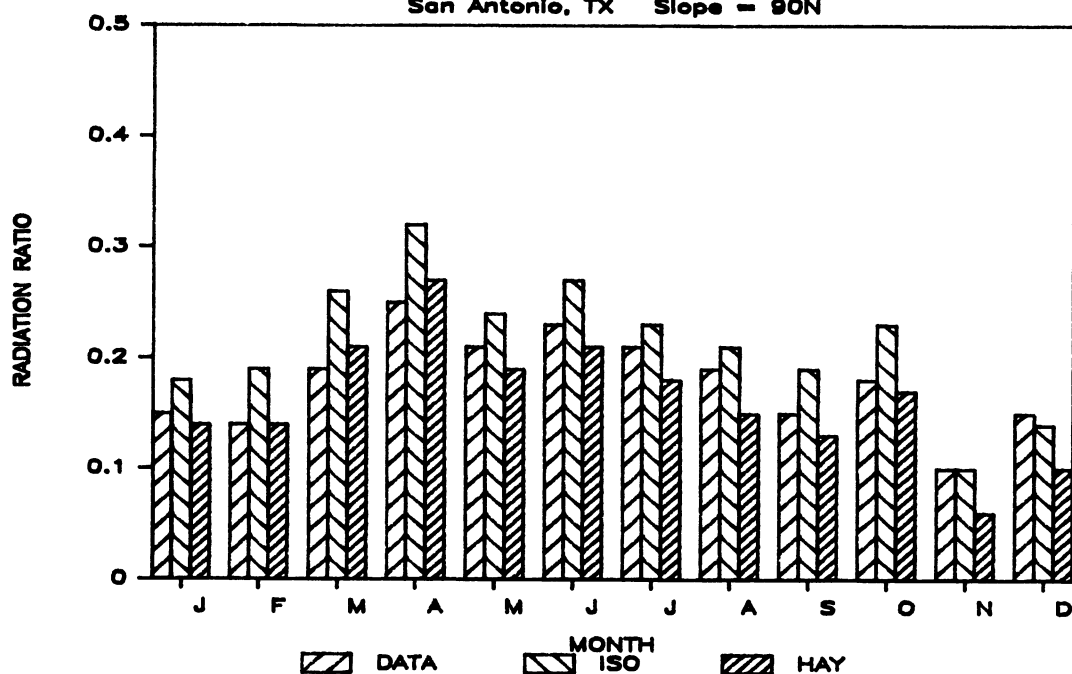


FIG. 2.21 \bar{R}'_s (I_d/I FROM ERBS CORR.)

Albany, NY Slope = 90N

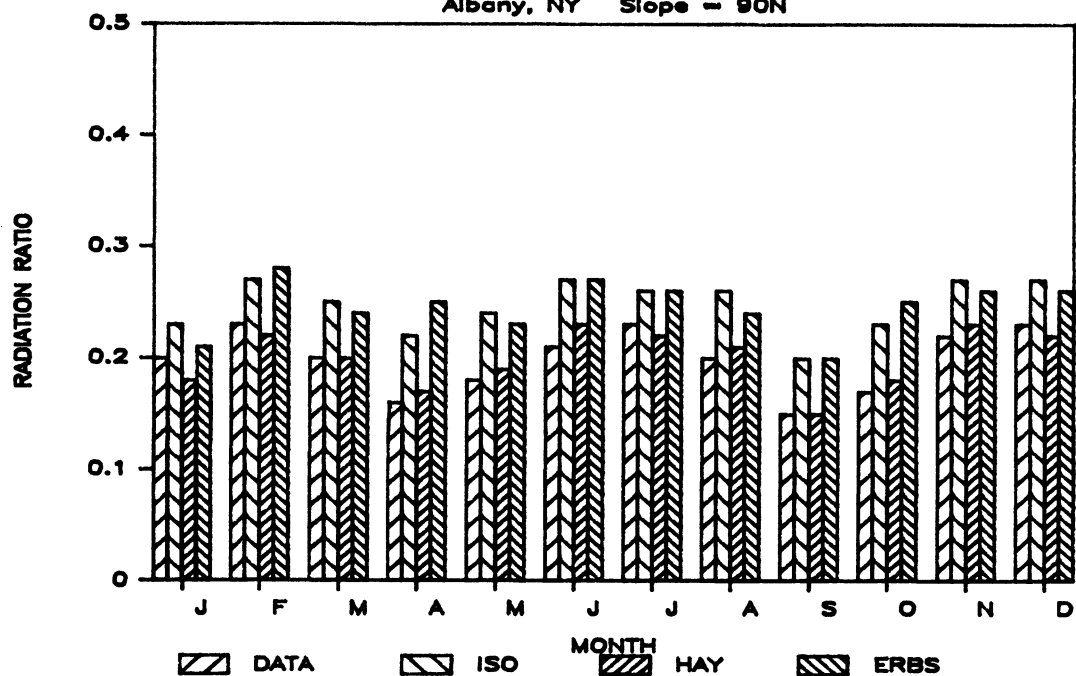
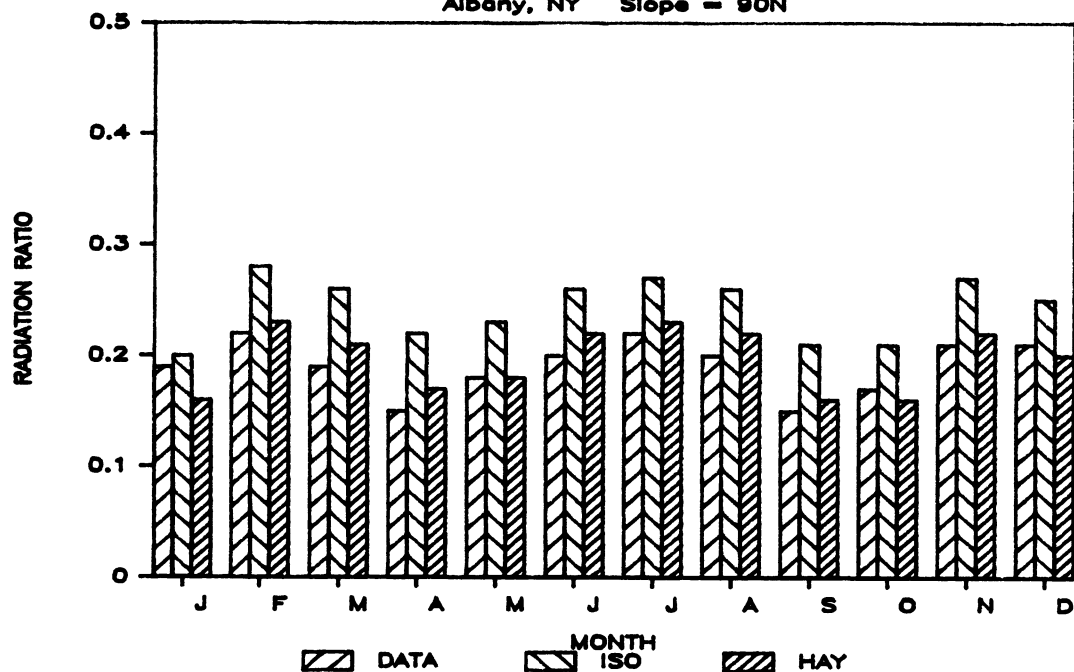


FIG. 2.22 \bar{R}'_s (I_d/I FROM NIP DATA)

Albany, NY Slope = 90N



group contains the San Antonio and Albany results, as found from both Erbs hourly correlation and data derived hourly diffuse fractions.

The bar graph legends used in these comparisons are as follow:

Data = \bar{R} calculated from actual insolation measurements;

Iso = \bar{R} calculated from the hourly isotropic model, Eq. (2.6);

Hay = \bar{R} calculated from the Hay hourly anisotropic model, Eq. (2.16);

Erbs = \bar{R} calculated from the monthly-average hourly isotropic model, Eq. (2.8), using Erbs' monthly-average daily diffuse fraction, Eq. (2.14).

In general, the same trends between the various models for calculating \bar{R} is seen using either diffuse fraction method. The values usually change slightly, as expected for methods using a different amount of data. Due to a large number of invalid NIP values, the number of hours used to calculate \bar{R} from data derived diffuse fractions was relatively small. In comparison, the number of valid hours using Erbs' hourly diffuse fraction was approximately equal to the number of hours with valid global horizontal data. Consequently, it could not be determined if the difference in \bar{R} values was caused by the methodology used for calculating the diffuse fraction, or from the change in the data base size.

In a few cases where the hourly isotropic and Hay anisotropic results were close, the "better" model would switch, depending on which method was used to calculate the diffuse fraction. However,

considering the small differences between the isotropic and Hay results, both radiation ratio models can actually be considered equal for these limited cases.

Unless otherwise indicated, the following discussions will be centered around the results from the Erbs diffuse fraction method, since it incorporated the larger data base.

A. Surface Slopes Equal to Latitude

Slopes tilted at angles equal to the latitude probably have the largest engineering interest. For these slopes, graphs 2.3 through 2.6 show the Hay anisotropic model best matches the actual data values. Out of the 24 months studied, only once did it perform worse than the isotropic model. In that case, the difference in isotropic and anisotropic values was only 1.2%, while the difference between actual and anisotropic values was 6%. The worse performance for the Hay anisotropic model was this underestimation of 6% (June in Albany). For three of the Albany winter months, the Hay model overestimated the actual value by as much as 4%.

The isotropic model error was largest during the fall and winter months. In San Antonio, the isotropic model underestimated the data value by as much as 10% in both November and December, and by 8% in September and October for Albany. In comparison, the Hay model underestimated the data values by 5% for San Antonio, and 2 to 4% for Albany. In general, the isotropic model performed its best during the summer months, although it still underestimated by 4% during June (Albany). In all cases for surface slope equal to latitude, the iso-

tropic model never overestimated the actual \bar{R} values. This underestimation can be attributed to the lack of a circumsolar diffuse radiation component in the isotropic model.

The monthly-average hourly radiation ratio values using Erbs monthly-average daily diffuse fraction generally agreed with the hourly isotropic model values. In a few cases it gave poorer results, the worst being an underestimation of the actual value by 13%. A poorer performance is expected for any "quick" method, when compared to the numerically integrated hourly model values.

B. Surface Slopes at 90 South

Vertical surfaces probably have the largest architectural interest, due to windows. For these slopes, Figures 2.7 through 2.10, show similar results as the surface slopes equal to the latitude. In general, the Hay model better estimated the data \bar{R} values. The isotropic model performed poorest during the winter, with underestimated values as large as 9% for Albany, and 18% for San Antonio. For those same months, the Hay model overestimated by 3% for Albany, and underestimated by 10% for San Antonio.

In a few summer cases, the isotropic model overestimated by as much as 12% (San Antonio), while the Hay model underestimated by 8% for the same month. However, these are large percentages of small radiation ratios, i.e. 0.25 for the case mentioned. Therefore, the effect of these errors on the resulting tilted insolation values are not significant, when compared to the magnitude of the initial horizontal insolation levels. Consequently, considering the overall

minimal change in \bar{R} , both hourly methods can be considered equivalent for these cases.

The \bar{R} values calculated from the monthly-average hourly isotropic model once again tended to closely match the hourly isotropic model values. The worst comparisons to the actual values were underestimations by 15% for November in Albany, and 19% for December in San Antonio.

C. Surface Slopes at 90° East and 90° West

Figures 2.11 through 2.18 show the \bar{R} 's calculated for surface slopes at 90° East and 90° West. For the east-facing surfaces, all models typically underestimated the actual values. This can be attributed to the lack of a horizon brightening diffuse radiation term. Typically, the isotropic model was usually slightly better than the Hay model, for both San Antonio and Albany. Surprisingly, the monthly-average hourly model tended to be the best of all three correlations.

The largest errors for the east-facing surfaces were during the winter months. The worst case was December in Albany, where both the isotropic and Hay models were low by 48%. In comparison, calculations using the NIP diffuse fraction showed a 39% error. However, the reduction in error using NIP data was accomplished by changing the magnitude of the data \bar{R} , and not the magnitude of the \bar{R} 's from the hourly isotropic and Hay models. Since the data \bar{R} is a ratio of tilted insolation values to horizontal values, one or both of these values must have greatly fluctuated between the two diffuse fraction

data bases. The hourly models require global horizontal data and either Erbs I_d/I or data I_d/I . However, the magnitudes of the isotropic and Hay model \bar{R} 's remained fairly constant, and therefore the global horizontal and NIP values remained fairly consistent between both diffuse fraction data bases. By default, the tilted insolation data must have been the greatly fluctuating value. Since the east-facing data are the only large-scale varying values, instrument error is indicated for the winter months.

San Antonio also had larger errors in the hourly models during the winter months, but only in the 25% range - which is still a large error. The summer month values were better at approximately 10% underestimation for the hourly models. The \bar{R} magnitudes between Erbs and the NIP diffuse fractions methods were similar.

The west-facing surfaces in San Antonio provided fairly good results for both hourly models. The exception was for September, where both the isotropic and Hay models underestimated the data result by 17%. However, in Albany both the isotropic and Hay models showed some drastic errors compared to the actual values. The worst case is for December, where the isotropic and Hay models overestimated by 65% and 76%, respectively. September also showed a severe overestimation with 52% and 62%. The isotropic and Hay models using the NIP diffuse fraction have slightly smaller winter time errors than the models using Erbs' diffuse fraction.

The reasons for these large \bar{R} model errors in only the Albany west-facing results are unknown. The overestimation for a west-

facing surface contradicts the horizon brightening theory, and the inconsistency between the west-facing and east-facing results are puzzling. Further investigation needs to be made, to see if these errors are from instrument failure, or if some other phenomenon is occurring.

D. Surface Slopes at 90° North

Figures 2.19 through 2.22 show the \bar{R} results for surfaces sloped at 90° North. The first observation is the expected low magnitude of the monthly-average daily radiation ratios. In most cases, the actual \bar{R} values are around 0.2 for both San Antonio and Albany. Therefore, any "large" errors result in small changes in the tilted surface values compared to the magnitudes of the initial horizontal radiation. However, the Hay model did give excellent estimates of the actual \bar{R} values for most cases. In general, both the isotropic model and the monthly-average hourly model noticeably overestimated by equal amounts.

2.7 Conclusions

The \bar{R} 's analyzed represent a relatively small, and short term data base. Nonetheless, comments can still be made on the results obtained.

For the two locations studied, Erbs' hourly diffuse fraction correlation usually misestimated actual monthly-average daily diffuse fractions by 3 to 5% of the maximum fraction. The largest error was 10%. Comparison between Erbs' and data hourly diffuse fractions

showed poorer agreement. Typical monthly RMS errors were around 0.18, the maximum being 0.32.

Hay's hourly anisotropic radiation ratio model usually provided better estimates of the actual monthly-average daily radiation ratio, then the isotropic hourly model. The best improvements by using the Hay model were for south-facing surfaces during winter months. For surfaces tilted at angles equal to the latitude, the isotropic model underestimated measured values as much as 10%, compared to 5% for the Hay model. For solar heating systems, these are the critical design conditions.

During summer months, both models provided closer results to actual data. Under a few conditions, the difference between the Hay model results and the isotropic model results is insignificant, due to the small \bar{R} magnitudes. For east and west surfaces, the isotropic model was usually slightly better than the Hay model.

The Hay model is easy to implement, and provided no "practical" penalties.

3. CLEARNESS INDEX FREQUENCY DISTRIBUTIONS

3.1 General Description

The ratio of terrestrial to extraterrestrial radiation received on a horizontal surface is commonly called the "clearness index". This concept was originally developed by Liu and Jordan [21] under the title of "cloudiness index", since the value is largely dependent upon the amount of clouds. However, the ratio increases for increasing atmospheric clearness, and therefore many sources have referred to it as the clearness index.

The hourly clearness index is noted as k_T , where by definition:

$$k_T = \frac{I}{I_0} \quad (3.1)$$

An analytical equation for I_0 was previously given as Eq. (2.13). Similarly, the daily clearness index K_T is defined as:

$$K_T = \frac{H}{H_0} \quad (3.2)$$

where the analytical equation for H_0 can be found in Duffie and Beckman [5].

Useful parameters are the monthly-average values of the hourly and daily clearness indexes. The monthly-average clearness index is the ratio of monthly-average terrestrial to extraterrestrial radiation for the hour or daily period, which can be found by summing the

individual quantities over a month. The monthly-average hourly clearness index is defined as:

$$\bar{k}_T = \frac{(\sum^N I)/N}{(\sum^N I_0)/N} = \frac{\bar{I}}{\bar{I}_0} \quad (3.3)$$

where N = the number of days in a month. In similar fashion, the monthly-average daily clearness index is defined as:

$$\bar{K}_T = \frac{(\sum^N H)/N}{(\sum^N H_0)/N} = \frac{\bar{H}}{\bar{H}_0} \quad (3.4)$$

Liu and Jordan [21] found that the cumulative distributions of the daily clearness indexes formed similar curves for a given monthly-average daily value. These curves represent the fraction of time the daily clearness index is at or below a given value during a month. Figure 3.1 shows the Liu and Jordan curves, which were developed for the five monthly-average values shown.

Whillier [35] found the hourly distributions were also similar to the daily distributions. In a later study, Theilacker [34] showed the hourly distributions to be slightly "steeper" - a larger slope for part of the distribution - than the daily distributions. An increase in slope results in larger changes in the clearness index for a given increment of the fractional time. This increase in the clearness index corresponds to the higher probability of having one hour that is completely sunny or completely cloudy, than an entire day that is completely sunny or completely cloudy.

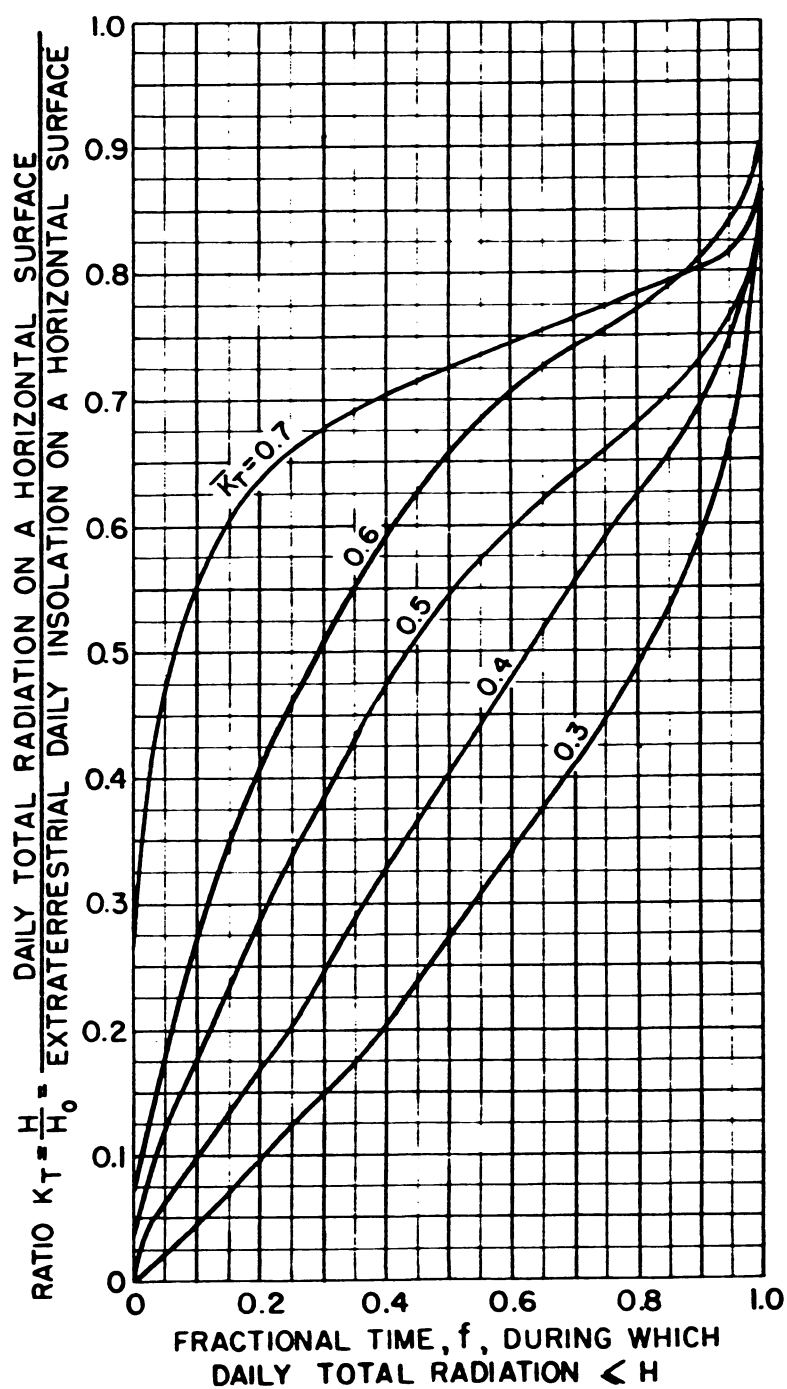


Figure 3.1: Liu and Jordan Cumulative Daily Clearness Frequency Distributions.
From Liu and Jordan [22]

Although the hourly distributions were slightly steeper than the daily distributions found by Liu and Jordan, Theilacker showed that they still had almost the same form. The exception was at fractional times approaching 1.0. Theilacker's curves had a flatter slope at these higher fractions, instead of the sudden approach to $k_T = 1$ as in the Liu and Jordan distributions. Theilacker also showed some seasonal and locational dependencies, but still within the same general curve shape. Although the hourly distributions did vary slightly from the daily distributions, generalized hourly distributions were not, and still are not available. However, Theilacker did conclude that the hour distributions could still be reasonably well represented by the Liu and Jordan curves.

Bendt et al. [1] compared the Liu and Jordan curves to a data base from 90 different locations. The two sets of daily clearness index curves were very similar, except at the high fractions. As shown in Theilacker's work, the Bendt data lacked the sudden change in slope at large fractional times. Next Bendt et al. developed a clearness distribution function based on probability theory for random insolation sequences. This distribution followed the data set extremely well, and also lacked the Liu and Jordan "tail" - the sudden increase in clearness indexes at high fractions.

For this present study, the Bendt distribution is used to compare the clearness frequency distribution from the San Antonio and Albany data. This decision is based on their use of a large data

set, the better representation at high fractions, and the analytical form of the required equations.

Clearness indexes are used extensively as the independent parameter in many solar correlations. They are useful for describing atmospheric conditions, and therefore have been used to find diffuse to total insolation fractions - as shown in Chapter 2, and for finding utilizable energy - as shown in Chapter 4. Through insolation distribution assumptions [5], hourly insolation levels can be estimated from daily clearness indexes. The clearness frequency distributions are useful for calculating long-term insolation levels for a given month, based on monthly-average values. Because of its simplicity, atmospheric descriptiveness, and versatility, the clearness index has become one of the most important parameters in solar calculations.

3.2 The Bendt Frequency Distribution

The Bendt cumulative frequency distribution is a function of the desired clearness index K_T , a maximum clearness index K_{\max} , and a theoretically derived parameter from statistical mechanics γ . The fractional time for a given K_T was shown to be:

$$f(K_T) = \frac{\exp(\gamma K_{\min}) - \exp(\gamma K_T)}{\exp(\gamma K_{\min}) - \exp(\gamma K_{\max})} \quad (3.5)$$

where $K_{\min} = 0.05$. The K_{\max} term was found to be a function of the monthly-average clearness index, where:

$$K_{\max} = 0.6313 - 0.267 \bar{K}_T - 11.9 (\bar{K}_T - 0.75)^8 \quad (3.6)$$

The parameter γ can be found by solving an integrated equation of a probability function for \bar{K}_T [1], where:

$$\bar{K}_T = \frac{(K_{\min} - \frac{1}{\gamma}) \exp(\gamma K_{\min}) - (K_{\max} - \frac{1}{\gamma}) \exp(\gamma K_{\max})}{\exp(\gamma K_{\min}) - \exp(\gamma K_{\max})} \quad (3.7)$$

Herzog [11] used Eqs. (3.6) and (3.7) to solve for γ for every 0.05 increment of \bar{K}_T between 0.3 and 0.7. He then derived the following equation for γ based on \bar{K}_T :

$$\gamma = -1.498 + [1.184 \Gamma - 27.182 \exp(-1.5 \Gamma)] / (K_{\max} - K_{\min}) \quad (3.8)$$

where $\Gamma = (K_{\max} - K_{\min}) / (K_{\max} - \bar{K}_T) .$

3.3 Frequency Calculation Methods from Data

Cumulative daily clearness frequency distributions show the fraction of time an individual daily clearness index is at or below a given value. Large fractional times indicate most days in the month are at or below a correspondingly large clearness index, while small fractional times indicate only a few days in the month are at or below the correspondingly small clearness index. Figure 3.1 shows this relationship between fractional time and daily clearness indexes. The relationship between fractional time and hourly clearness indexes are analogous to daily distributions.

The Albany and San Antonio hour data provided both daily and hourly clearness frequency distributions for a given month. The daily clearness frequency distributions were found by calculating the clearness index for each day and then sorting the indexes by increasing value. Since each clearness index represents one day, the cumulative fraction for a given clearness index is the day of the month, divided by the total number of days in the month. The hourly clearness frequency distributions were similarly made using the hourly clearness indexes for each day.

The cumulative frequency distributions for monthly-average hourly clearness indexes were also calculated using the minute data. Since most months have approximately 1860 minutes for a given hourly period, the "Bin Method" was used to simplify the output. Fifty "Clearness Index Bins" were created between 0 and 1, in 0.02 increments: i.e. Bin #1 was for $k_T = 0$ to 0.02; Bin #2 was for $k_T = 0.02$ to 0.04; etc. The clearness index was then calculated for each minute within the hourly period, and put into the appropriate bin. The cumulative number of clearness indexes was then found by summing the number of clearness indexes in each bin, along with the totals from each preceding bin. This gave the total number of clearness indexes at or below the clearness index for the midpoint of each bin. The cumulative fraction was then found by dividing the cumulative numbers for each bin, by the total number of clearness indexes. This method resulted in a workable number of points to describe the minute cumulative frequency distribution.

Short-term clearness indexes occasionally exceed 1.0, indicating that terrestrial radiation is exceeding extraterrestrial radiation for that period. Norris [25] suggested this peculiarity may be attributable to sunlight reflecting from the sides of clouds, concentrating the insolation over a small area. Since this phenomenon is rare, the clearness index scale on frequency distributions have always ranged between 0 and 1. In this study, any clearness indexes exceeding 1.0 were reset to 1.

The area under a cumulative clearness frequency distribution curve must equal the monthly-average clearness index. Due to the number of significant digits used in the following distribution plots, the actual areas shown may have errors as large as $\pm 2\%$.

3.4 Frequency Distributions for Hourly Periods

Figures 3.2 through 3.17 show some of the frequency distributions for a given monthly-average hourly clearness index. The graphs include minute and hourly clearness frequency distributions along with the Bendt correlation. The degree of superposition between the hour data and Bendt's correlation shows how closely the given month matches the accepted long-term average. Dissimilar curves indicate the hourly period within the month are not typical of long-term values. San Antonio and Albany both have some months that are similar to long-term distributions (Figs. 3.7-3.13 and 3.15) and other months that are dissimilar (Figs. 3.2-3.6 and 3.14). None of the hourly data distributions have the Liu and Jordan tail - k_T approaching 1 at large fractional times.

FIG. 3.2 kT FREQUENCY DISTRIBUTION

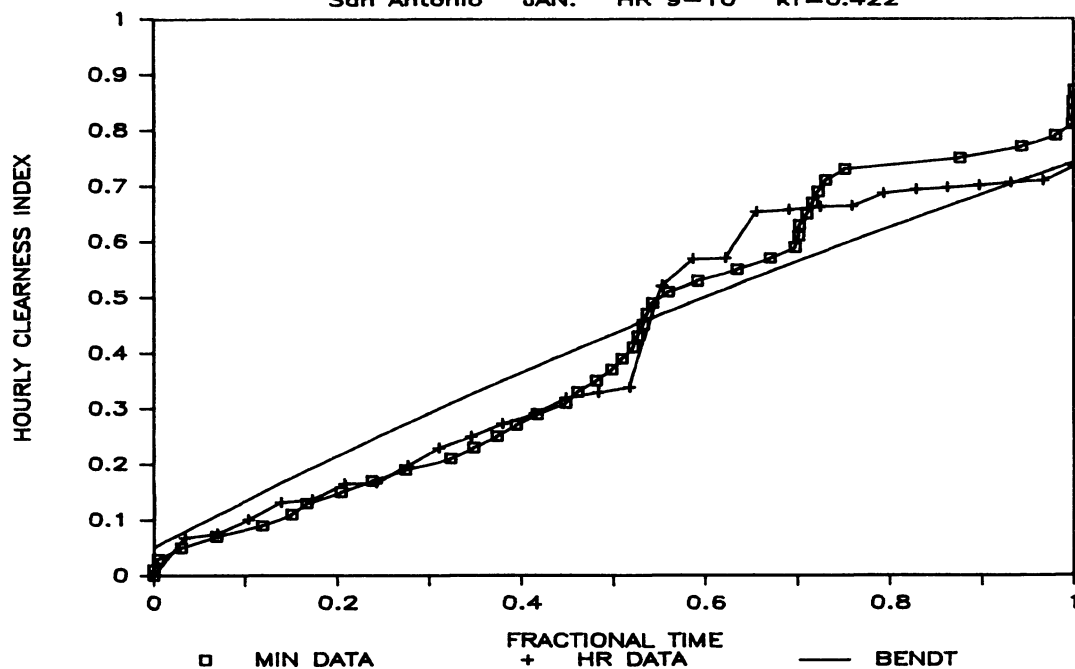
San Antonio JAN. HR 9-10 $kT=0.422$ 

FIG. 3.3 kT FREQUENCY DISTRIBUTION

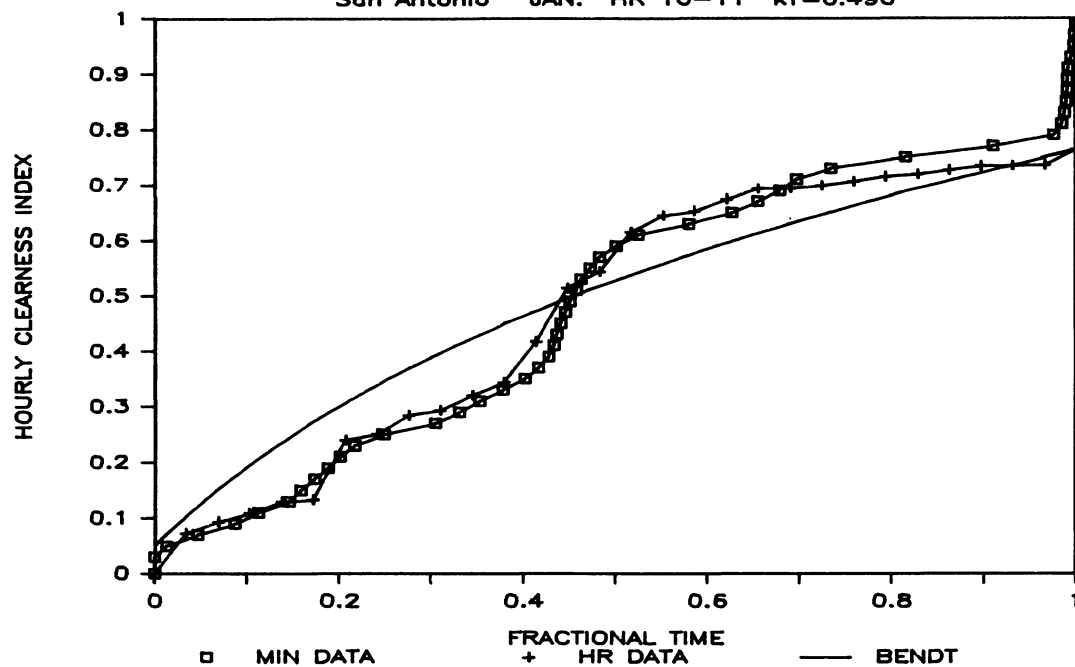
San Antonio JAN. HR 10-11 $kT=0.490$ 

FIG. 3.4 kT FREQUENCY DISTRIBUTION

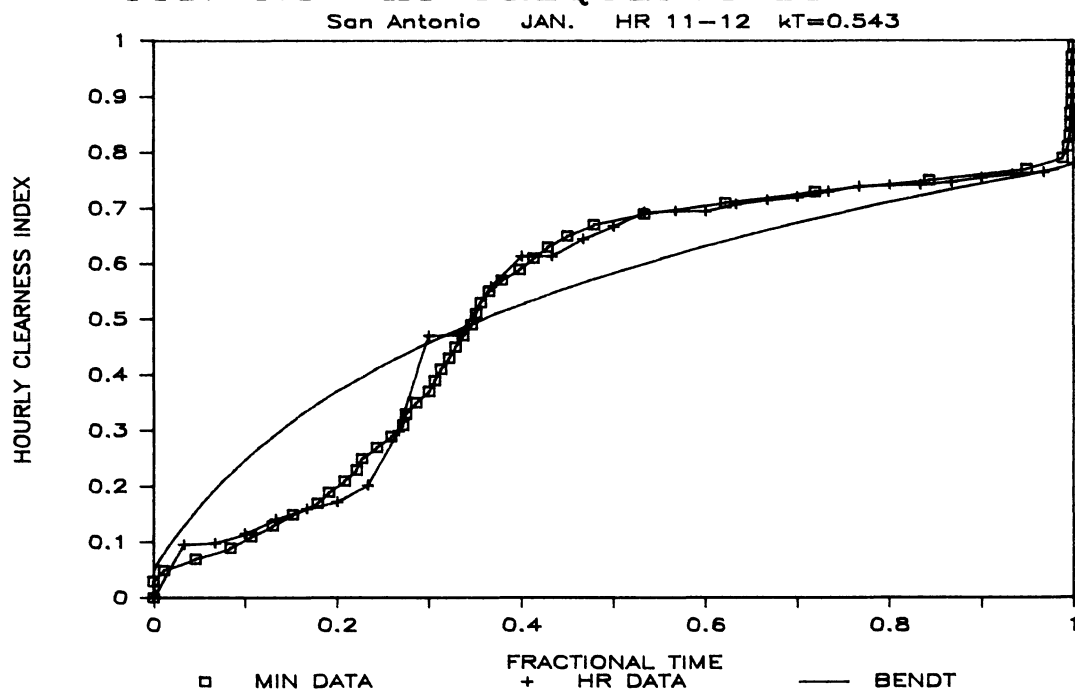
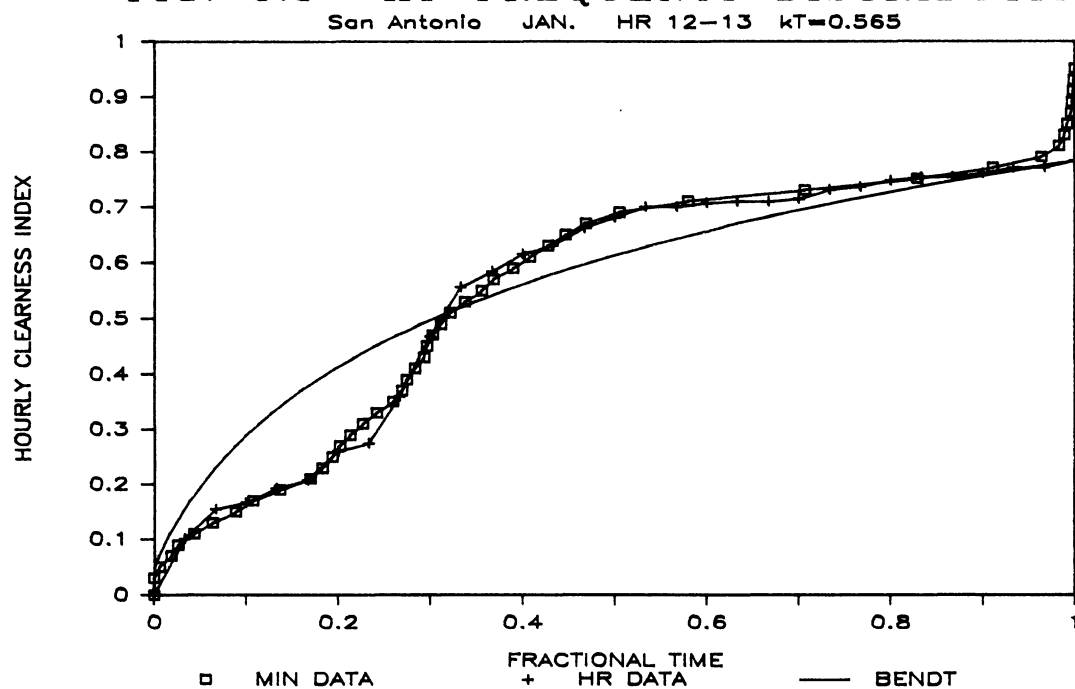


FIG. 3.5 kT FREQUENCY DISTRIBUTION



kt FREQUENCY DISTRIBUTION (kt = 0.433)

San Antonio, TX JUNE Hour 14-15

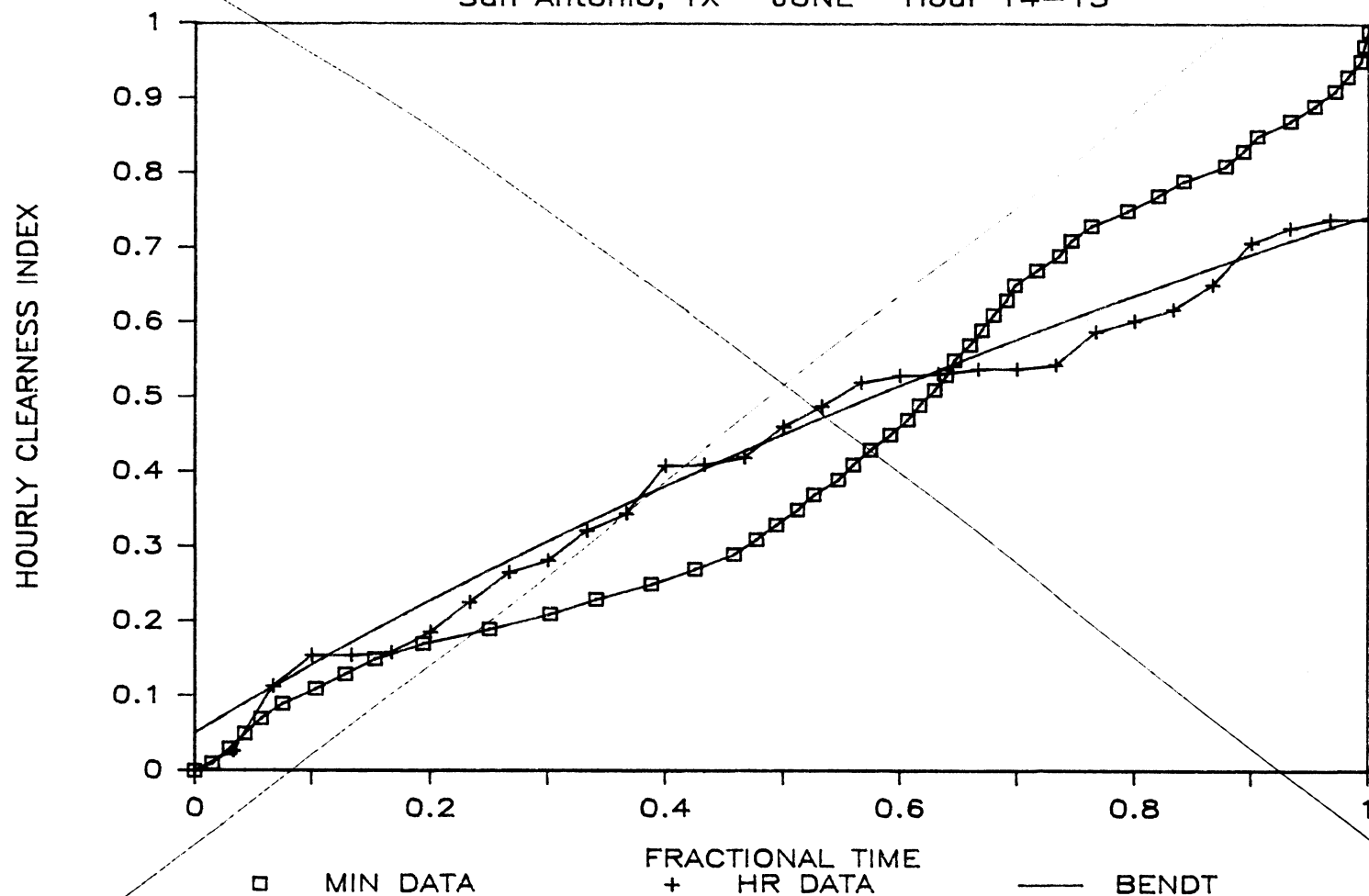


FIG. 3.6 kT FREQUENCY DISTRIBUTION

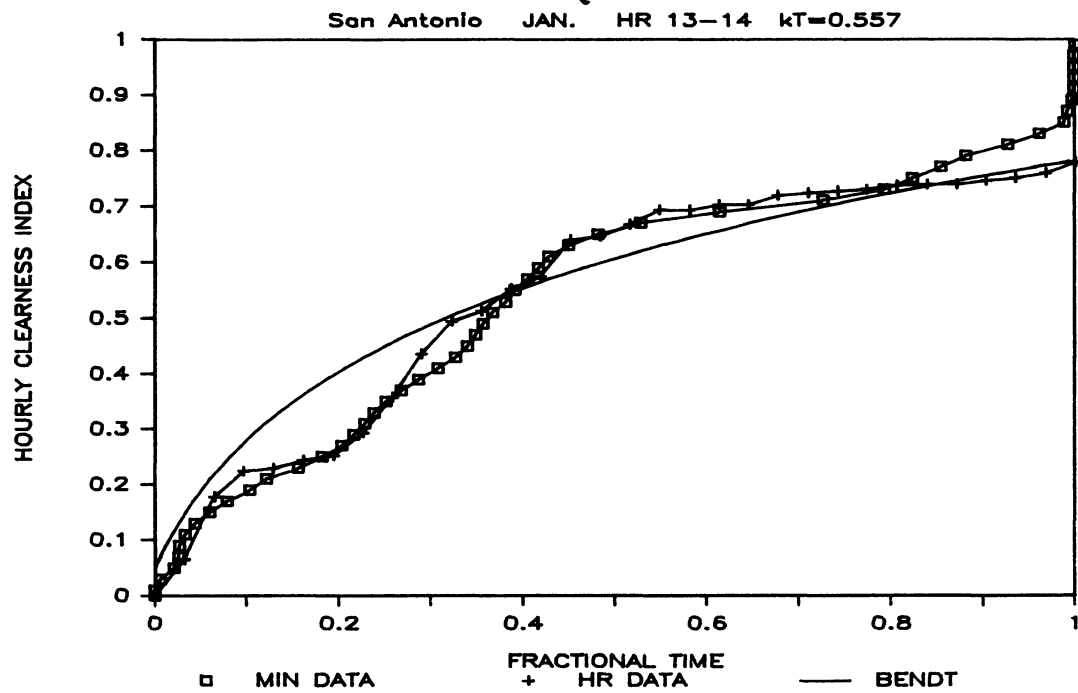


FIG. 3.7 kT FREQUENCY DISTRIBUTION

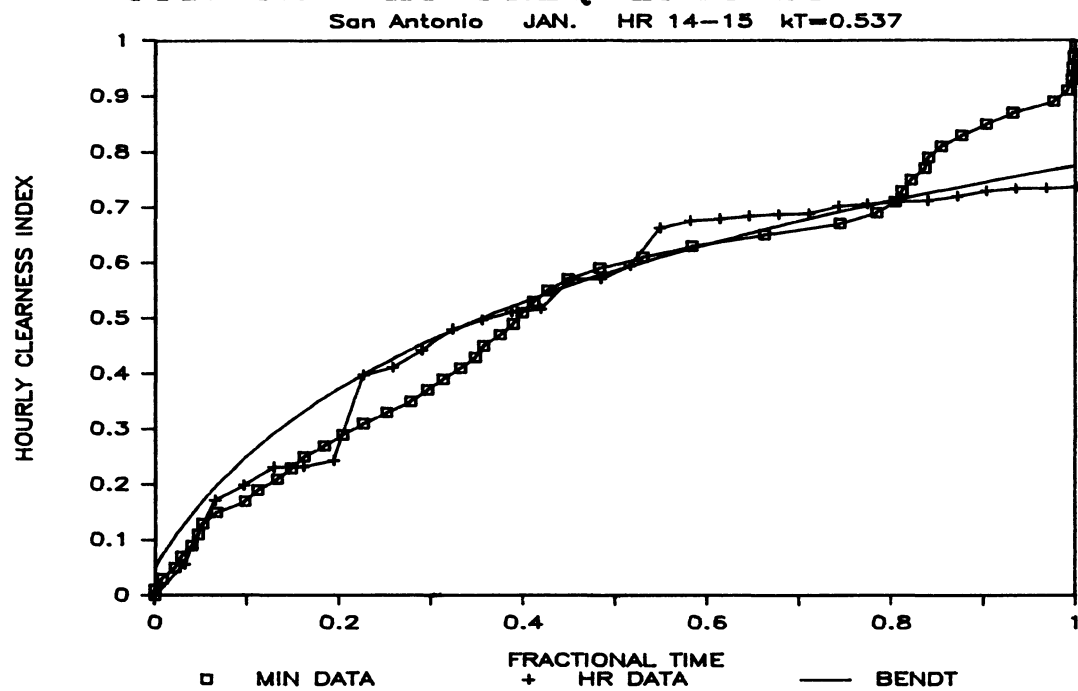


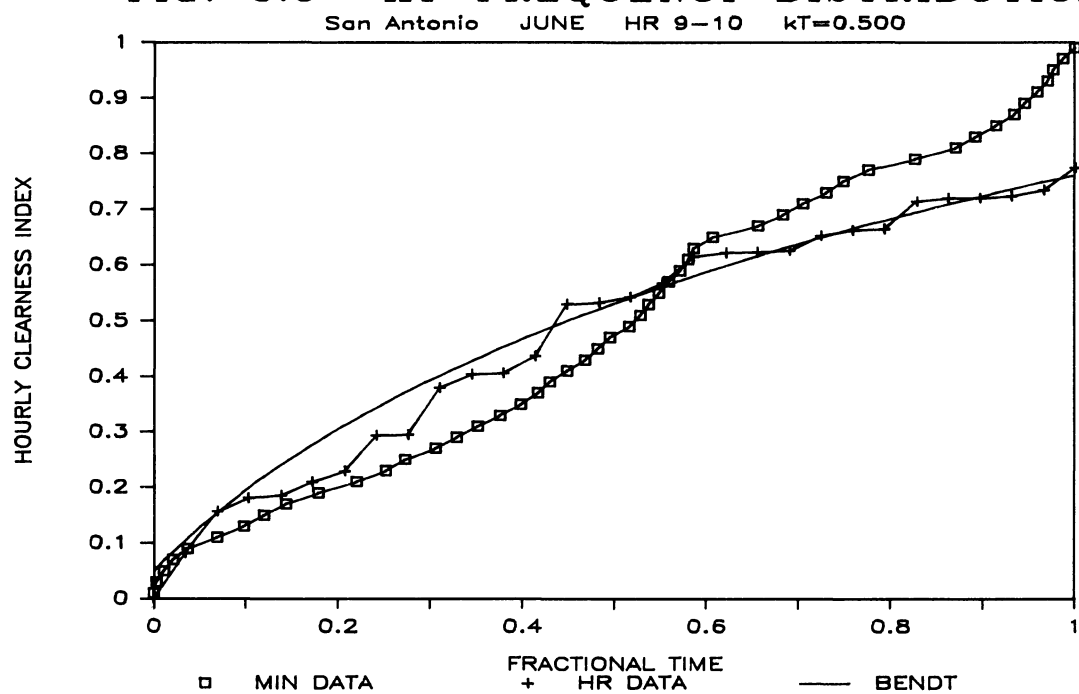
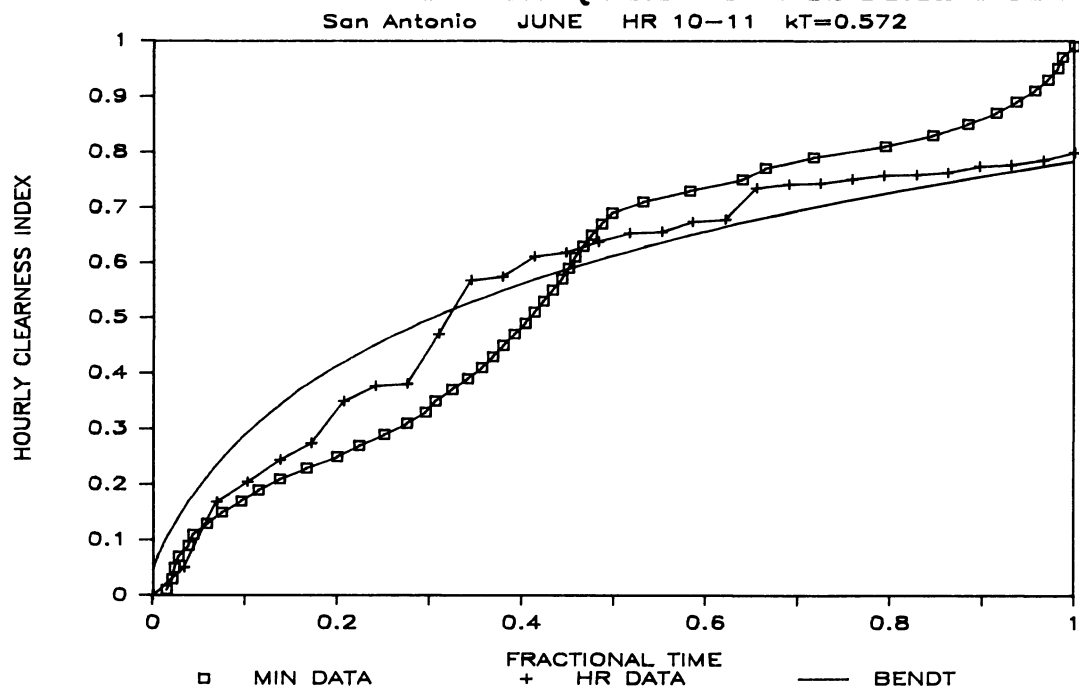
FIG. 3.8 kT FREQUENCY DISTRIBUTIONFIG. 3.9 kT FREQUENCY DISTRIBUTION

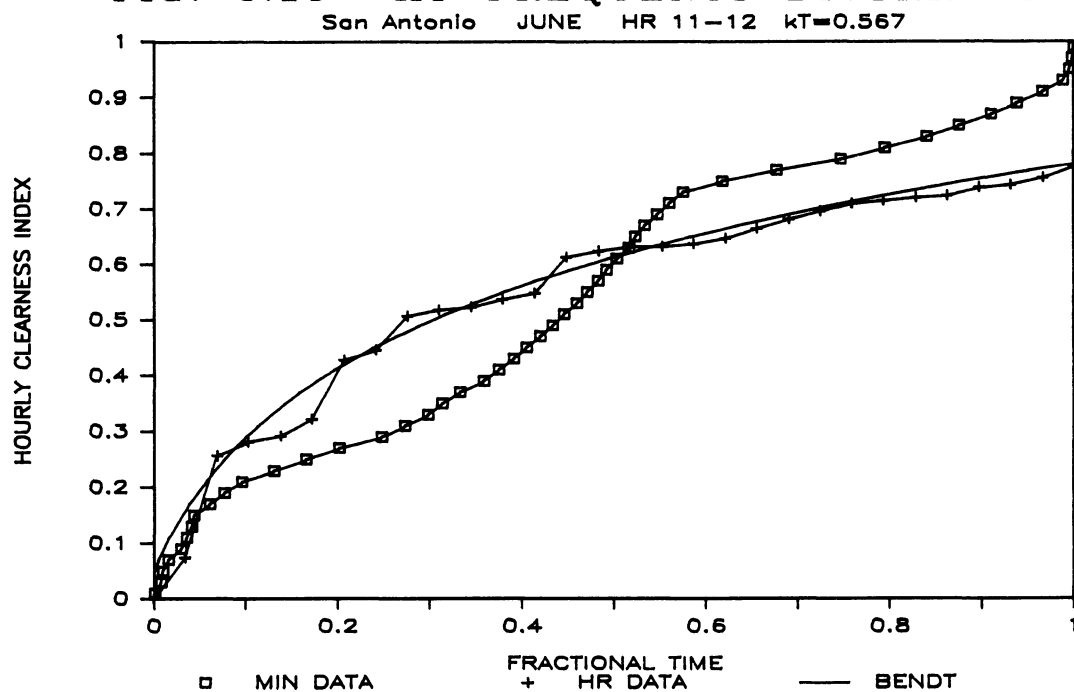
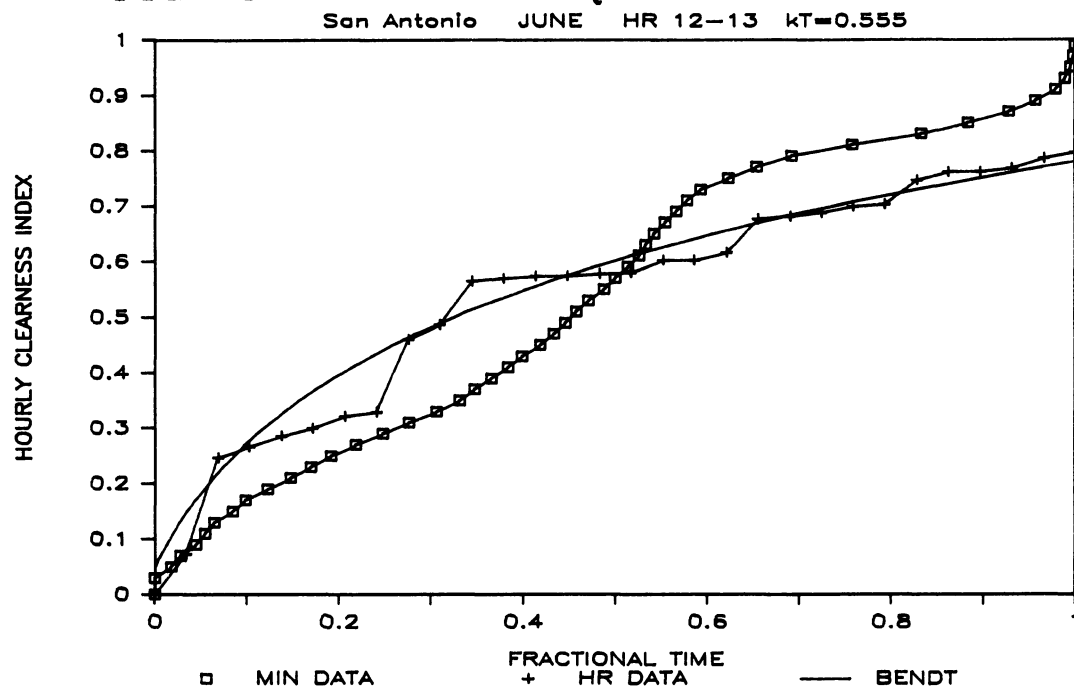
FIG. 3.10 kT FREQUENCY DISTRIBUTIONFIG. 3.11 kT FREQUENCY DISTRIBUTION

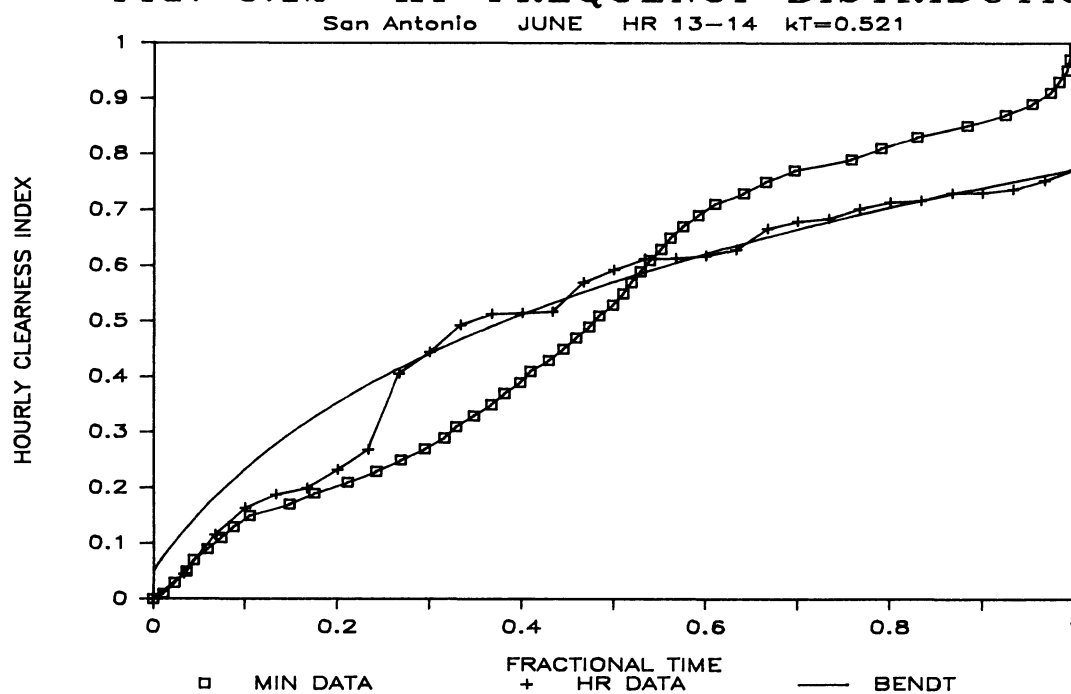
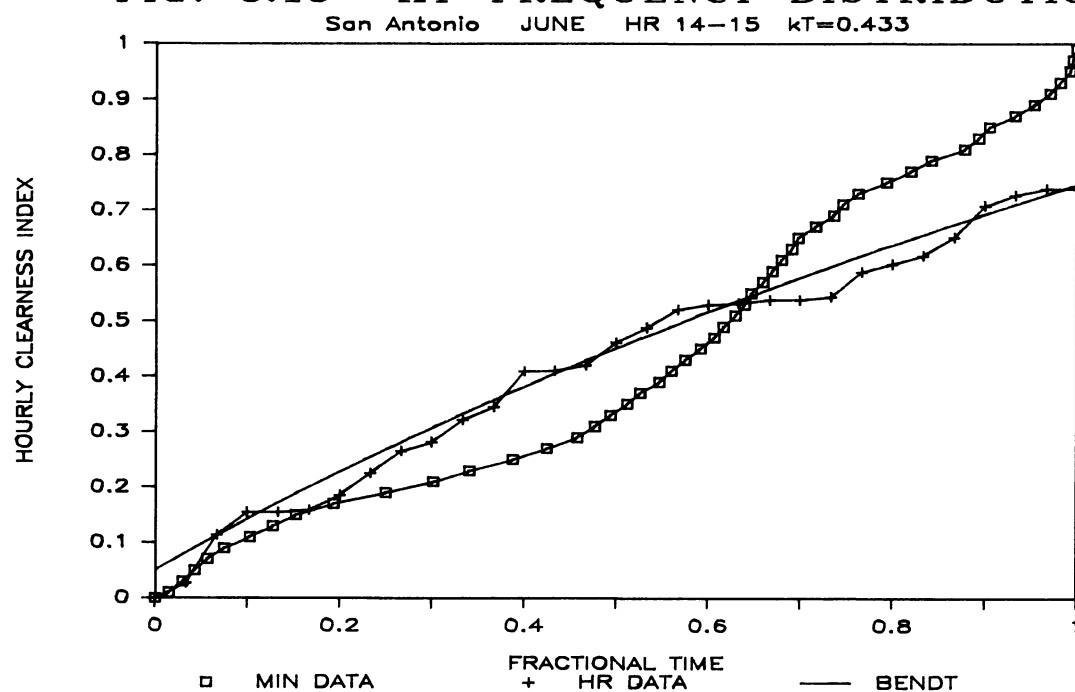
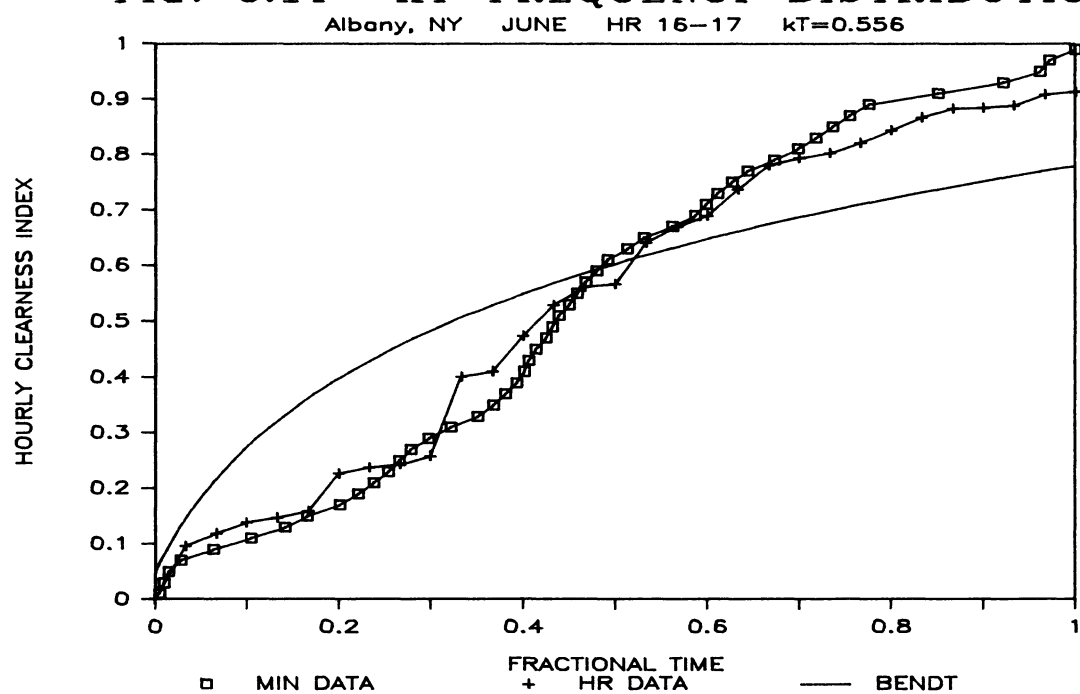
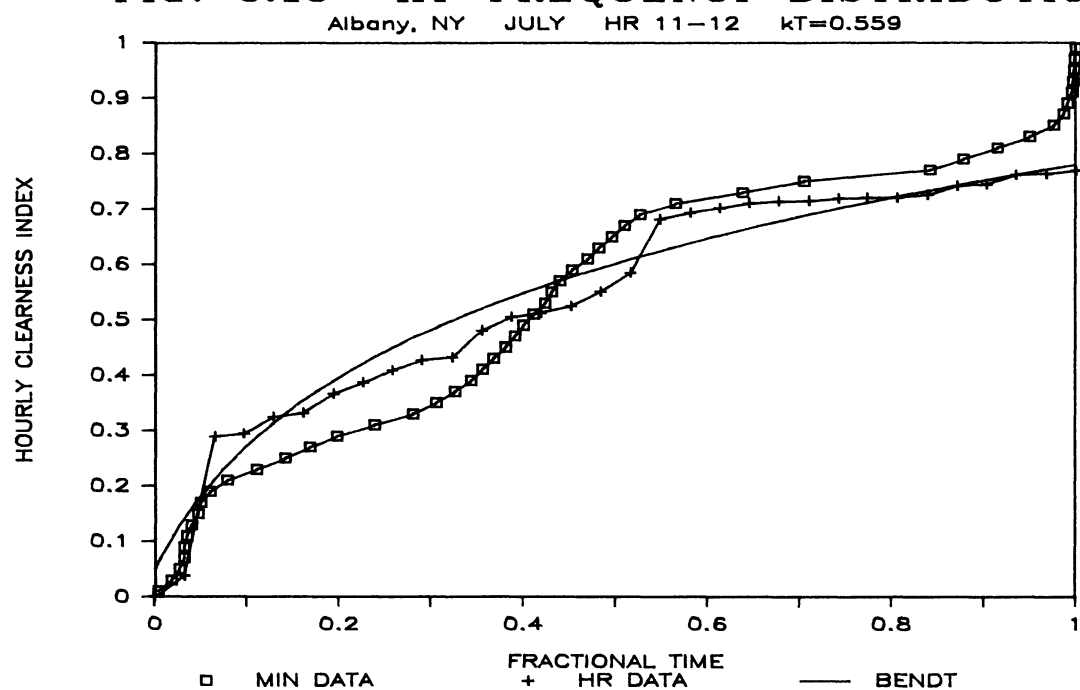
FIG. 3.12 kT FREQUENCY DISTRIBUTIONFIG. 3.13 kT FREQUENCY DISTRIBUTION

FIG. 3.14 kT FREQUENCY DISTRIBUTIONFIG. 3.15 kT FREQUENCY DISTRIBUTION

kt FREQUENCY DISTRIBUTION (kt = 0.572)

San Antonio, TX JUNE Hour 10-11

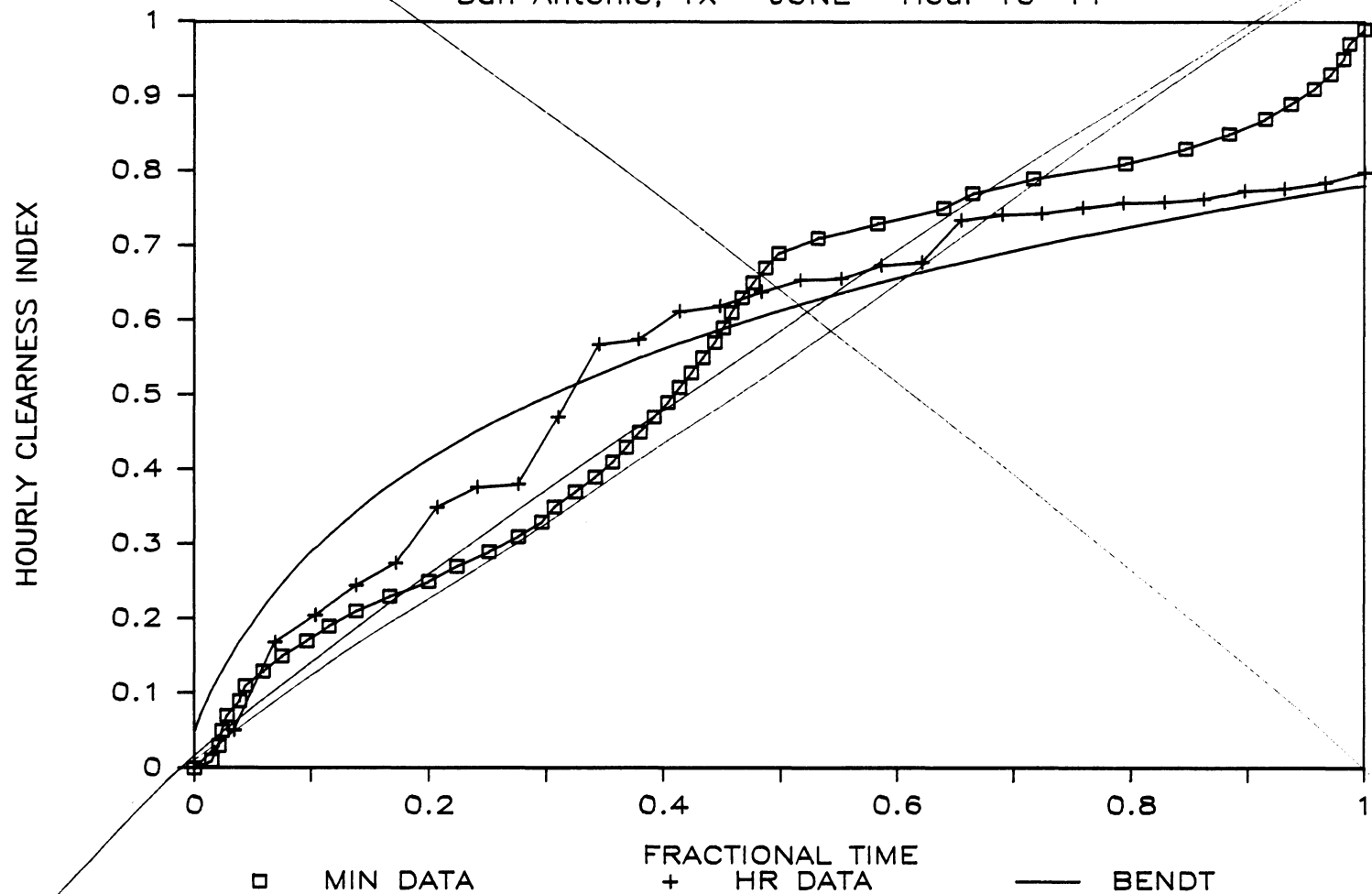


FIG. 3.16 kT FREQUENCY DISTRIBUTION

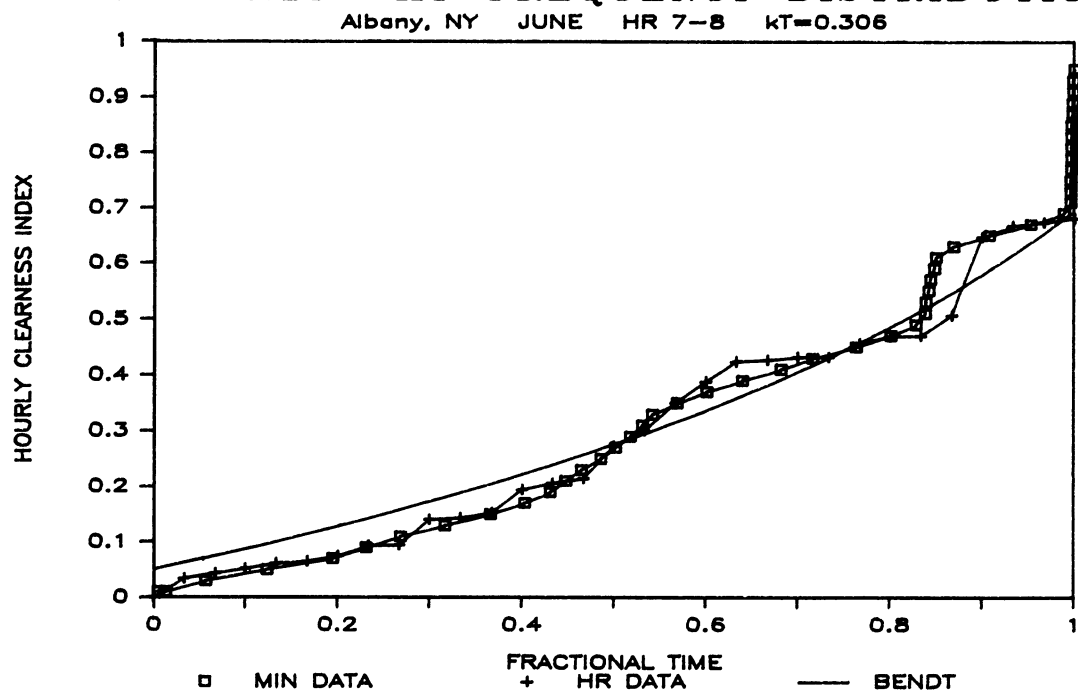
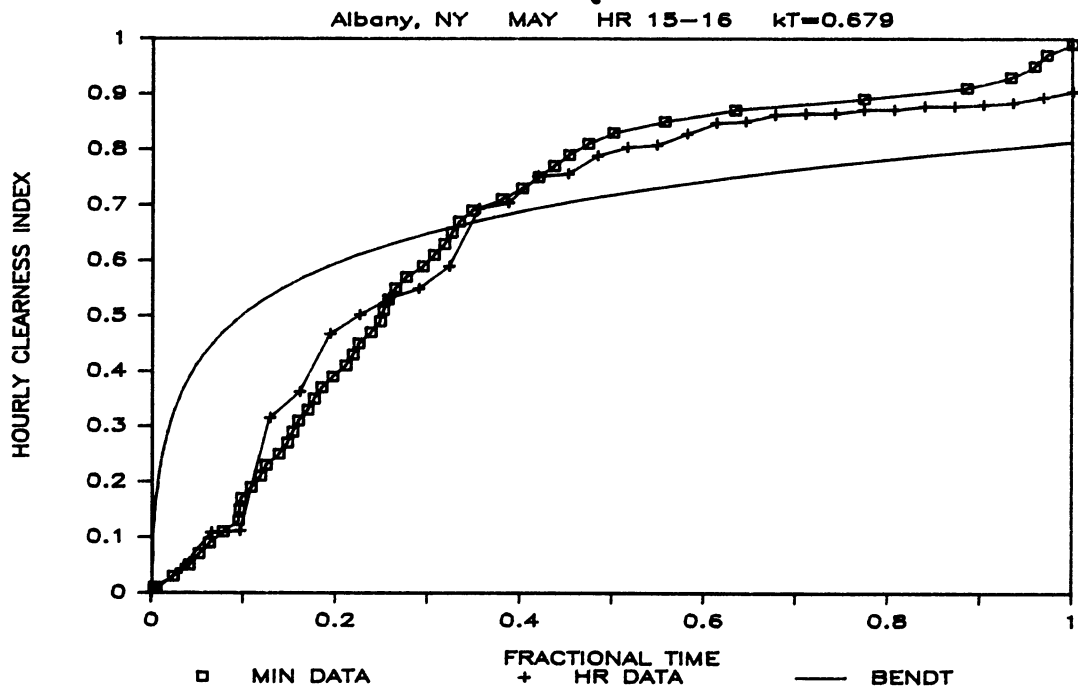


FIG. 3.17 kT FREQUENCY DISTRIBUTION



The minute clearness frequency distributions drawn for hourly periods give some unexpected results. The first surprise is the return of the Liu and Jordan tail. The monthly-average clearness indexes of the graphs shown range between 0.31 and 0.68, with hourly periods between 9 a.m. and 5 p.m. In every case, there is a sudden approach to $k_T = 1.0$. These large k_T values indicate that within any hourly daylight period in a given month, there will always be some minutes where the terrestrial insolation approaches the extraterrestrial insolation.

The other observation is the degree of variability between the hour data and minute data. Figure 3.5 for San Antonio shows the hour data and minute data almost superimposed. Figure 3.11 shows the hour data and minute data with two very different shapes. Both of these graphs have very similar monthly-average hourly clearness indexes: 0.57 and 0.56, respectively.

The other hourly periods in San Antonio for the same months (Figs. 3.2-3.13) show the same trends: for January, the hour data and minute data are almost superimposed; for June, the two distributions are very different. Figures 3.14 and 3.15 for $\bar{k}_T = 0.56$ in Albany, show the same results. The two data distributions in Fig. 3.14 are very similar, while the two data distributions in Fig. 3.15 show a little more difference.

The two extreme \bar{k}_T graphs (Fig. 3.16 - $\bar{k}_T = 0.31$ and Fig. 3.17 - $\bar{k}_T = 0.68$) do show practically superimposed hour data and minute data distributions, as expected. Low \bar{k}_T 's represent months where each day

results in low hourly insolation levels, as in extremely cloudy conditions during the entire month. Under thick cloud conditions, the insolation level within an hour remains fairly constant. Therefore, a minute time-step will not provide new insolation information, and the resulting minute clearness frequency distribution coincides with the hourly clearness frequency distribution. For large $\overline{K_T}$'s, high hourly insolation levels are found for each day in the month - i.e. extremely clear conditions with no clouds, smog, fog, etc. Once again, the insolation level within an hour remains fairly constant, and the resulting hourly clearness frequency distribution coincides with the minute clearness frequency distribution.

The minute data distributions vary from noticeably differing from the hour data distributions, to superimposing with them. Since the hour data were generated by averaging measured minute values, the minute distributions better represent the actual solar insolation. This superposition variability between minute data and hour data has two implications:

- 1) hour time steps are sometimes too large to accurately represent insolation distributions, possibly due to intermittent clouds; and
- 2) Since the difference in distributions occurred for cases with the same monthly-average hourly clearness index, another independent parameter(s) must be involved in fully describing the distributions for hourly periods.

In the past, the monthly-average hourly clearness index has been used as the only independent parameter defining a frequency distribution. If the second implication is correct, then the clearness frequency distribution may not actually follow a known distribution defined only by \bar{k}_T , but possibly a distribution defined by \bar{k}_T in conjunction with some other factor(s). This other independent parameter(s) is presently unknown, but may be one of the parameters found by Garrison [7] in his study of diffuse fractions: solar elevation; surface albedo; atmospheric precipitable water; and atmospheric turbidity (See Chapter 2).

The other independent parameter(s) could help explain a previous finding by Theilacker [34]. As part of a larger study on clearness indexes, Theilacker found the hourly clearness frequency distributions for Miami, Florida to have shapes "flatter" than the Liu and Jordan distributions. He attributed this to haze caused by the ocean environment, which would agree with Garrison's atmospheric precipitable water parameter. Theilacker concluded that climatic and locational parameters should be included in truly generalized distributions, but the improved accuracy through added correlation complexity would be undesirable. From an engineering point of view, the added correlation complexity may still be undesirable.

In an attempt to better understand the minute data distributions for monthly-average hourly clearness indexes, Figs. 3.18 and 3.19 were made to compare only the minute data distributions for the same \bar{k}_T . Figure 3.18 is for $\bar{k}_T = 0.56$, and Fig. 3.19 shows $\bar{k}_T = 0.57$.

$\bar{k}_T = 0.56$ FREQUENCY DISTRIBUTIONS

Minute Data from Previous Figures

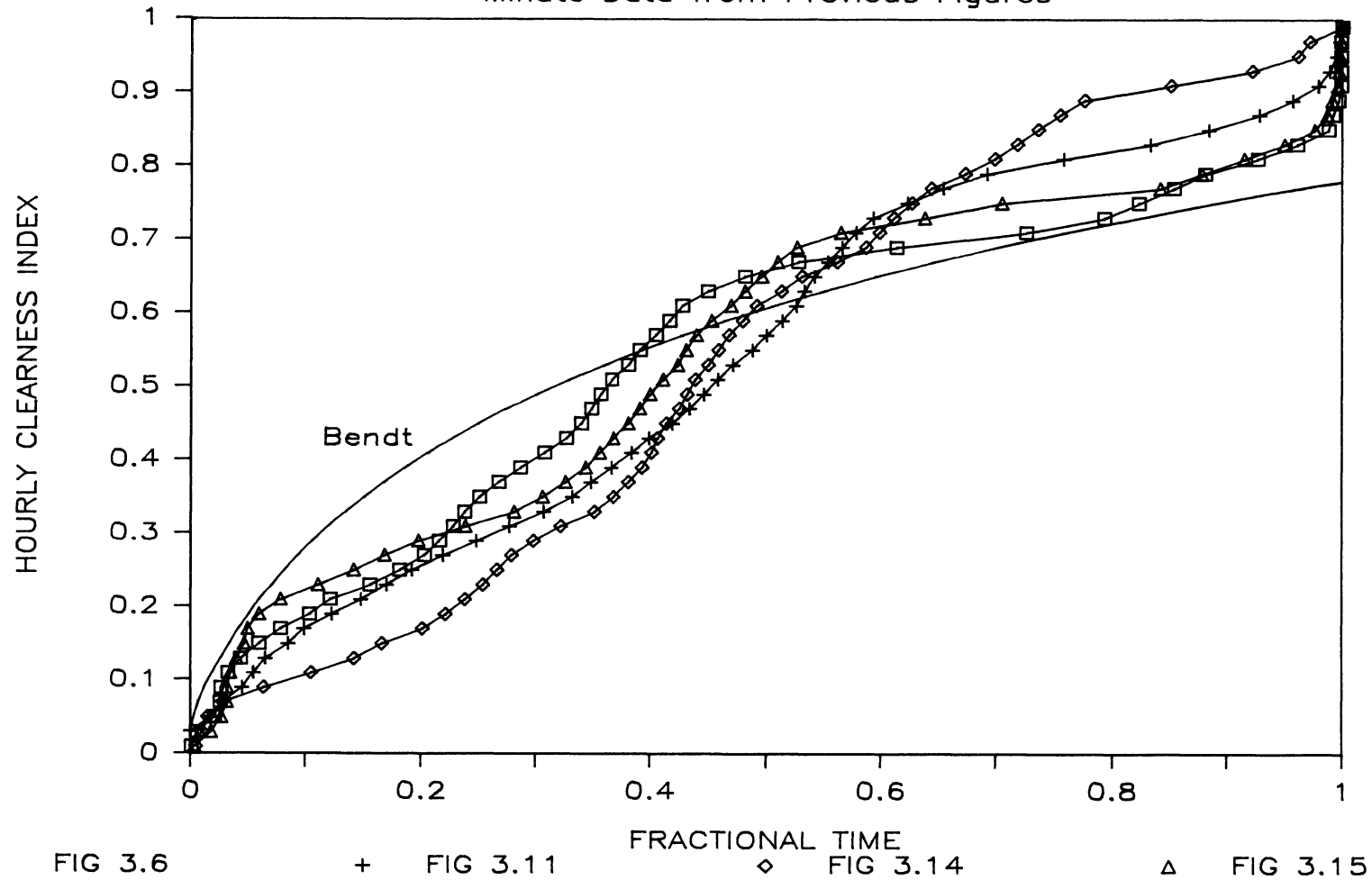


Figure 3.18: $\bar{k}_T = 0.56$ Frequency Distributions.

$k_T = 0.57$ FREQUENCY DISTRIBUTIONS

Minute Data from Previous Figures

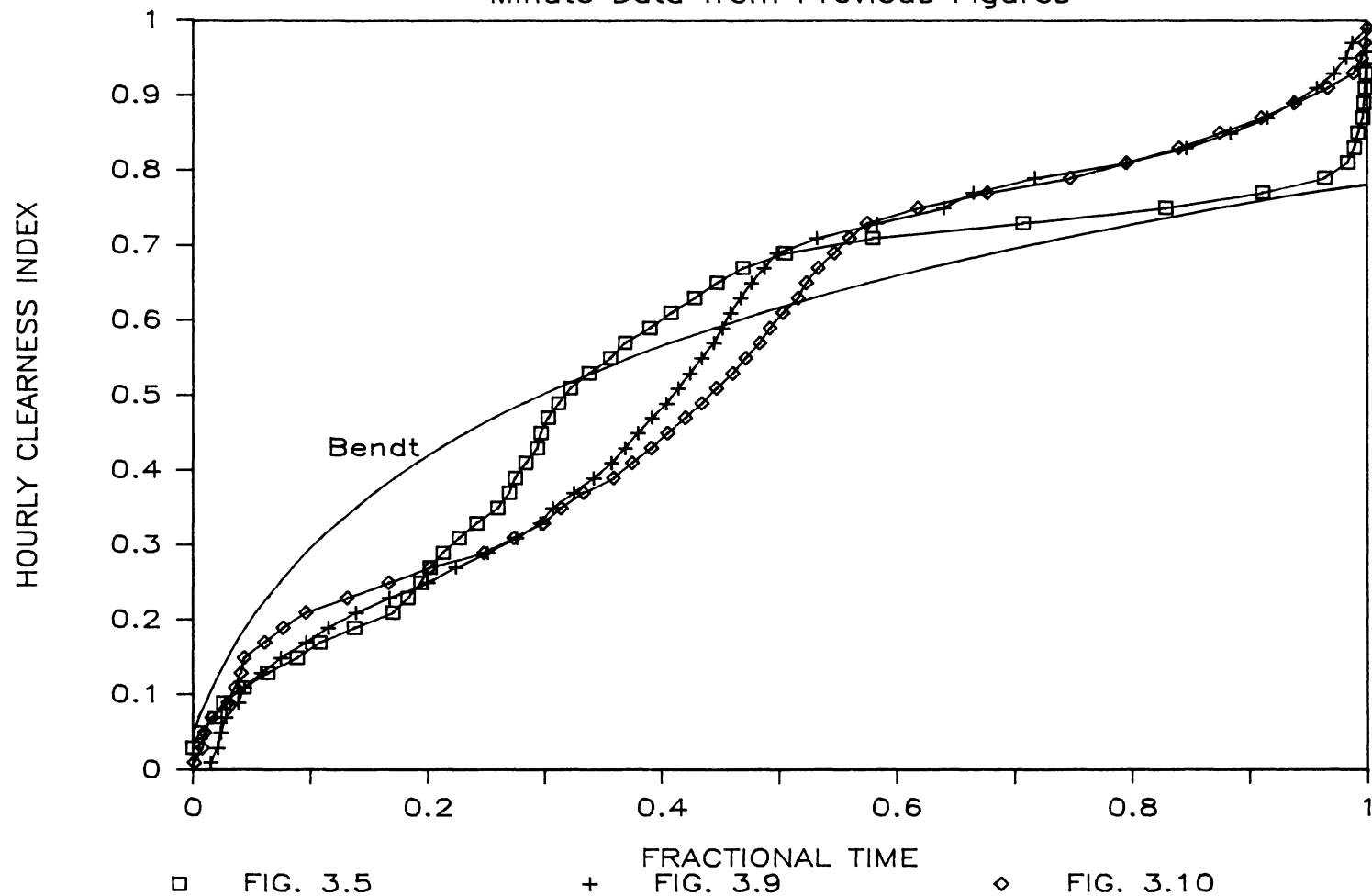


Figure 3.19: $\bar{k}_T = 0.57$ Frequency Distributions.

Both graphs show some variability in the curve shapes. Although the data base is small, other independent parameters appear to be required to adequately define minute clearness frequency distributions for hourly periods within a month.

3.5 Frequency Distributions for Daily Periods

Figures 3.20 through 3.23 show some of the daily frequency distributions for a given monthly-average daily clearness index. The graphs are for San Antonio in January, San Antonio in June, Albany in June, and Albany in July. All four distributions have \overline{K}_T 's approximately equal to 0.5. Plotted with each graph is the generalized Bendt distribution for the same \overline{K}_T .

In all cases shown here, the data distributions follow the Bendt distribution fairly well. There are no large differences in shape, as there were in the minute data distributions. This implies the insolation levels during the months presented are somewhat close to "typical" distributions.

The other observation is the lack of the Liu and Jordan tail. This is in agreement with the Bendt distribution and Theilacker's observations. It also suggests that individual daily insolation levels do not approach extraterrestrial values. For the cases here, the maximum daily insolation levels are within 75% of the extraterrestrial values.

3.6 Conclusions

The clearness frequency distributions analyzed represent a small data base, and therefore no general conclusions can be made. How-

FIG. 3.20 KT FREQUENCY DISTRIBUTION

San Antonio, TX JAN. KT=0.50

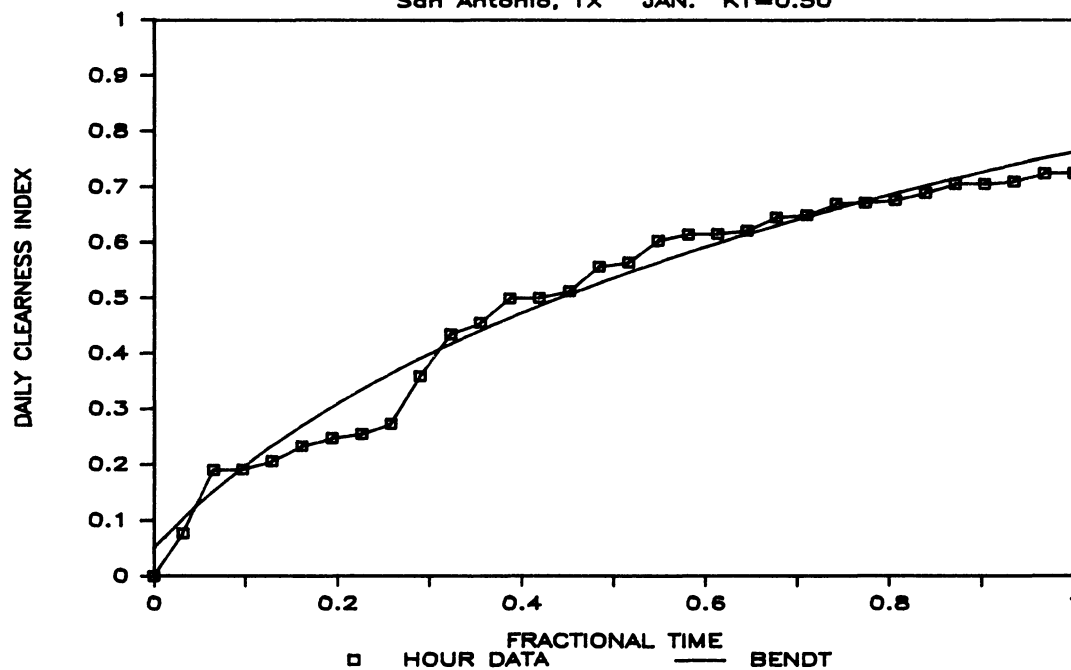


FIG. 3.21 KT FREQUENCY DISTRIBUTION

San Antonio, TX JUNE KT=0.50

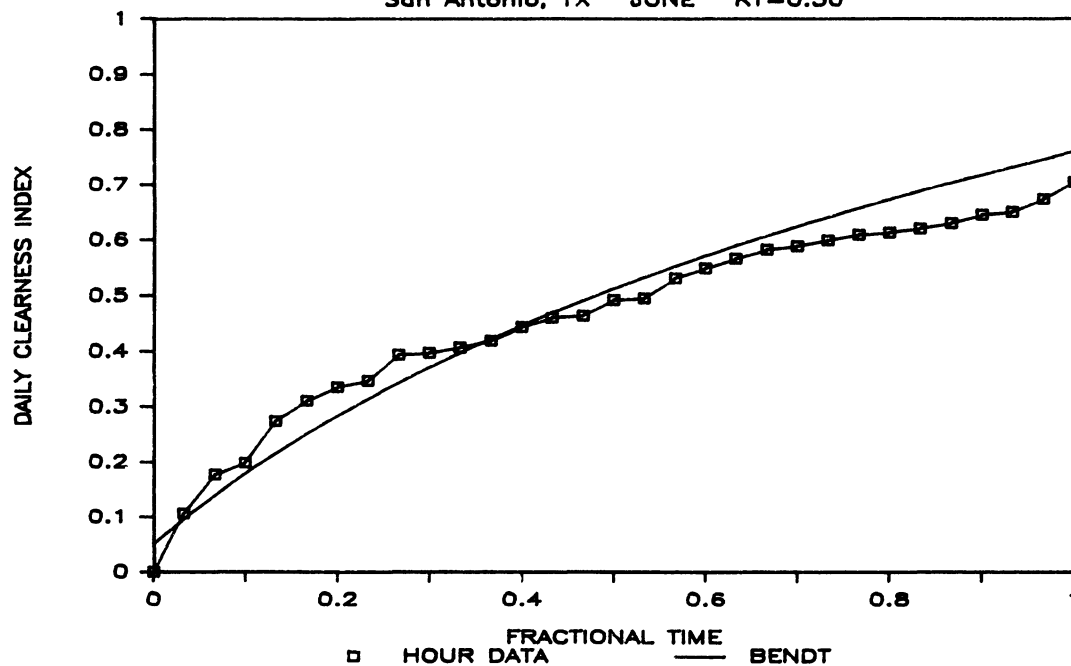


FIG. 3.22 KT FREQUENCY DISTRIBUTION

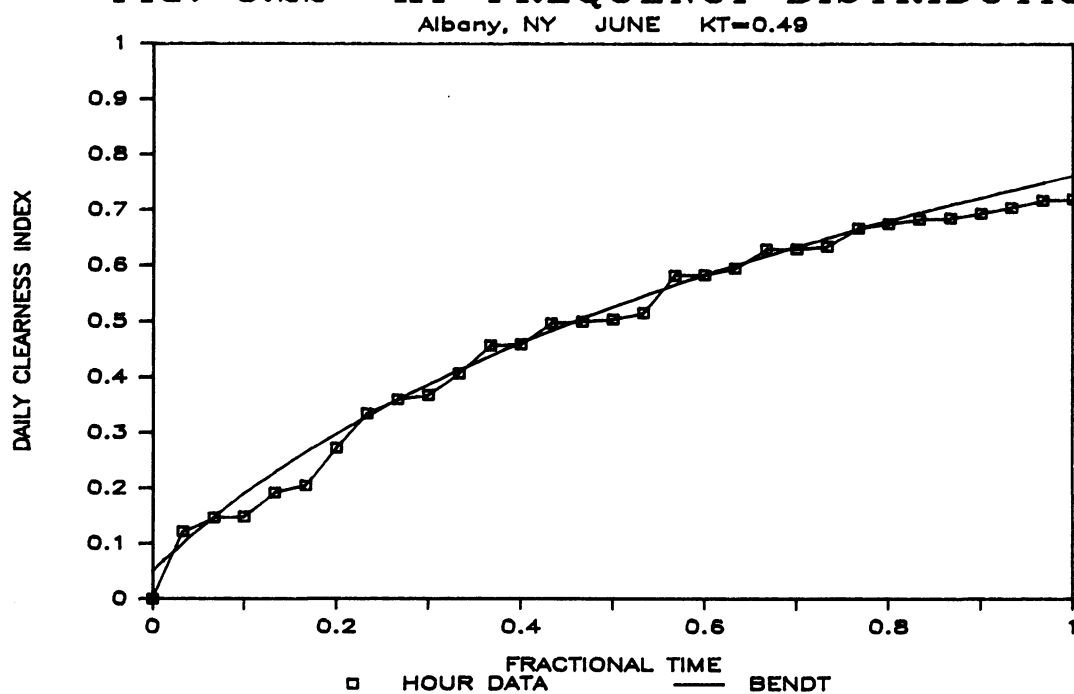
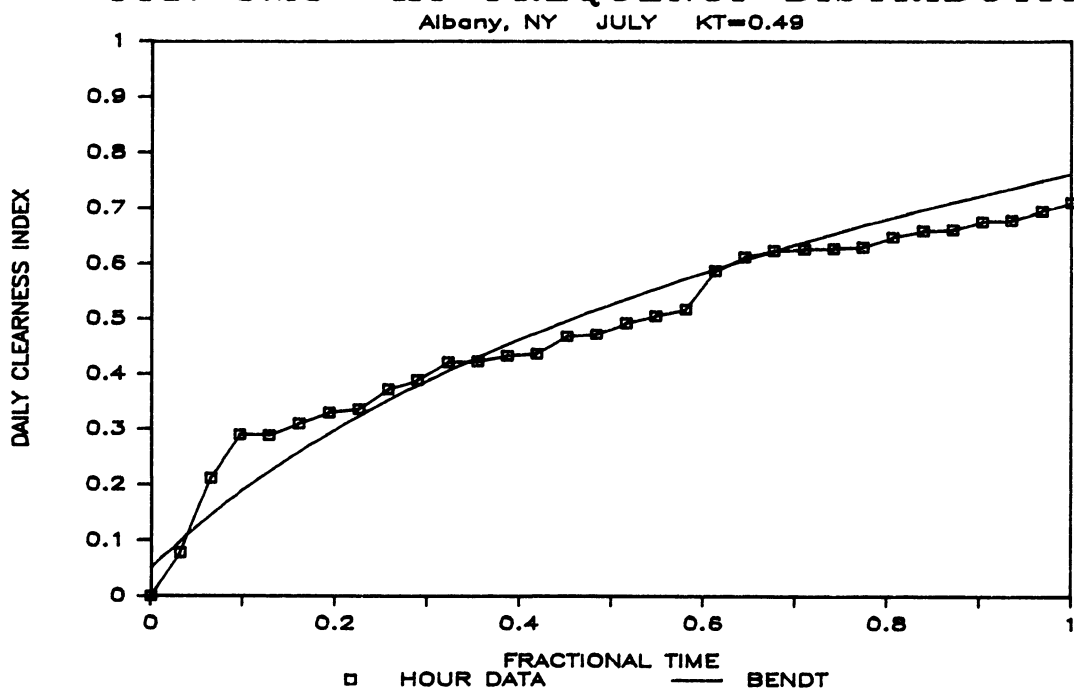


FIG. 3.23 KT FREQUENCY DISTRIBUTION



ever, the following implications were found:

1. Hourly data is occasionally too large of a time step to accurately represent actual insolation levels. Improvement can sometimes be made using minute data. The effect of using minute versus hour data for utilizable energy calculations is discussed in Chapter 4.
2. Minute clearness frequency distributions for hourly periods within a month show more variability in insolation levels than the generalized daily distributions presently used to describe hourly insolation levels. These generalized curves may need to be updated to accurately represent distributions for hourly periods.
3. Minute data distributions for hourly periods rapidly approach $k_T = 1.0$ at large fractional times. Therefore, individual minute insolation levels can approach extraterrestrial values.
4. The strong possibility of more than one independent parameter defining the clearness frequency distributions for hourly periods was shown. At present, this other parameter(s) is unknown, but may be one or more of the following: solar elevation; surface albedo; atmospheric precipitable water, or atmospheric turbidity.
5. The daily clearness frequency distributions calculated from hour data do approximately follow the Bendt et. al [1] clearness frequency distributions. The rapid approach to $K_T = 1.0$ at large fractional times as shown by Liu and Jordan [21] was not observed. Therefore, the maximum daily insolation will always be well below the extraterrestrial levels. For the cases shown

here, the maximum daily insolation values are below 75% of the extraterrestrial values.

4. UTILIZABILITY

4.1 Background on Utilizability

Utilizability is the ratio of energy above a given threshold or critical level, to the total incident energy. This critical level can be the energy required to maintain a collector plate at the fluid inlet temperature. Consequently, the incident solar energy above this level is the "useful" or "utilizable" energy for the desired goal. Since utilizability is a fraction of useful to total energy, it ranges between 0 and 1. Large utilizability values indicate a large percentage of the energy is available for the desired goal, while small utilizability values indicate a small percentage is available.

Utilizability values are usually given for long-term monthly average periods. Figure 4.1 shows the solar irradiation for a hypothetical three day month. The abscissa is time, while the ordinate is the irradiation on the surface. Each day represents one of three different kinds of days: hazy, clear, and cloudy. The horizontal line drawn through the curves indicates an arbitrary critical level, I_c . The cross-hatched areas represent the total energy above this critical level which can be used to heat a home, heat water, charge a battery, etc. On the cloudy day, the insolation is too low to contribute any useful energy for the desired goal. The clear day receives the most irradiation, and therefore has the largest area above the critical level.

UTILIZABILITY EXAMPLE

Hypothetical 3 Day Month

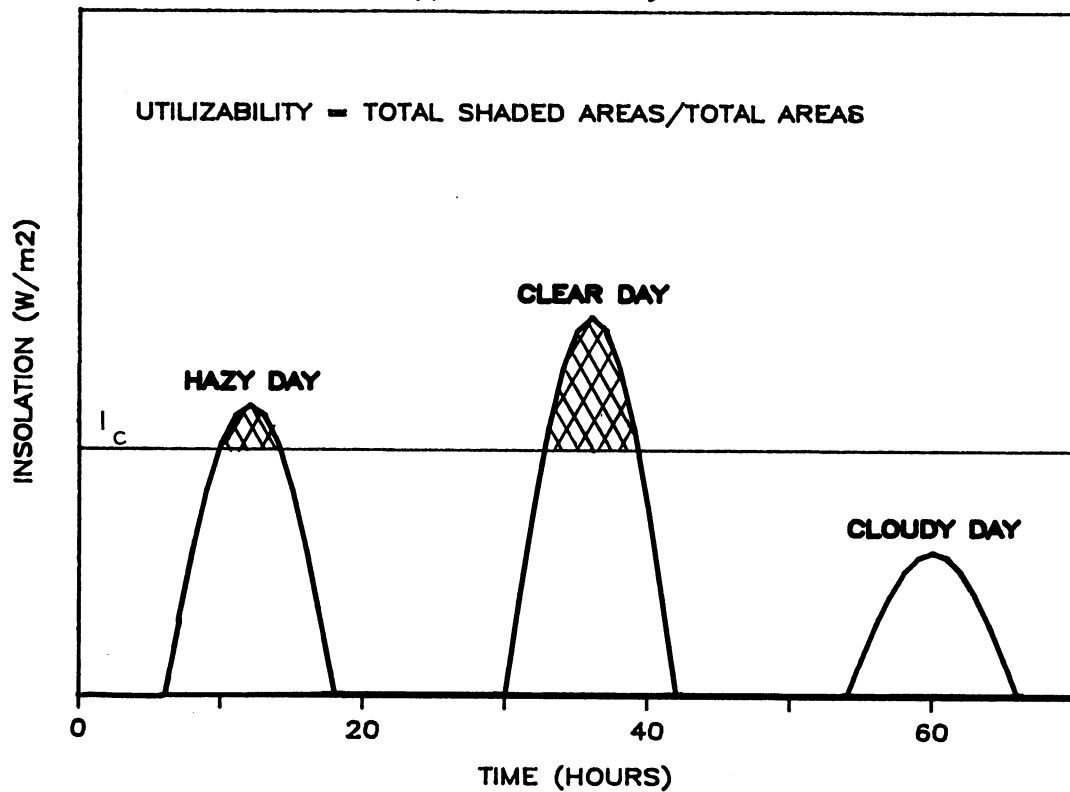


Figure 4.1: Utilizability Example for Hypothetical Month.

The distribution of hazy, clear, and cloudy days varies for every month. Months with all clear days will have high utilizability values for a given critical level, while months with all cloudy days will have low utilizability values. Months with a combination of hazy, clear, and cloudy days will have a higher utilizability than months with the same total irradiation, but with all hazy days. Figure 4.2 shows the same hypothetical 3 day month, in comparison to a month with all hazy days. The total areas under both sets of curves are equal. However, the month with the variable weather results in more energy above the critical level than the constant weather month.

Since utilizability depends on this distribution of hazy, clear, and cloudy days, it is considered as a solar radiation statistic. Using this statistic, the useful energy above a known critical level can be calculated, given the expected total irradiation for the month. This useful energy can then be used for design calculations.

The utilizability concept was first proposed by Whillier [35], as an approach to predict the long-term performance of flat-plate solar collectors. Since then, the utilizability concept has been expanded for many uses, as summarized by Klein and Beckman [17]. In general, utilizability is applicable for analysis of solar processes with constant critical levels or as theoretical limits for processes with variable critical levels.

Many correlations have also been developed to calculate the utilizability for a given critical level and surface orientation, usual-

UTILIZABILITY EXAMPLE

Hypothetical 3 Day Months

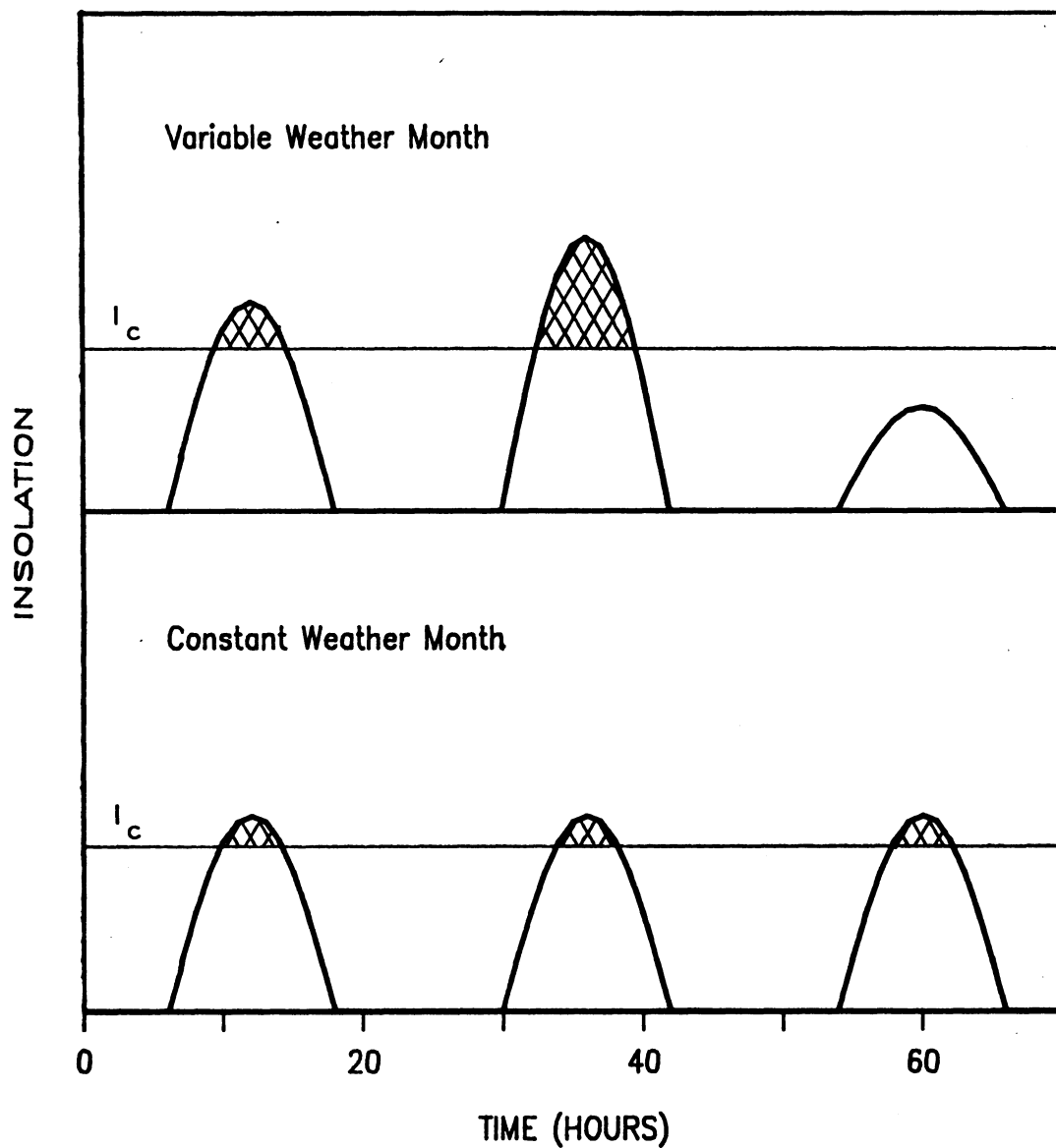


Figure 4.2: Utilizability Comparison Example for Two Hypothetical Months.

ly south-facing surfaces [17]. Because utilizability is a solar radiation statistic, correlations produce long-term monthly-average daily $\bar{\phi}$ values or long-term monthly-average hourly ϕ values.

4.2 Utilizability Calculation Methods

Utilizability correlations are useful engineering design tools for statistically calculating long-term energy above critical levels. The accuracy of these correlations are important, as both underestimating and overestimating usable energy is undesirable.

By nature of the utilizability concept, periods with large variation in insolation levels produce larger utilizability values than constant insolation values, as shown by Fig. 4.2. Therefore, the time-step that insolation is measured over also becomes important. Large time-steps average insolation levels over the given period, decreasing the effect of the larger values. Large time-steps therefore decrease the apparent utilizable energy that is above a given critical level.

Figure 4.3 shows the importance of the time-step in calculating the utilizable energy. Instrument A represents insolation measured in steps equal to 1 time unit. During the first unit of time, the insolation was above the shown critical level, indicating utilizable energy. Instrument B received the same total insolation, but measured this radiation with a time-step equal to 3 units. As is typical for radiation measuring devices, the insolation was averaged over the time-step. Even though both instruments are measuring the same insolation, instrument A recorded utilizable energy, while

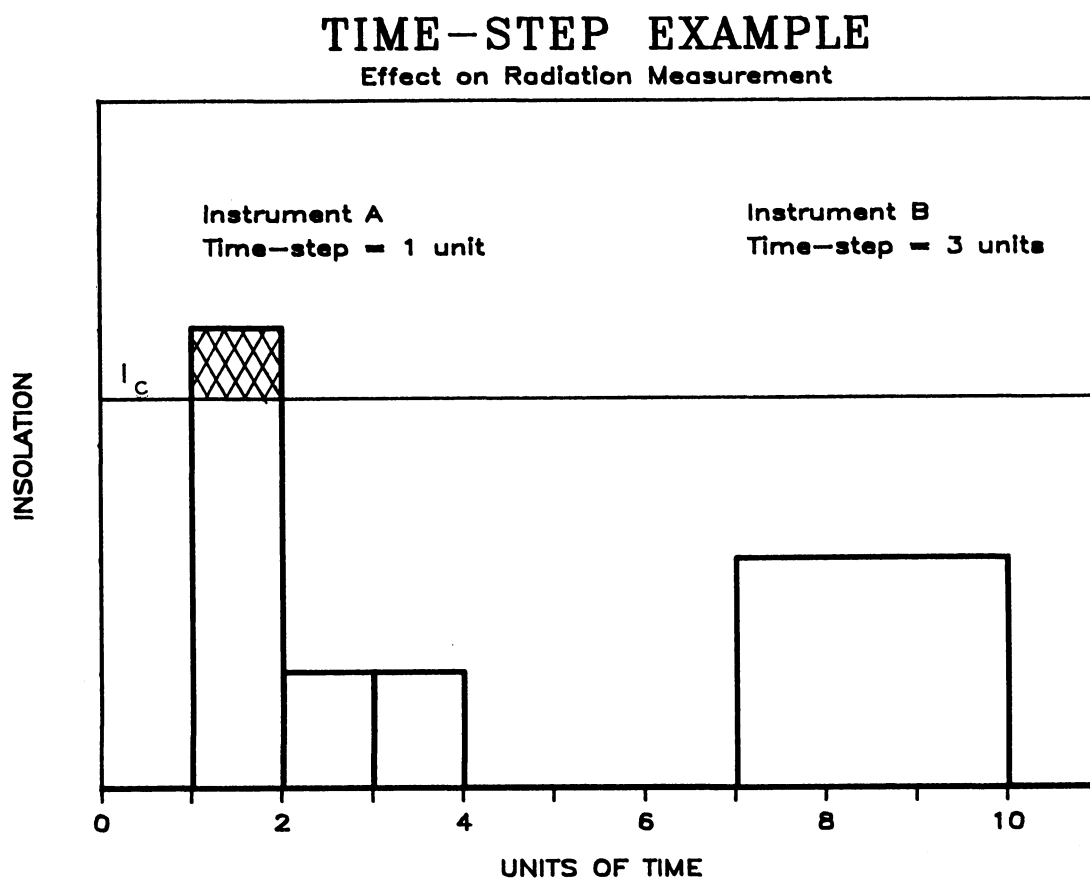


Figure 4.3: Generic Comparison of Time-Steps in Representing Radiation Data.

instrument B "washed out" the period of high insolation and therefore shows no utilizable energy.

Existing correlations were developed from hour data, but as shown above and in Chapter 3, hour data is not always an accurate representation of actual insolation levels. The SEMRTS data provides valuable information about insolation on a minute-by-minute basis. The SEMRTS data also provides insolation information for surfaces at several orientations. Therefore a comparison was made of monthly-average hourly and monthly-average daily utilizability values calculated from hour data, minute data, and Clark's [2] monthly-average hourly correlation.

4.2.1 Utilizability From Data

For a given surface, utilizability is the summation of all insolation above a critical level divided by the summation of the total insolation. For monthly-average hourly utilizability, this can be written as:

$$\phi = \frac{\sum_{N} (I_T - I_C)^+}{\sum_{N} I_T} \quad (4.1)$$

where $(I_T - I_C)^+$ implies positive values only, and N = days in month [17]. Similarly, monthly-average daily utilizability can be written as:

$$\bar{\phi} = \frac{\sum_{N} \sum_{hrs} (I_T - I_C)^+}{\sum_{N} \sum_{hrs} I_T} \quad (4.2)$$

Both functions are easily programmed to process real data. For this study, both the minute data and the hour data were used to calculate utilizability. For the minute data, an extra summation was required to account for the 60 minutes that constitute an hour.

4.2.2 Clark's Correlation

Many algorithms exist for calculating the utilizability on south-facing surfaces. Some methods analytically integrate energy levels represented by long-term clearness frequency distributions, and then calculate monthly utilizability for a given critical level [17]. Clark [2] took a different approach by directly correlating calculated values of hourly utilizability obtained from many years of hourly horizontal insolation data. The resulting correlation was for monthly-average hourly utilizability for all surface orientations.

Clark's data base consisted of 23 years from Madison, Wisconsin; 23 years from Albuquerque, New Mexico; and 15 years from Seattle, Washington. In a comparison to numerically integrated data values, Clark's method had a root mean square error of 5% [17]. Consequently, due to its accuracy, surface versatility, and algebraic simplicity, it was chosen as the existing algorithm to compare with data values.

Clark defined his correlation in terms of the critical insolation ratio X_c , and the "minimum" critical insolation ratio X_m . The critical insolation ratio is a common dimensionless expression for the critical level divided by the monthly-average radiation on the surface, or

$$X_c = \frac{I_c}{I_T} \quad (4.3)$$

X_m is therefore the minimum critical insolation level where the utilizability equals 0. Using these ratios, the hourly utilizability correlation was expressed as:

$$\phi = \begin{cases} 0, & X_c > X_m \\ (1 - (X_c/X_m))^2, & X_m = 2 \\ |a| - \sqrt{a^2 + (1 + 2a)((X_m - X_c)/X_m)^2}, & \text{otherwise} \end{cases} \quad (4.4)$$

where

$$a = \frac{X_m - 1}{2 - X_m}$$

After attempts to derive equations for X_m from general equations, Clark empirically found the minimum critical level to best be represented by:

$$X_m = 1.85 + 0.169 \frac{\tilde{R}}{\bar{k}_T^2} - 0.0696 \frac{\cos \beta}{\bar{k}_T^2} - 0.981 \frac{\bar{k}_T}{(\cos \delta)^2} \quad (4.5)$$

For a given location, orientation, and critical level, the required input parameters for Clark's correlation are the monthly-average hourly clearness index, \bar{k}_T and monthly-average hourly radiation ratios, \tilde{R} . As shown in Chapter 2, \tilde{R} can be correlated to the monthly-average hourly clearness index, making \bar{k}_T the only independent parameter. Since utilizability is usually desired for more than

one hour, algorithms use the monthly-average daily clearness index, \bar{K}_T along with the r_d/r_t relation presented in Chapter 2, to estimate \bar{k}_T . The \bar{K}_T , \bar{k}_T relation is as follows:

$$\bar{k}_T = \frac{r_t}{r_d} \bar{K}_T \quad (4.6)$$

where r_t/r_d equals the reciprocal of Eq. (2.13).

Insolation levels and the resulting utilizability vary from year to year. Clark's correlation was developed from 61 years of data, and therefore represents long-term or average utilizability levels. Long-term \bar{K}_T 's are used in design applications to estimate average utilizability for a given location. However, the Albany and San Antonio data sets represent only one year periods. To allow comparison between data and Clark utilizability values under "identical" short-term conditions, clearness indexes calculated from the data base were used.

To investigate the different sources of error in Clark's correlation, three different approaches were devised. The \bar{k}_T algorithm using r_t/r_d assumes symmetrical insolation levels about noon. Due to actual asymmetries found in the data, the first approach used \bar{K}_T 's calculated from the data. The monthly-average hourly radiation ratios were calculated from the isotropic model (Eq. 2.8), with Erbs' \bar{H}_d/\bar{H} correlation (Eq. 2.14) and the r_d/r_t relation as shown in Chapter 2.

Method two used the actual monthly-average daily clearness indexes, along with the r_t/r_d relation to calculate the \bar{k}_T 's. This approximates typical usage of Clark's correlation with the symmetrical insolation level assumption, but still under "identical" monthly-average daily conditions. The isotropic model was still used to calculate \tilde{R} .

Method three used the actual monthly-average hourly clearness index again, along with actual monthly-average hourly radiation ratios. This eliminates any error from radiation ratio assumptions and modeling, and therefore is considered the most accurate version of Clark's correlation used in this study.

4.2.3 Critical Level Calculation

Due to varying amounts of radiation a surface receives during a year, appropriate critical levels for each surface were calculated for each month. Calculating new monthly critical levels allows the same number of utilizability values under all conditions, which is required for RMS error comparisons (see Section 4.2.4).

Eleven critical levels were calculated for each surface, based on a percentage of the maximum noon-time irradiation. An approximation of the noon-time radiation was derived by multiplying the horizontal extraterrestrial irradiation I_0 (see Eq. 2.13) by the noon-time value of R_b ,

$$I_{\text{noon}} = I_0 R_b|_{\text{noon}} = I_0 \frac{\cos(\theta)}{\cos(\theta_z)} \Big|_{\text{noon}} \quad (4.7)$$

For noon, $w_1 = -7.5^\circ$ and $w_2 = 7.5^\circ$. Since these are small angles, $\sin(w_2) - \sin(w_1)$ approximately equals $w_2 - w_1$, which equals 0.262 radians. Also, the earth-sun distance correction term can be approximated by 1.03. Consequently, the horizontal extraterrestrial equation can be rewritten as:

$$I_o = 13,750 G_{sc}(1.03)(0.262)[\cos(\phi) \cos(\delta) + \sin(\phi) \sin(\delta)] \quad (4.8)$$

where for this application, ϕ equals the latitude. Now, $\cos(\theta_z)_{\text{noon}} = \cos(\phi) \cos(\delta) + \sin(\phi) \sin(\delta)$. Therefore, combining Eqs. (4.7) and (4.8),

$$I_{\text{noon}} = 13,750 G_{sc}(1.03)(0.262) \cos(\theta)$$

$$\text{or,} \quad I_{\text{noon}} = 5,020 \text{ Kw/m}^2 \cos(\theta) . \quad (4.9)$$

To aid in the computer programming, the same critical levels were used for both daily and hourly utilizability calculations. For J varying between 1 and 11, the critical level equation was:

$$I_c = 495 \text{ (KJ/m}^2\text{)} K_{\text{max}} C (J - 1). \quad (4.10)$$

K_{max} was a polynomial equation equal to the Bendt et al. [1] K_{max} term described in Chapter 3, where:

$$K_{\max} = 0.2075 + 2.771 \bar{K}_T - 4.750 \bar{K}_T^2 + 2.917 \bar{K}_T^3 \quad (4.11)$$

and C is a variable defined by the surface orientation. For horizontal and most south-facing surfaces:

$$C = \cos (\theta)_{\text{noon}} .$$

Otherwise, for

East & West surfaces:	$C = 0.7 K_T$ (Albany)
	$C = 0.8 K_T$ (San Antonio)
North surfaces:	$C = 0.3 K_T$
South surfaces,	
for $\cos (\theta)_{\text{noon}} < 0.3$:	$C = 0.3$

These critical levels allowed 8 to 11 non-zero daily utilizability values and 6 to 11 non-zero hourly utilizability values to be calculated for all conditions. Usually, 10 to 11 non-zero values resulted. For each case considered, only the first zero utilizability values were included in the RMS error comparisons. The other zero utilizability values provided redundant information, and therefore were considered invalid for RMS error calculation.

4.2.4 RMS error Calculation

With a total of 24 months of data, each with 8 global radiation measuring instruments and various methods of calculating the hourly

and daily utilizability, it is necessary to find a systematic and efficient approach for comparing the results. Because of its small time step, the utilizability calculated from minute data is the most accurate of all methods used for this study. Consequently, all of the other methods were compared to the minute data results. To aid in this comparison, the RMS error was calculated using all valid utilizability values. As used here, the RMS error is:

$$\text{Utilizability RMS Error} = \sqrt{\frac{\sum_{I_c=1}^J (\phi_A - \phi_B)^2}{J - 1}} \quad (4.12)$$

where ϕ_A is the minute data utilizability, and ϕ_B is the utilizability from one of the other four methods.

A large RMS error represents a pair of extremely different utilizability values, while a small RMS error represents a pair of virtually identical utilizability values. To find a cut-off RMS error value between identical and unidentical utilizability values, RMS error values were compared to graphs of the utilizabilities versus critical levels. Based on these comparisons, an RMS error of 0.02 or less represents an approximately identical set of utilizability values for the given range of critical levels. Figure 4.4 shows an example of minute data and hour data utilizability values having an RMS error of 0.02.

DAILY UTILIZABILITY, RMS ERROR = 0.02

Albany, NY 90S Feb 1981

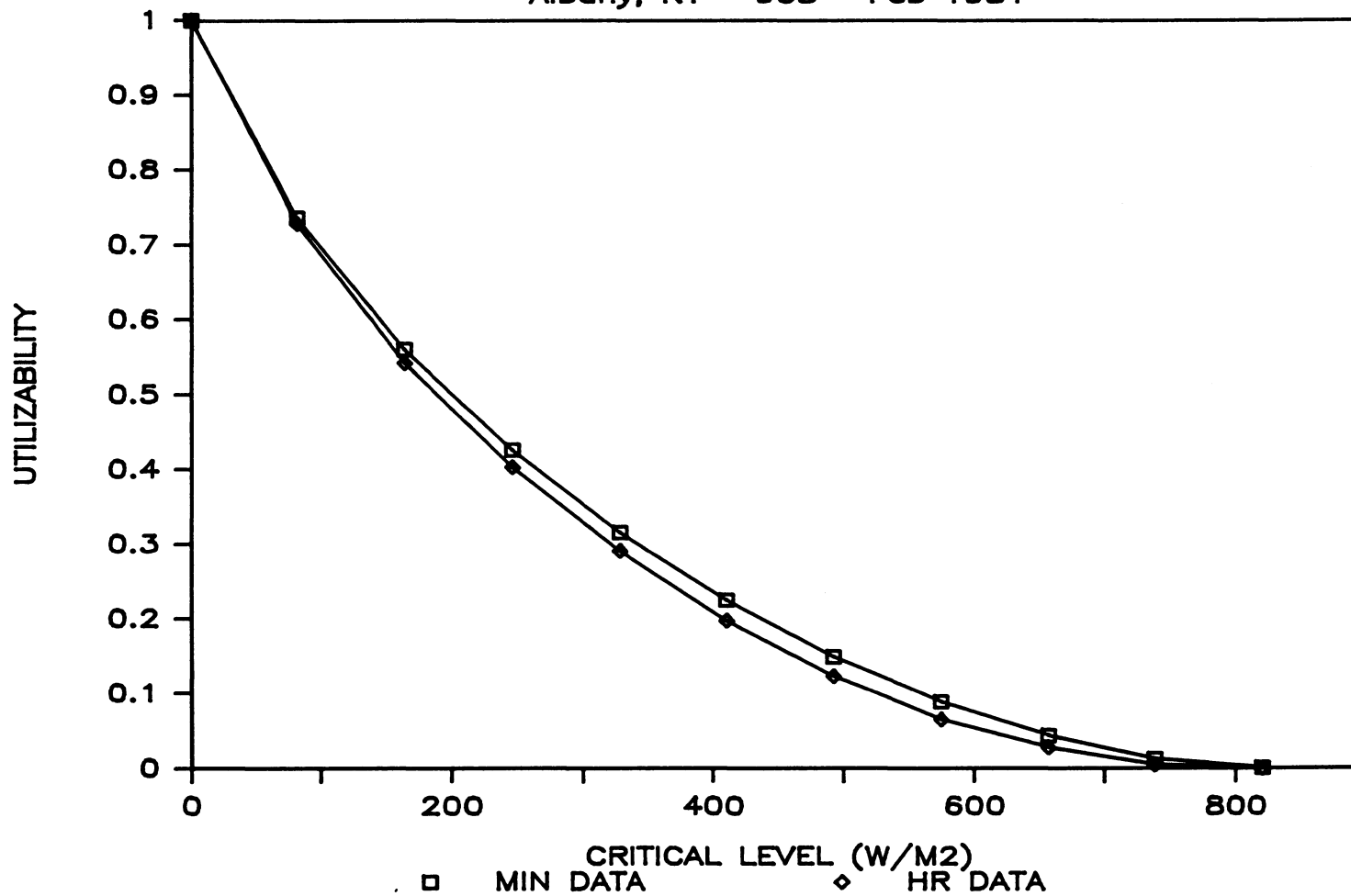


Figure 4.4: Utilizability Example of a 0.02 RMS error.

In Fig. 4.4, the utilizability from the minute data is greater than the utilizability from the hour data, as previously discussed. Also, at a critical level equal to 0 W/m^2 , both methods show a utilizability equal to 1, indicating that all of the energy is "utilizable". Due to this common "starting point" of 1, deviation between utilizability values calculated from any two methods occurs at non-zero critical levels.

4.2.5 Utilizability Method Abbreviations

Five methods of calculating utilizability were used in this study. Two methods used only measured data: minute data, or hour data. The other three methods utilized a form of Clark's correlation, as discussed in Section 4.2.2. To avoid confusion, the RMS error graphs presented in the following sections used label abbreviations to designate the appropriate method. The following key describes these abbreviations:

MN = Numbers from Minute Data

HR = Numbers from Hour Data

CL(k) = Numbers from Clark's correlation, with actual \bar{k}_T input

CL = Numbers from Clark's correlation, with actual \bar{k}_T input

CL(kR) = Numbers from Clark's correlation, with actual \bar{k}_T and \tilde{R} input

The RMS error between any two methods is therefore designated by hyphenating the two abbreviations.

4.3 Monthly-Average Hourly Utilizability

Monthly-average hourly utilizability is useful for analysis of solar processes where critical levels change during the monthly-average day. Defining independent critical levels for each monthly-average hour may yield a better prediction of the solar process performance, then assuming a constant critical level during the entire monthly-average day.

To find areas for improving ϕ correlations, results from the five calculation methods previously discussed were compared. Due to the number of surfaces studied, the comparisons have been categorized by surface orientation. All comparisons are for the hour 12-13.

4.3.1 South-Facing Surfaces at Slope Equal to Latitude

Figures 4.5 and 4.6 show the ϕ RMS error for the five methods of calculating utilizability during hour 12-13. Figure 4.5 is for San Antonio, while Fig. 4.6 is for Albany. The acceptable ϕ RMS error of 0.02 has been drawn in for reference. Within each of these bar graphs are several points of interest worth discussing.

A. Hour Data versus Minute Data:

For both San Antonio and Albany, the ϕ RMS error between the minute data and hour data exceeded 0.02 for seven of the twelve months. In a few cases, the difference between the hour data and minute data values are very noticeable: 0.041 for March in Albany, and 0.054 for June in San Antonio.

Figures 4.7 and 4.8 show the utilizability values for one month with an extremely low and with a high RMS error, respectively.

FIG. 4.5 UTILIZABILITY RMS ERROR

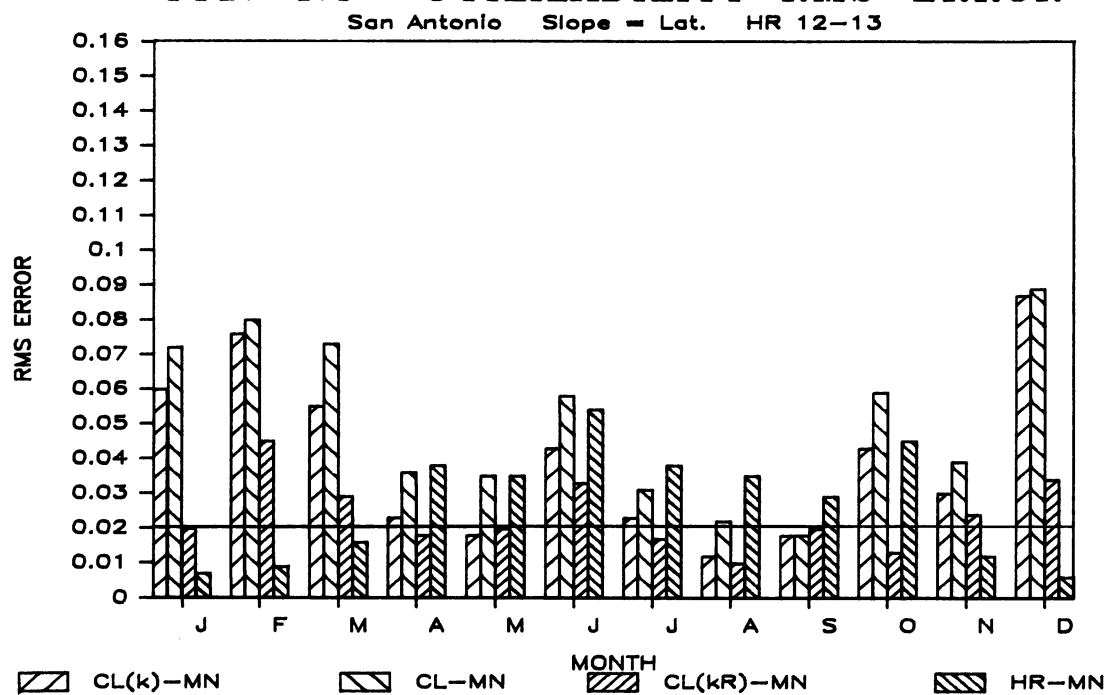
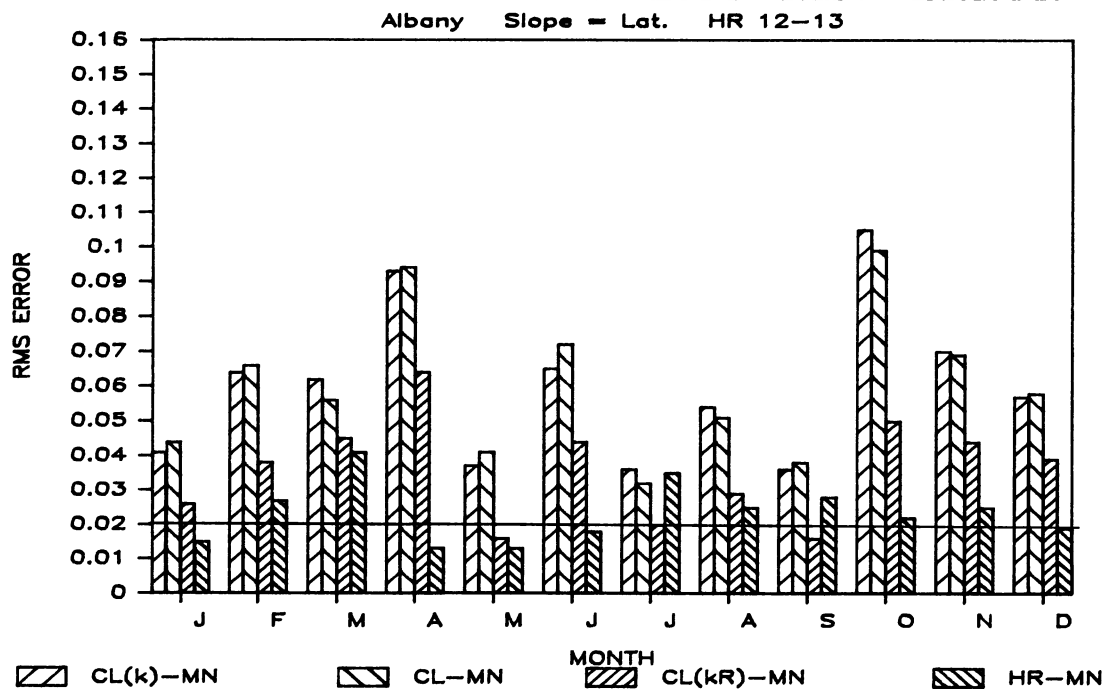


FIG. 4.6 UTILIZABILITY RMS ERROR



HOURLY UTILIZABILITY 30S JAN. 1982

San Antonio, TX Hour 12-13 $K_t=0.566$

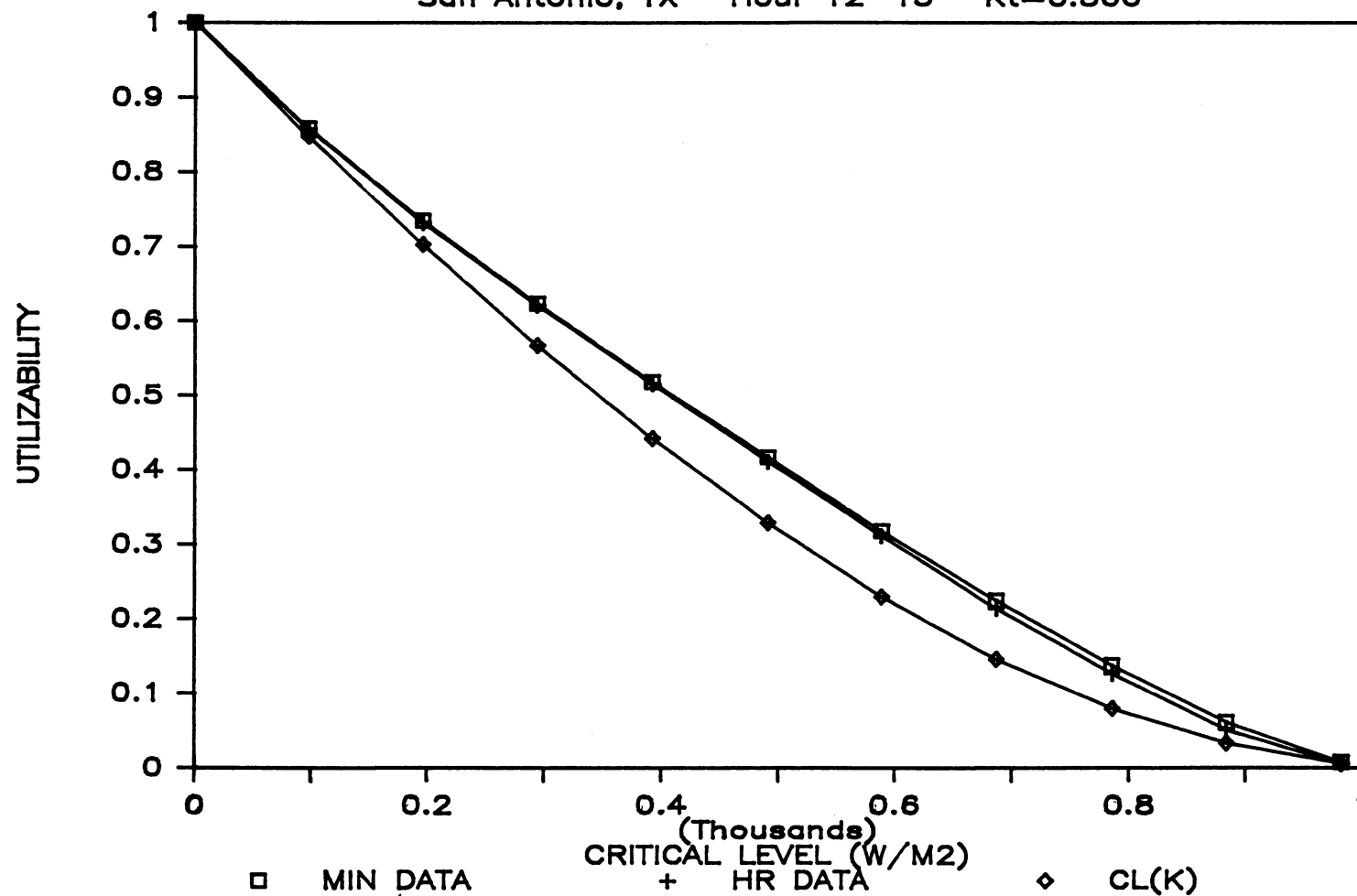


Figure 4.7: Monthly-average Hourly Utilizability Values.

HOURLY UTILIZABILITY 30S JUNE 1981

San Antonio, TX Hour 12-13 kt=0.555

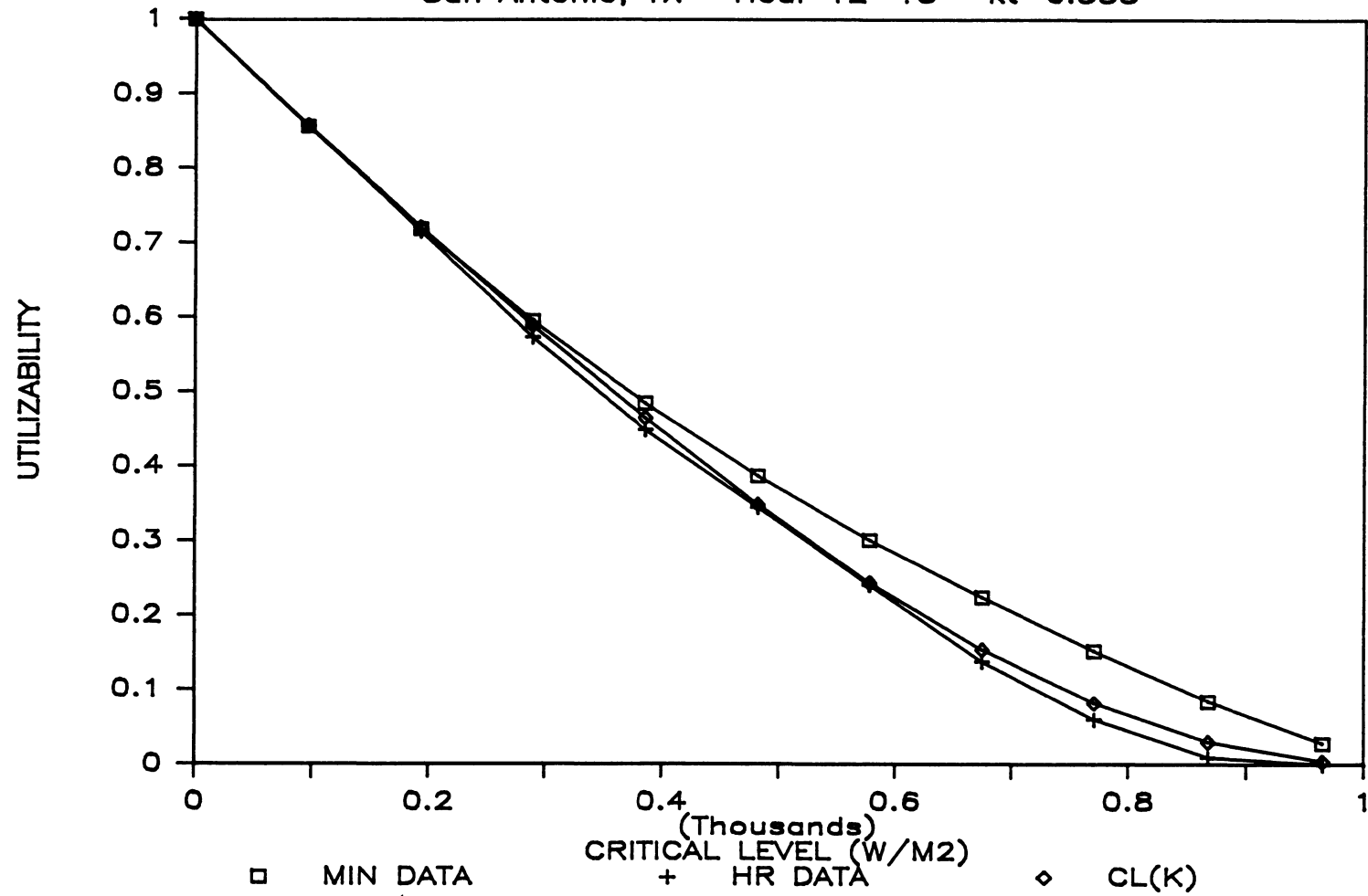


Figure 4.8: Monthly-average Hourly Utilizability Values.

Figure 4.7 is for San Antonio in January, and Fig. 4.8 is for San Antonio in June. Both utilizability graphs show values calculated from the minute data, hour data, and Clark's correlation using actual \overline{k}_T 's. The minute data versus hour data ϕ RMS error for San Antonio in January is 0.007, which is very acceptable. As seen in Fig. 4.7, the hour data and minute data utilizabilities are almost coincident. The Clark utilizability values will be discussed later.

In contrast, the minute data versus hour data ϕ RMS error for San Antonio in June (Fig. 4.8) is a very large 0.054. For June, the minute data provides valuable insolation information that was lost in the hour data. At a critical level of 400 W/m^2 , the minute data shows an approximate 9% increase from the hour data in utilizable energy.

The importance of using minute data for south-facing ϕ calculations is related to the differences between the minute data and hour data clearness frequency distributions discussed in Chapter 3. The clearness frequency distribution is a form of insolation profile for the given month. Therefore, the "steeper" the frequency distribution (more variability in insolation), the larger the utilizability.

Figure 3.11 shows the difference in clearness frequency distributions between the minute data and hour data for June in San Antonio for the hourly period 12-13. The minute data distribution is much steeper than the hour data distribution, and as expected, the utilizability from the minute data in Fig. 4.8 is much larger than the utilizability from the hour data. Similarly, Fig. 3.5 - January in

San Antonio - show almost identical distributions from both the minute data and hour data for the 12-13 hour period. As expected, the utilizabilities calculated from the minute data and hour data are also almost identical.

B. Clark Methods versus Minute Data:

Figures 4.5 and 4.6 also show the ϕ RMS error between the three Clark methods and the minute data. In most cases, the utilizability calculated from Clark's correlation using actual \overline{k}_T 's, CL(k)-MN, is significantly different than the utilizability calculated from the minute data. These large RMS errors are surprising, considering the insolation conditions are suppose to be identical, as defined by \overline{k}_T . The reasons for these differences in utilizability values may be threefold:

- 1) the minute data clearness frequency distributions for hourly periods do not coincide with the long-term hourly distribution built into Clark's correlation;
- 2) Clark's correlation poorly represents long-term hourly data; and
- 3) the isotropic radiation model used in Clark's correlation is inaccurate.

Clark's correlation was not derived from known long-term frequency distributions, although it was fitted to long-term hour utilizability data that would have represented these distributions. As shown in Chapter 3, the minute data clearness frequency distributions for hourly periods are always different from the generally accepted long-term distributions. Therefore, the differences between minute

data clearness frequency distributions for hourly periods and long-term hourly frequency distributions, will account for some of the differences between Clark's utilizability values and minute data values.

The theory of Clark's correlation not accurately representing long-term distributions can not be substantiated. Using actual \bar{k}_T 's and \tilde{R} 's in Clark's correlation eliminates "outside" sources of errors. Therefore, the ϕ RMS errors shown by the CL(kR)-MN bars represent the errors from minute data not representing long-term hourly distributions along with inherent correlation errors. These two sources of errors can not be separated. Figures 4.5 and 4.6 show the net effect of the minute data and correlation errors are below the allowed 0.02 RMS error in 10 of the 24 months studied. For other months, these RMS errors are significant, especially in Albany. However, without a larger data base, conclusive statements concerning the long-term accuracy of Clark's correlation can not be made.

While the CL(kR)-MN error bars representing these minute data and correlation errors are sometimes significant, the CL(kR)-MN ϕ RMS errors are the smallest of the three Clark methods, indicating that another source of error is also present.

Comparing the CL(k)-MN RMS error bars to the CL(kR)-MN bars on Figs. 4.5 and 4.6, show the largest error in Clark's correlation is usually caused by using the isotropic radiation model with Erbs' \bar{H}_d/\bar{H} model. The CL(k)-MN error bars typically are substantially the larger of the ϕ RMS error bars shown. Only on two occasions, March

and September in San Antonio, did the ϕ RMS error increase by using the actual R 's. For both of these cases, the increase was small, and the ϕ RMS error was still within the acceptable 0.02 range. The other 22 months show large reductions in the ϕ RMS error with the use of the correct radiation ratio in Clark's correlation. This finding supports the need to improve the monthly-average hourly radiation ratio model.

Figure 4.7, January in San Antonio, includes the CL(k) utilization values along with the previously discussed minute data and hour data values. The 0.06 RMS error reflects the underestimation of minute data ϕ by Clark's correlation using the isotropic model.

Comparing the ϕ RMS error bars between CL(k)-MN and CL-MN shows the effect of using the r_t/r_d correlation between daily and hourly values. For San Antonio, using \bar{K}_T 's and r_t/r_d usually caused noticeable increase in the ϕ RMS error, implying the distribution of \bar{K}_T 's within the monthly-average day did not represent the long-term distributions. Since Clark's correlation is dependent on \bar{K}_T , the incorrect estimation of \bar{K}_T caused erroneous calculation of the utilization. For Albany, the RMS error occasionally decreased, but never significantly. Compared to the other RMS errors for both San Antonio and Albany, the largest error in Clark's correlation is still caused by using the monthly-average hourly isotropic radiation model with Erbs' \bar{H}_d/\bar{H} correlation.

4.3.2 South-Facing Vertical Surfaces

Figures 4.9 and 4.10 show the ϕ RMS errors for south-facing vertical surfaces in San Antonio and Albany, respectively. The same trends that are found for south-facing surfaces equal to latitude, can also be seen here. The hour data and minute data occasionally give different results as shown by the HR-MN bars, but the differences are usually slightly smaller than the differences for slope equal to latitude. Most of the hour data versus minute data errors are around the acceptable 0.02 RMS error. As shown in the slope equal to latitude ϕ RMS errors, the differences between using \bar{K}_T and \bar{K}_T in Clark's correlation, CL(k)-MN versus CL-MN, is usually negligible.

For San Antonio, the largest source of error in Clark's correlation is the radiation ratio model, as is seen by comparing CL(k)-MN to CL(kR)-MN. The largest RMS error shown by CL(k)-MN occurs during winter months where the RMS error may be as high as 0.145. This pattern of large utilizability errors during winter months corresponds to the large winter \tilde{R} errors found in the isotropic radiation ratio analysis in Chapter 2. During winter months when the sun is low in the sky, the normal component of beam and circumsolar diffuse radiation increases on vertical south-facing surfaces. Since the isotropic model lacks a circumsolar diffuse radiation component, the underestimation of radiation increases, which decreases the estimation of utilizable energy. The estimation of \bar{H}_d/\bar{H} is also large during winter months, as shown in Fig. 2.1. This overestimation of

FIG. 4.9 UTILIZABILITY RMS ERROR

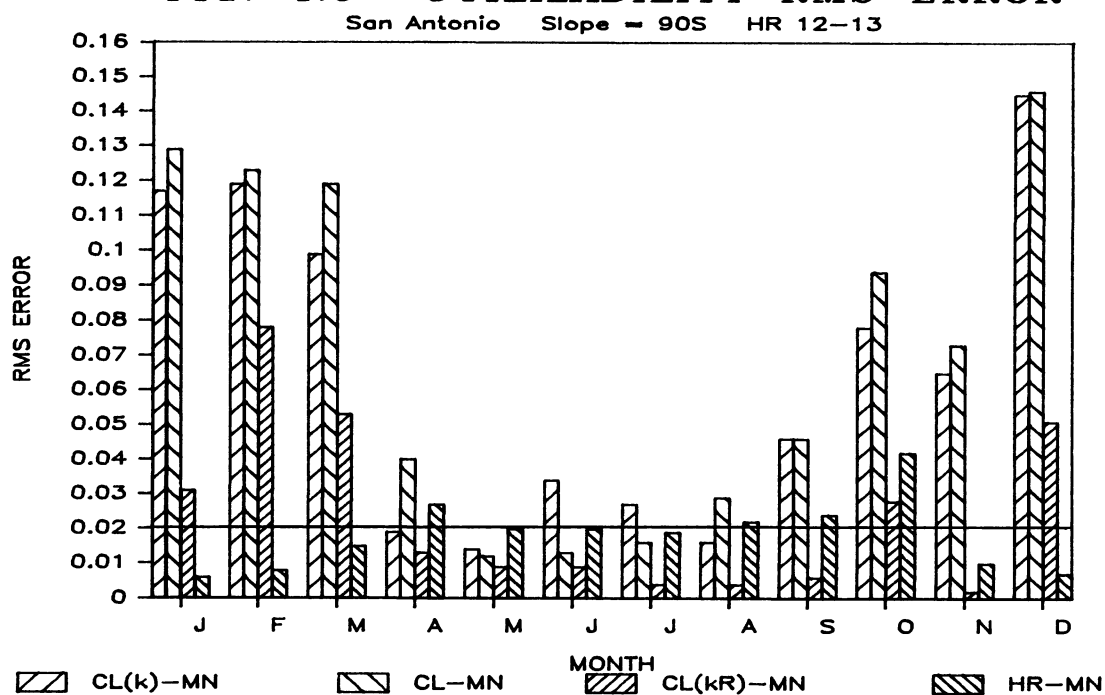
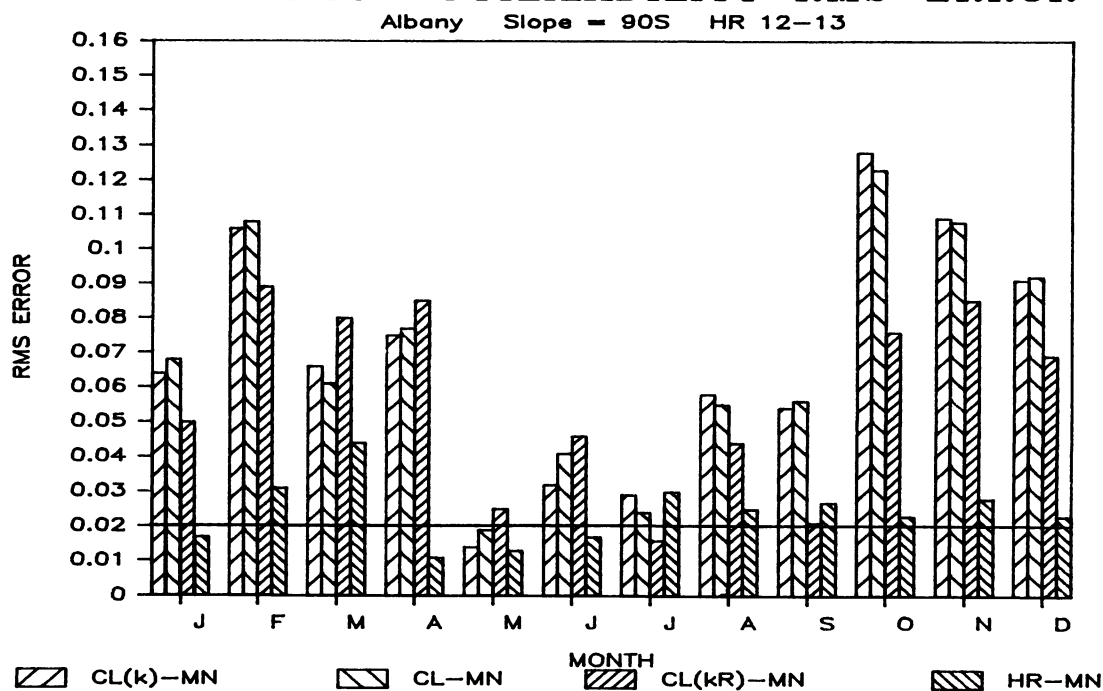


FIG. 4.10 UTILIZABILITY RMS ERROR



diffuse radiation underestimates the beam radiation component in the isotropic model, which adds a second source of error in the estimation of south-facing tilted surface radiation.

Figure 4.11 shows the minute data, $CL(k)$, and $CL(kR)$ utilization values for December, where the $CL(k)$ -MN RMS error is 0.145 and the $CL(kR)$ -MN RMS error is 0.05. As expected for Clark's correlation using the isotropic model, $CL(k)$ grossly underestimates the minute data values. At a 400 W/m^2 critical level, $CL(k)$ shows a utilization value that is 58% of the minute data value. Although this error results from comparing a long-term correlation to one month of data, an underestimation in utilizable energy by 42% would be a substantial error for a solar heating system during winter months.

For all critical levels, Clark's correlation using actual radiation ratios $CL(kR)$, better estimates the minute data ϕ values than $CL(k)$. At a 400 W/m^2 critical level, $CL(kR)$ underestimates the minute data value by 16%. While a 16% error is still large, the underestimation of minute data ϕ by Clark's correlation is reduced by 26 percentage points, just by using the actual \tilde{R} . The 16% error is attributed to the minute data not corresponding to long-term hourly distributions, and to inherent correlation error in Clark's model.

For Albany - Fig. 4.10, the RMS error bars for $CL(kR)$ -MN indicate the combined effect of Clark's correlation misrepresenting long-term hour distributions and the minute data base differing from long-term hour distributions, are substantial for most months. Since the minute data represents only a one year data base, the differences be-

HOURLY UTILIZABILITY DEC. 1982

San Antonio, TX Slope = 90S

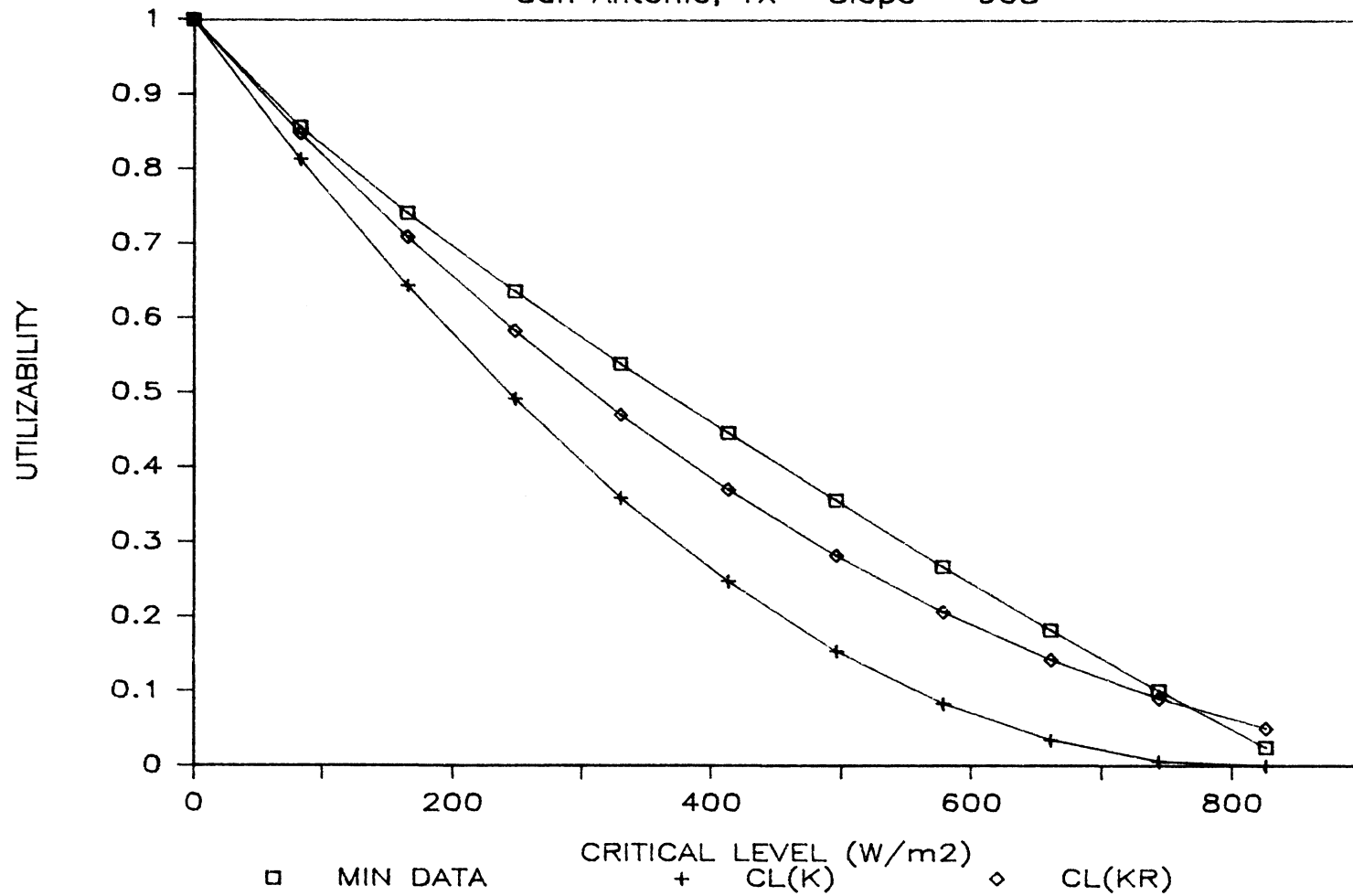


Figure 4.11: Monthly-Average Hourly Utilizability Values (Hour 12-13).

tween the minute data values and long-term hour distributions are suspected of causing the largest part of this error. As shown by the CL(k)-MN error bars, utilizability values calculated from Clark's correlation using the isotropic radiation model with Erbs' $\overline{H}_d/\overline{H}$ correlation are significant during winter months.

4.3.3 West-Facing Vertical Surfaces

Figures 4.12 and 4.13 show the ϕ RMS error for west-facing vertical surfaces in San Antonio and Albany, respectively. In San Antonio, the RMS errors are relatively small compared to the south-facing RMS errors. The worst RMS error is 0.045, which represents the difference between hour data and minute data utilizability. Because of the small and random changes in RMS error, no trends are found in the various utilizability calculation methods. In Albany, six months show substantial error in Clark's correlation using the isotropic radiation model. The worst cases show an RMS error around 0.17. However, as discussed in Chapter 3, some of the west-facing Albany data are questionable, which could cause these large differences in utilizability values between Clark's correlation and minute data.

4.3.4 North-Facing Vertical Surfaces

Figures 4.14 and 4.15 show the ϕ RMS error for north-facing vertical surfaces in San Antonio and Albany, respectively. For all 24 months studied, the difference in utilizability values between hour data and minute data are within the accepted 0.02 RMS error. The largest differences in minute data and hour data insolation

FIG. 4.12 UTILIZABILITY RMS ERROR

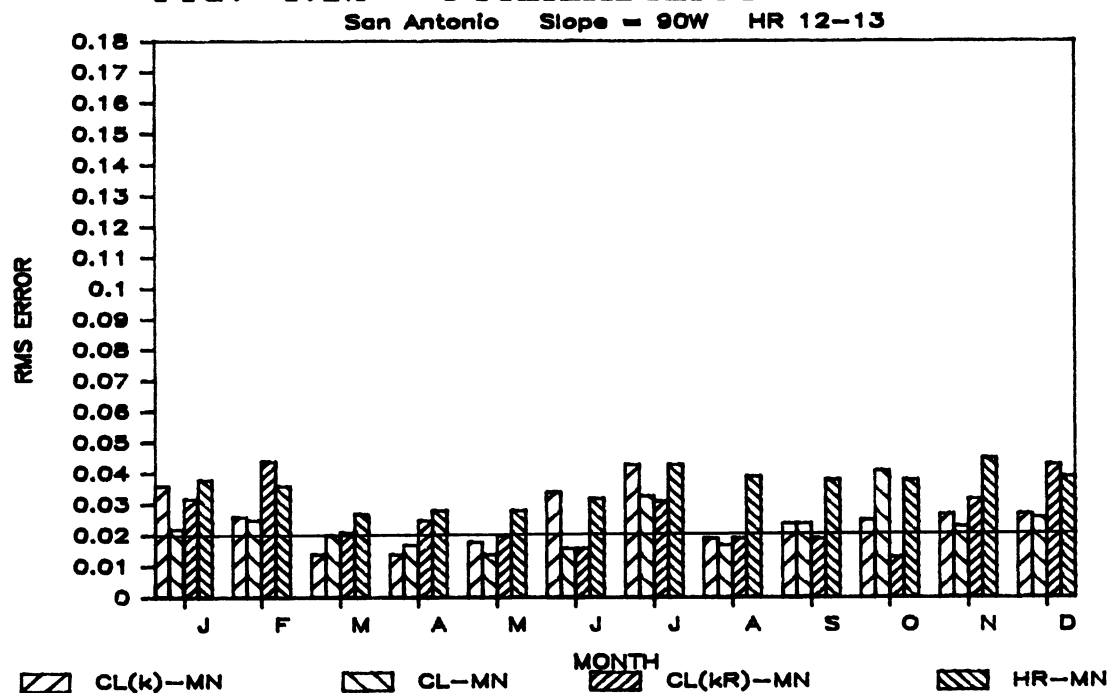


FIG. 4.13 UTILIZABILITY RMS ERROR

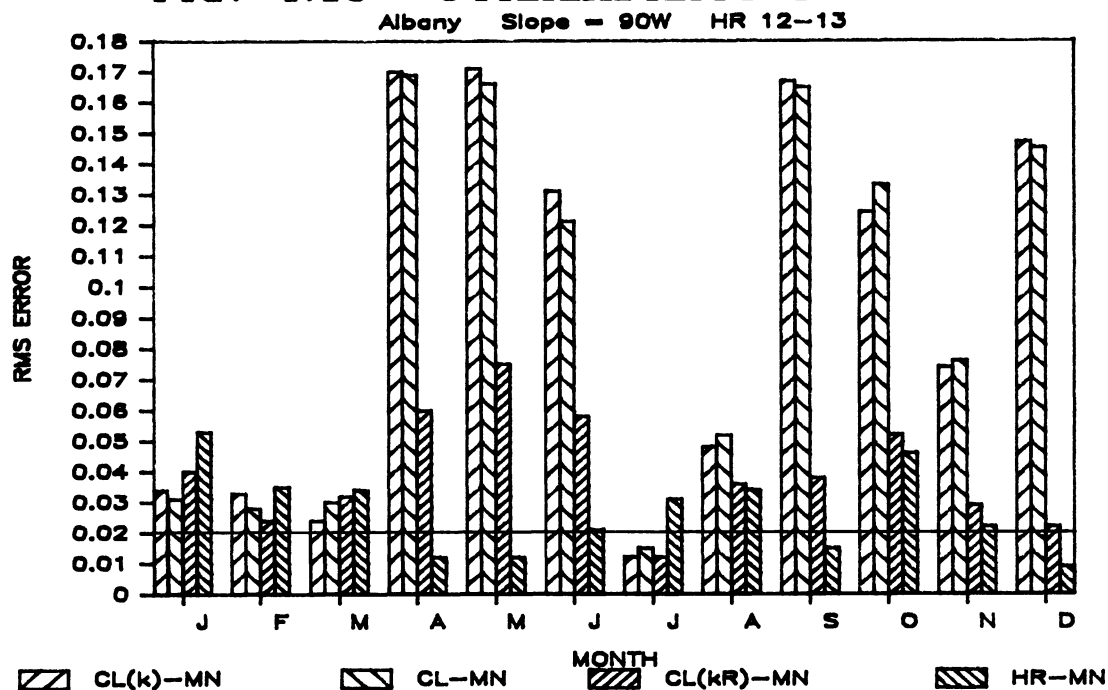


FIG. 4.14 UTILIZABILITY RMS ERROR

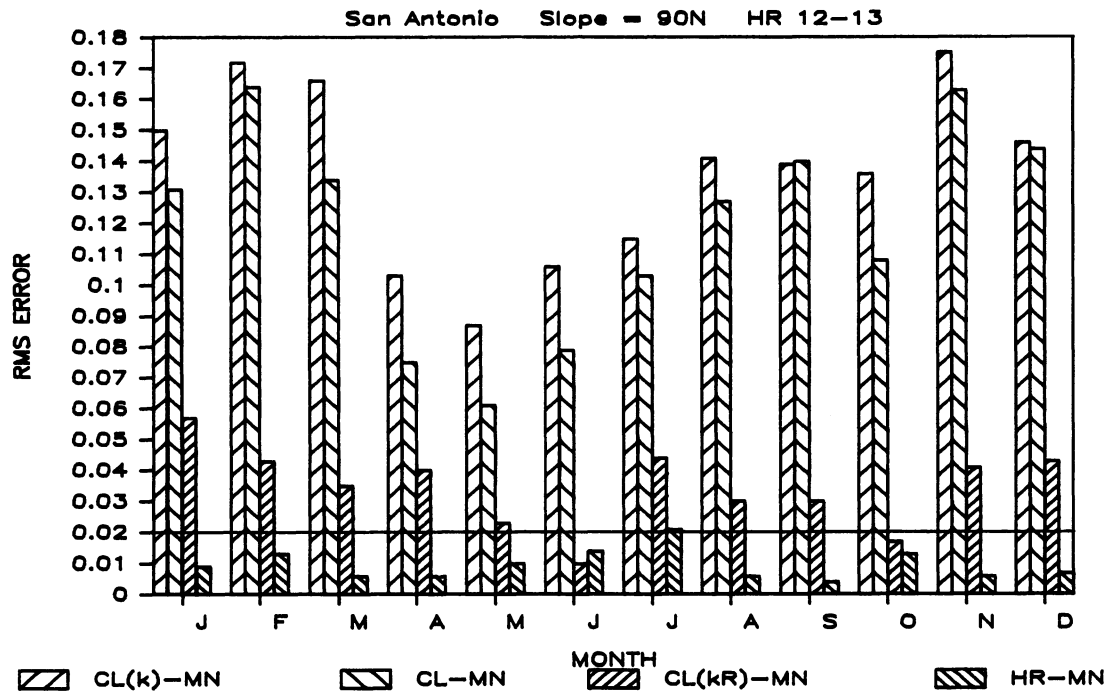
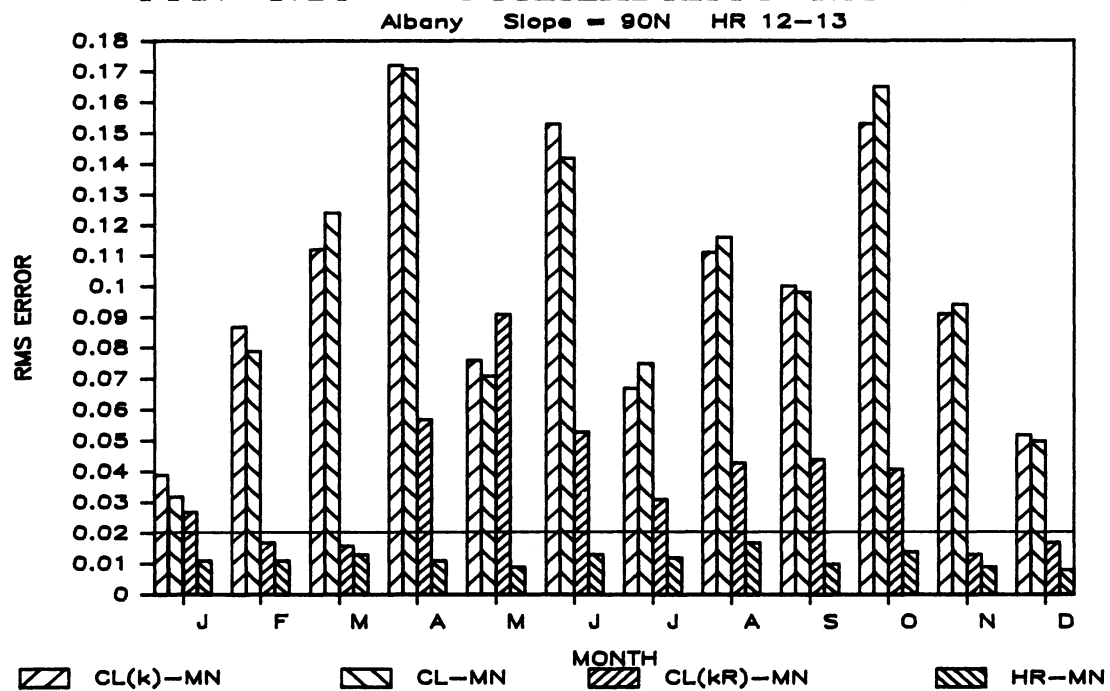


FIG. 4.15 UTILIZABILITY RMS ERROR



levels are thought to be caused from intermittent beam radiation. However, north-facing surfaces receive only diffuse and ground reflected radiation, except for possible early morning and late evening beam radiation during summer months. Therefore, the north-facing minute data and hour data insolation levels should be similar, as indicated by the low ϕ RMS errors.

The largest error associated with Clark's correlation is from the monthly-average hourly isotropic radiation model with Erbs' $\overline{H}_d/\overline{H}$ correlation. The worst cases show ϕ RMS errors exceeding 0.17. As shown in Chapter 2, the isotropic assumption noticeably overestimates the actual radiation on north-facing surfaces, which causes Clark's correlation to grossly overestimate the utilizable energy. A typical example is shown in Fig. 4.16 for April in Albany. Since north-facing surfaces receive low insolation levels, the critical levels are extremely low compared to south-facing surfaces. At a 70 W/m^2 critical level, $CL(k)$ overestimates the minute data by 85%. Using the actual \tilde{R} in Clark's correlation causes a 26% underestimation of the minute data value, as shown by $CL(kR)$.

Another source of error in Clark's utilizability values are from the combined effects of Clark's correlation misrepresenting long-term data, and differences between this short-term minute data base and long-term hour insolation levels. The worst error for these effects is 0.09 in Albany during May. In this case, the ϕ RMS error increases by using actual \tilde{R} 's. For all other cases, using actual \tilde{R} 's in Clark's correlation decreases the ϕ RMS error.

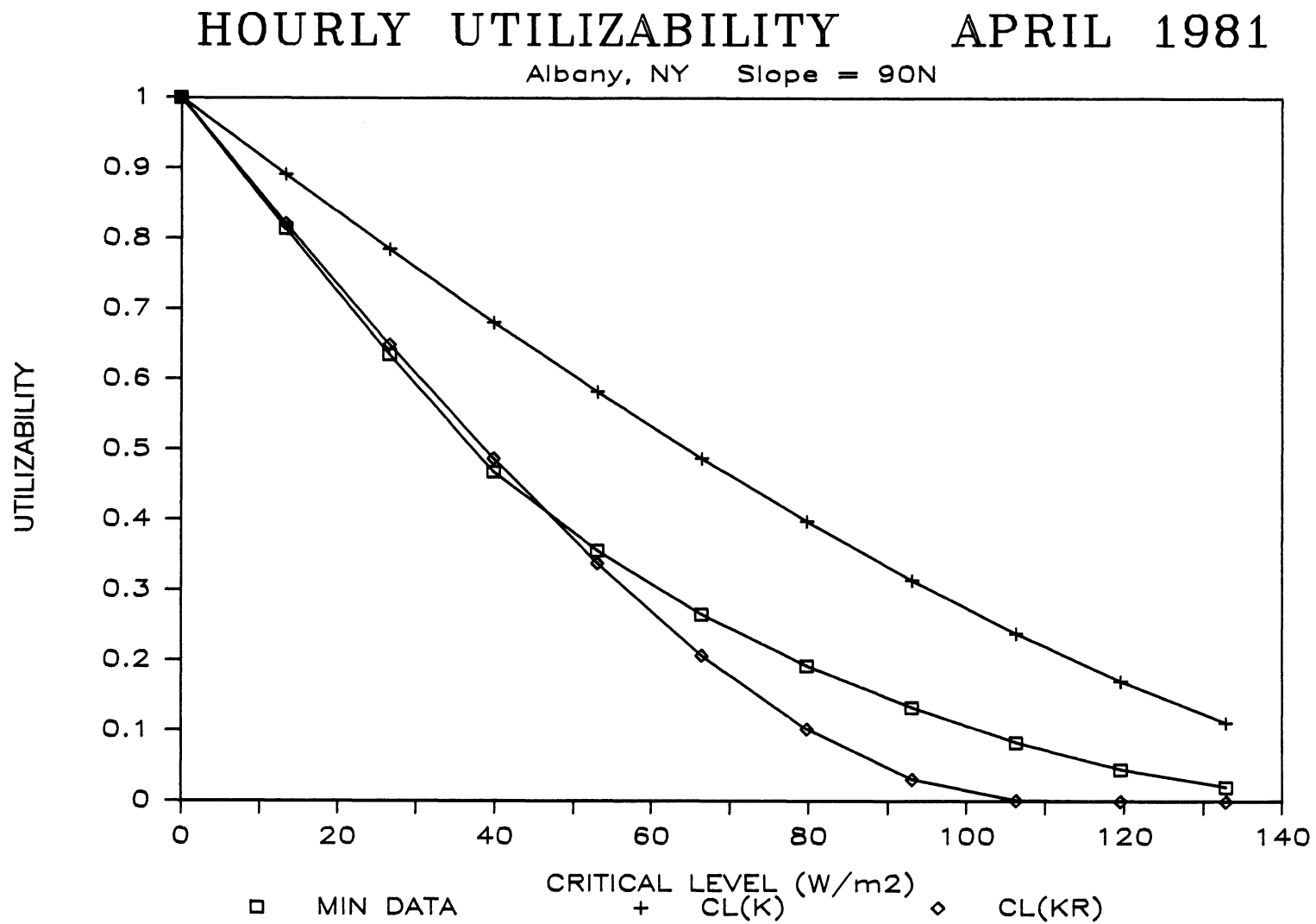


Figure 4.16: Monthly-Average Hourly Utilizability Values (Hour 12-13).

4.3.5 Summary of Monthly-Average Hourly Utilizability Comparisons

The comparison of utilizability values incorporates a short-term data base, and therefore conclusions concerning long-term effects can not be made. However, noteworthy indications have been found.

For south-facing surfaces during hour 12-13, half of the months studied show significant differences between minute data and hour data utilizabilities. This difference between minute data and hour data utilizability values is mostly attributed to variation in the beam component of radiation, caused by passing clouds. Although the long-term difference between minute and hour data are not known, a significant difference in utilizability is expected for some months with partly cloudy conditions (i.e., $\bar{K}_T \sim 0.5$). As discussed in Chapter 3, other unknown independent parameters may also affect insolation levels, besides \bar{K}_T . The effects of these parameters on utilizability is presently unknown. For north-facing surfaces, the differences between minute data and hour data ϕ values are negligible, due to the lack of a beam radiation component.

The largest error in Clark's correlation is from the monthly-average hourly isotropic radiation ratio model with Erbs' \bar{H}_d/\bar{H} correlation. Substantial reduction in these utilizability correlation errors is usually made by using actual \tilde{R} 's calculated from the data. Although differences can usually be seen between Clark's correlation with actual \bar{K}_T 's and Clark's correlation with actual \bar{K}_T 's and the r_t/r_d relation, this difference is typically small compared to the error from using the isotropic radiation model.

4.4 Monthly-Average Daily Utilizability

4.4.1 General Discussion

Monthly-average daily utilizability is useful for analysis of solar processes with constant critical levels for all hours during a month, or as a theoretical limit for a solar process. Clark's monthly-average hourly correlation can still be used to find the monthly-average daily value, by summing the numerator and denominator components of ϕ , over all daylight hours. The ratio of these sums is the monthly-average daily utilizability, $\bar{\phi}$. For this study, the same five methods used to calculate ϕ were also used to calculate $\bar{\phi}$.

The $\bar{\phi}$ RMS errors have been plotted on the same scales as the ϕ RMS errors, for the respective surface orientations. In general, the magnitude of the $\bar{\phi}$ RMS error is smaller than the corresponding hourly values discussed in Section 4.3. Mid-day insolation levels are the largest values occurring within a day. Consequently, the potential differences between utilizable energy calculated by the five methods described is also large. In comparison, monthly-average daily utilizability calculations incorporate all daylight hours, and therefore minimize large deviations that were observed during mid-day hours. Even though the $\bar{\phi}$ RMS error magnitudes are smaller, the trends shown by the $\bar{\phi}$ RMS error analysis are still present.

Figures 4.17 through 4.24 show the $\bar{\phi}$ RMS errors for the same surface orientations discussed in Section 4.3 for both San Antonio and Albany. Figures 4.17 and 4.18 are for south-facing surfaces at slope equal to latitude, Figs. 4.19 and 4.20 are for south-facing

FIG 4.17 DAILY UTILIZABILITY RMS ERROR

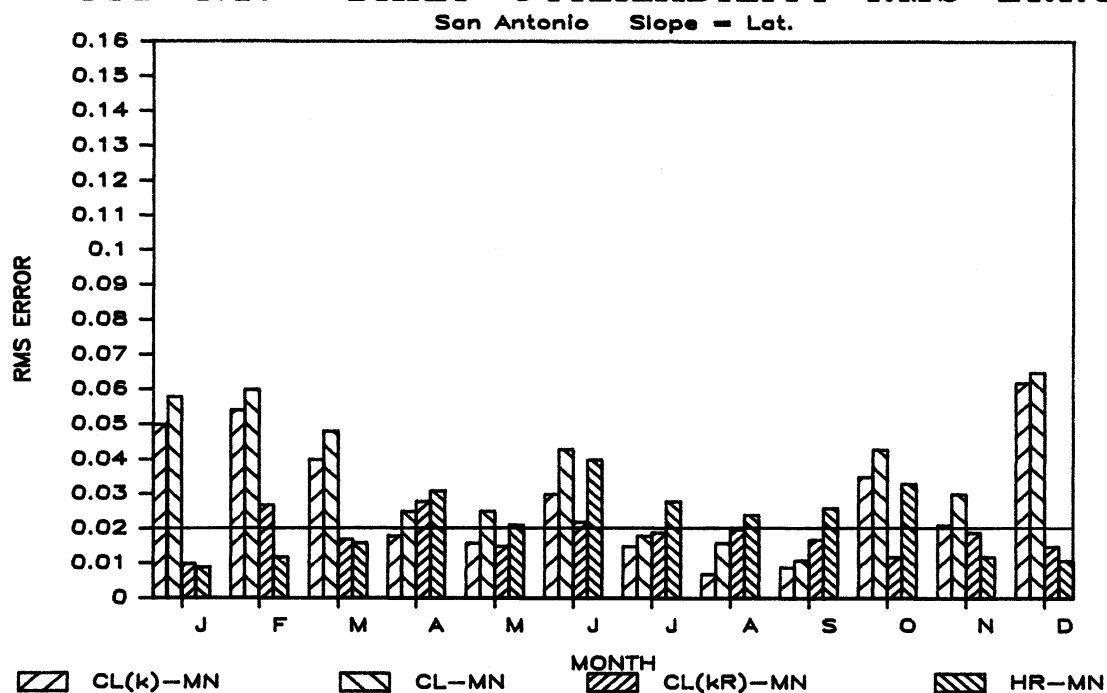


FIG 4.18 DAILY UTILIZABILITY RMS ERROR

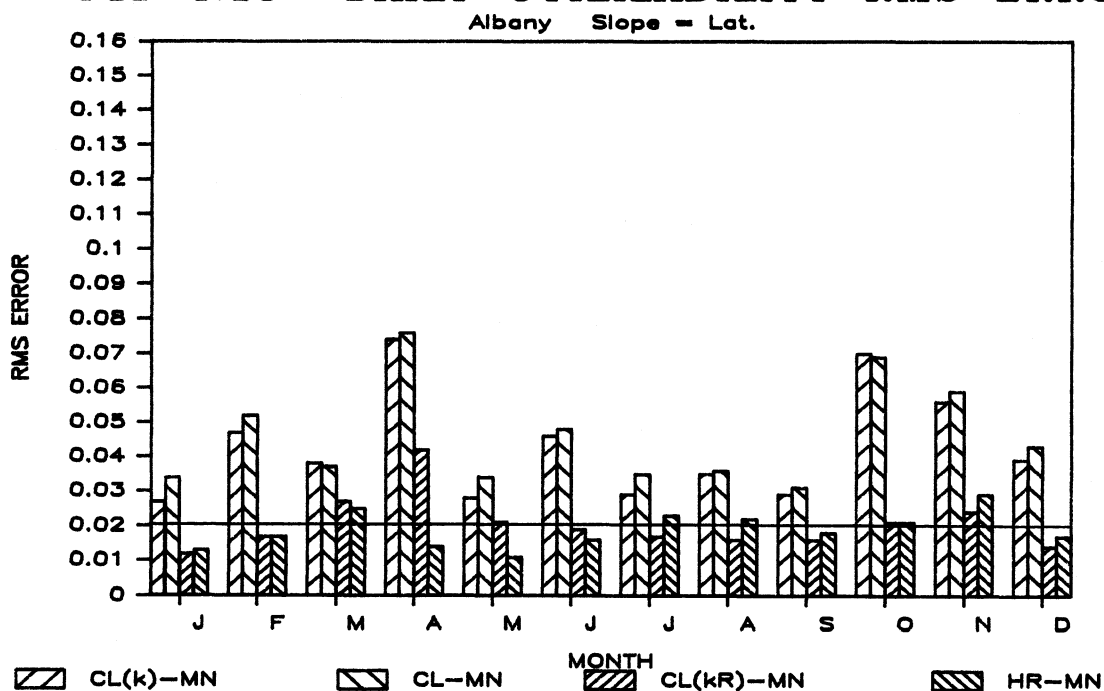


FIG 4.19 DAILY UTILIZABILITY RMS ERROR

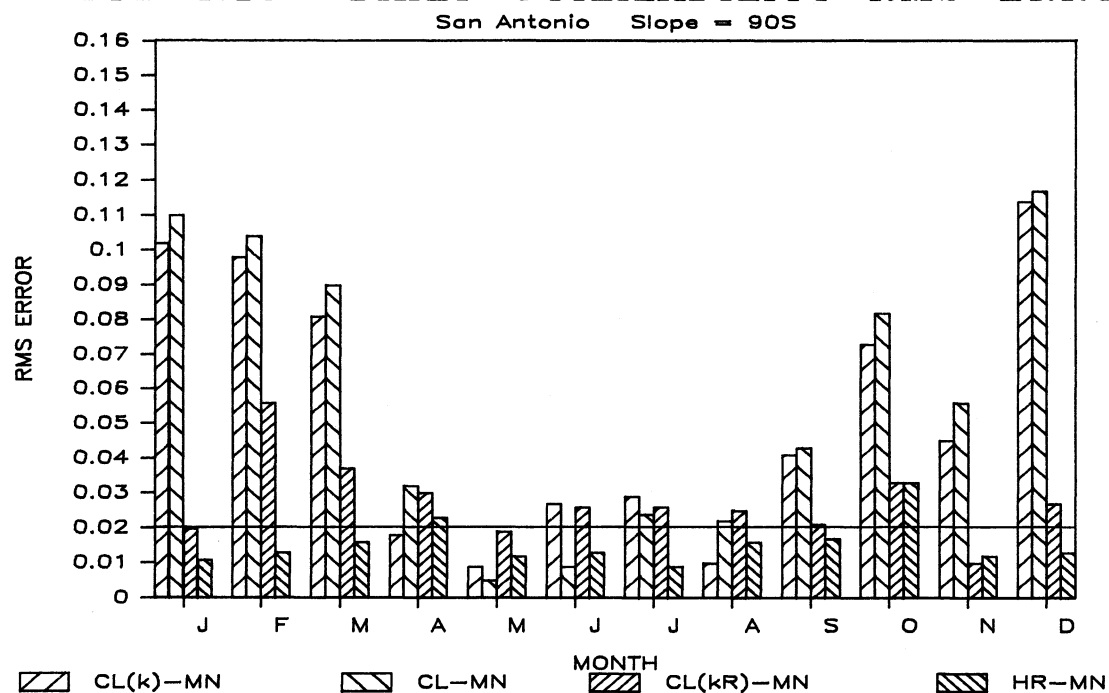


FIG 4.20 DAILY UTILIZABILITY RMS ERROR

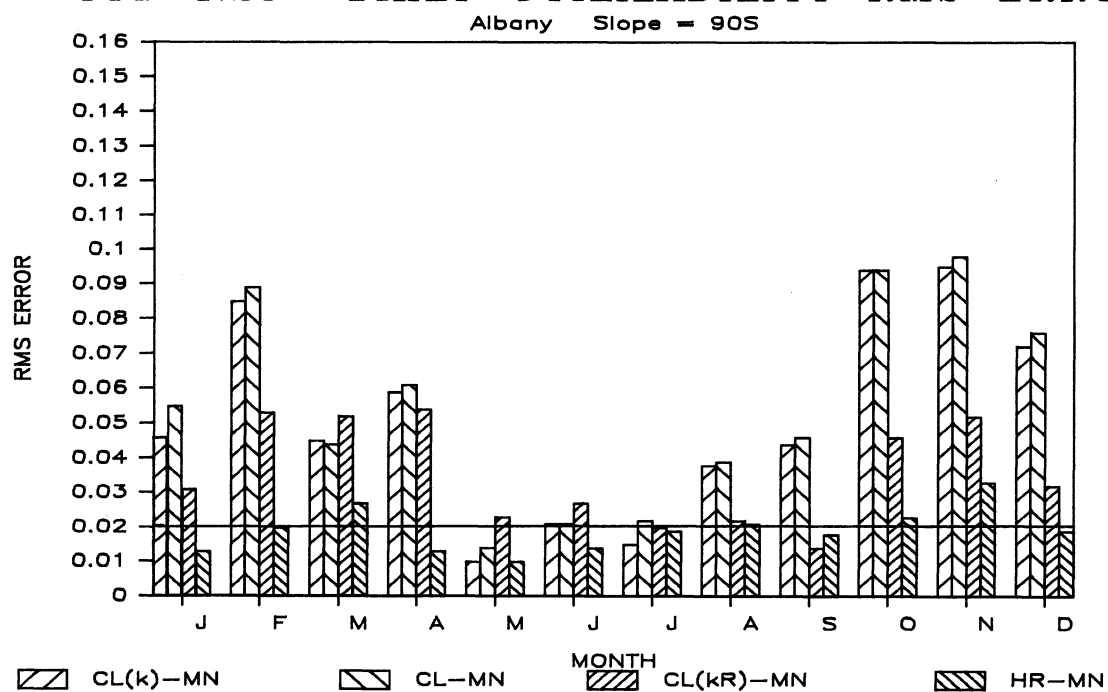


FIG 4.21 DAILY UTILIZABILITY RMS ERROR

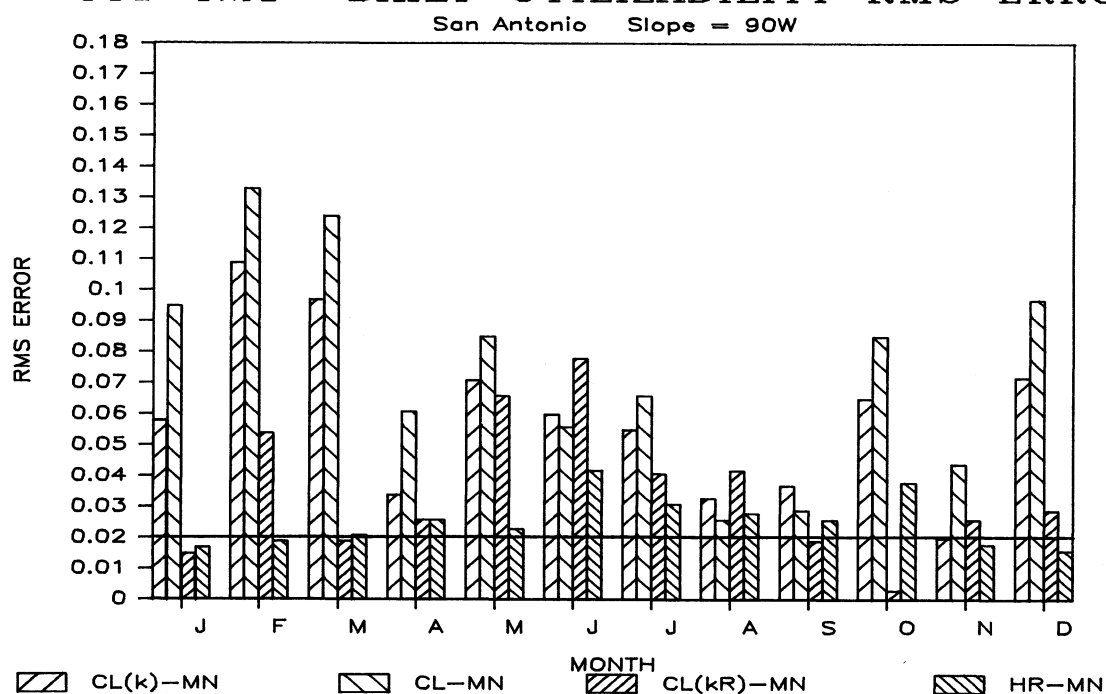


FIG 4.22 DAILY UTILIZABILITY RMS ERROR

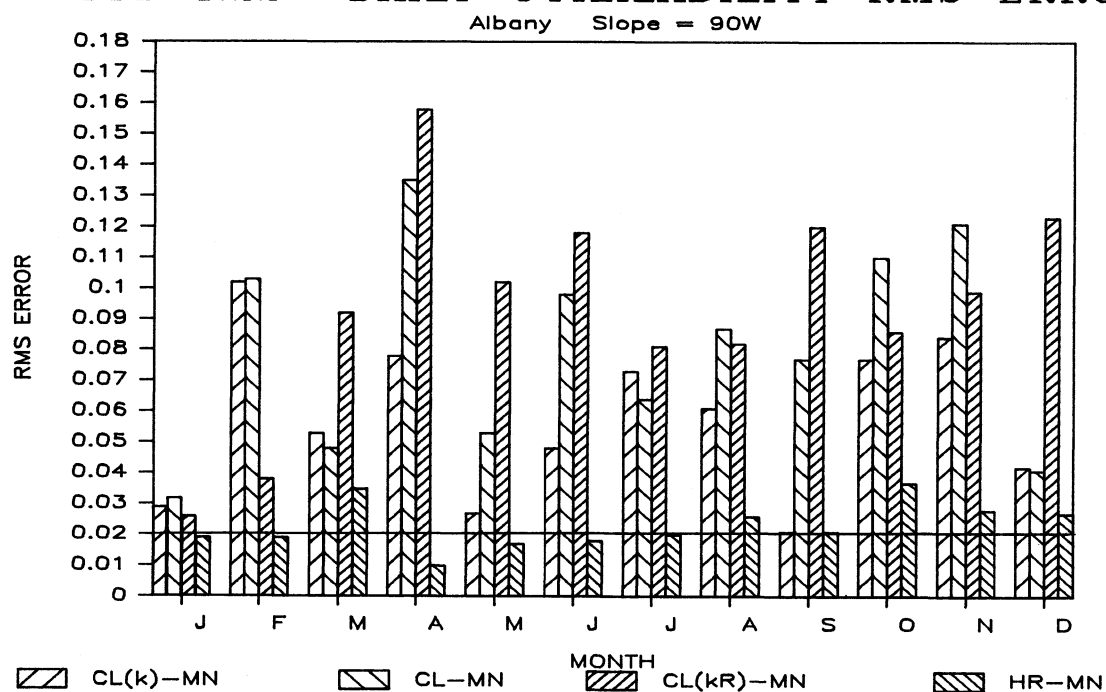


FIG 4.23 DAILY UTILIZABILITY RMS ERROR

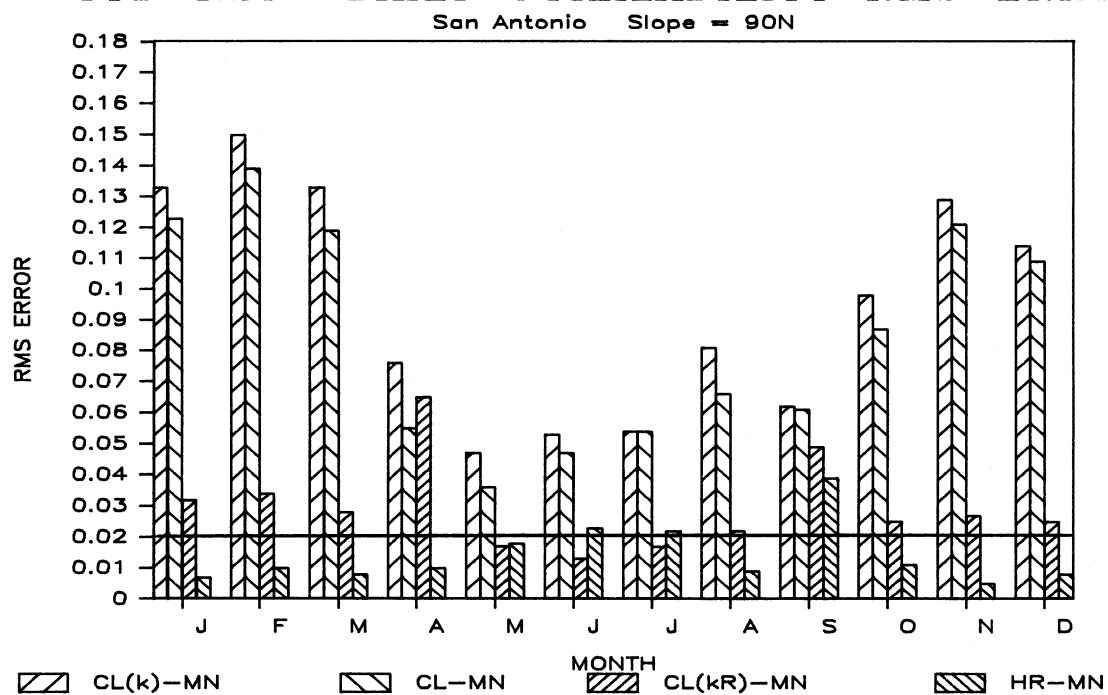
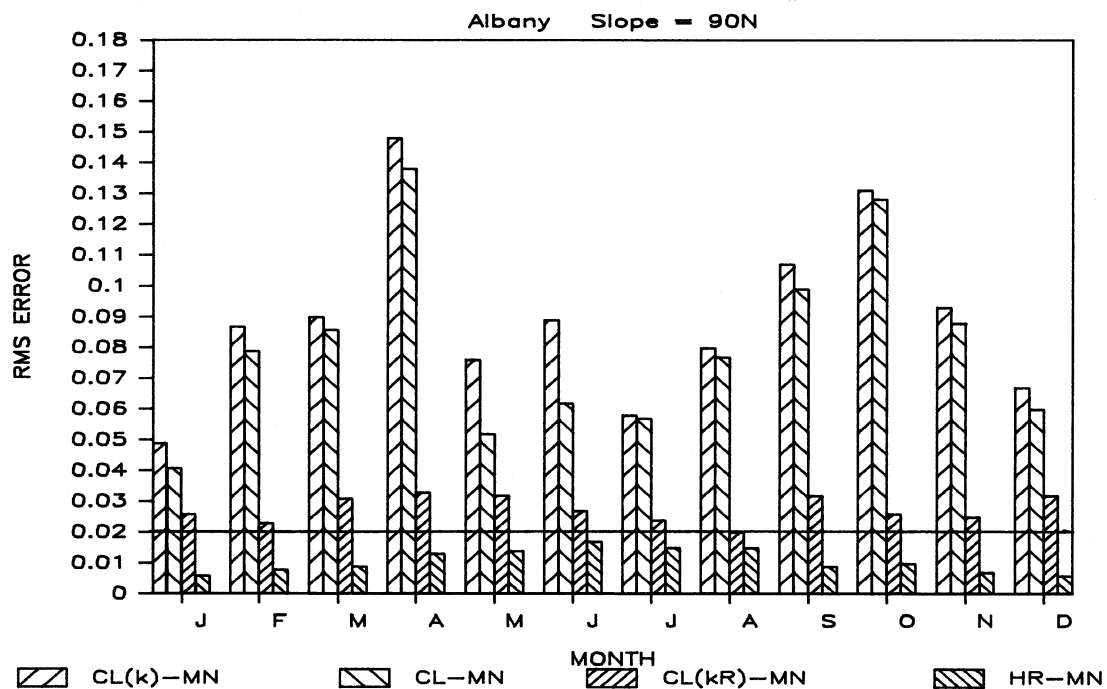


FIG 4.24 DAILY UTILIZABILITY RMS ERROR



vertical surfaces, 4.21 and 4.22 are for west-facing vertical surfaces, and 4.23 and 4.24 are for north-facing vertical surfaces.

Surfaces receiving large components of beam radiation show the largest difference between minute data and hour data utilizability. South-facing surfaces at slope equal to latitude, which potentially receive large amounts of beam radiation, show significant differences for approximately half of the months studied. South-facing vertical surfaces, which receive less beam radiation than surfaces at slope equal to latitude, only show significant differences in 4 of the 24 months studied. West-facing vertical surfaces may receive large amounts of beam radiation during afternoon hours. San Antonio frequently has afternoon clearings, and consequently 8 of the 12 months studied show significant differences between minute data and hour data utilizability values. Albany only shows 5 months with significant differences. North-facing surfaces may receive some beam radiation near sunrise and sunset during long summer days. Consequently, only June and July in San Antonio show minute data versus hour data ϕ RMS errors slightly exceeding 0.02. All other months studied show negligible differences.

The largest error in Clark's correlation results from using the isotropic radiation model with Erbs' diffuse fraction, as is seen by comparing the CL(k)-MN error bars to the CL(kR)-MN error bars. Based on the findings of Chapter 2, including a circumsolar diffuse radiation component in the radiation ratio model should usually improve the accuracy of utilizability calculated from Clark's correlation.

Improved methods for calculating $\overline{H}_d/\overline{H}$ and the resulting monthly-average hourly diffuse fraction also need to be made, as indicated in Section 2.6.1. Bad data is suspected of causing the large CL(kR)-MN errors shown in Fig. 4.22, for west-facing vertical surfaces in Albany.

Using r_t/r_d to calculate \overline{k}_T from \overline{K}_T in Clark's correlation does cause a noticeable difference in utilizability values. As discussed in Section 4.3, the r_t/r_d relation assumes symmetrical insolation levels during the day. While both San Antonio and Albany show asymmetrical insolation levels, as reflected by the difference between CL-MN and CL(k)-MN error bars, the error associated with the symmetrical assumption is small compared to the error resulting from using the isotropic \tilde{R} .

4.4.2 Summary of Monthly-Average Daily Utilizability Comparisons

The trends found in the ϕ analysis, Section 4.3, are also found in the $\overline{\phi}$ analysis. Minute data versus hour data $\overline{\phi}$'s are frequently significantly different for those surfaces that receive large components of beam radiation during the day. Surfaces with little or no beam radiation usually show negligible differences between minute data and hour data $\overline{\phi}$'s. The largest error in Clark's correlation is from the monthly-average hourly isotropic radiation ratio model with Erbs' $\overline{H}_d/\overline{H}$ correlation. The error associated with the symmetrical insolation assumption for calculating \overline{k}_T is small compared to the error resulting from using the isotropic radiation model and estimated diffuse fraction.

4.5 Conclusion

Comparisons of monthly-average hourly utilizability and monthly-average daily utilizability calculated from minute data, hour data, and three versions of Clark's correlation, were made. The comparisons incorporate a two year data base, and therefore conclusions concerning long-term effects can not be made. However, the following indications were found.

The largest difference between minute data and hour data values result mostly from intermittent beam radiation. Therefore, surfaces with large amounts of normal incident beam radiation (e.g., south-facing surfaces at slope equal to latitude) will show the largest differences between minute data and hour data utilizability values. In comparison, surfaces with little or no beam radiation will show small differences between minute data and hour data utilizability values.

The comparison of short-term minute data utilizability values to Clark's long-term hourly correlation values show significant differences in some months and orientations. Based on the comparison of clearness frequency distributions in Chapter 3, a long-term difference between minute data and Clark's correlation is expected for surfaces receiving large amounts of normal incident beam radiation.

The monthly-average hourly isotropic radiation ratio model using Erbs diffuse fraction correlation is usually the largest source of error in Clark's utilizability correlation. For south-facing surfaces, the largest errors occur during winter months, where under-

estimations are sometimes substantial. The worst case is a 42% underestimation of the minute data utilizability. In comparison, Clark's correlation using actual \tilde{R} 's underestimates the minute data utilizability by 16% for the same conditions. This 16% error results from: the data base not corresponding to long-term distributions, inherent correlation errors, and modeling discrepancies between a minute-by-minute data base and an hourly data base. Using actual \tilde{R} 's in Clark's correlation usually reduces the error in estimating utilizability. Therefore, improvements as large as 30% are predicted for long-term estimations for south-facing surfaces, with the use of improved \tilde{R} models and a utilizability correlation based on minute data.

RECOMMENDATIONS

This study reevaluates isotropic radiation ratio models; clearness frequency distributions; and utilizability values calculated from minute data, hour data, and Clark's [3] correlation. Mathematical model results are compared to a two year data base, which was collected by Trinity University and State University of New York at Albany as part of the Solar Energy and Meteorological Research and Training Site Program. Based on the findings in this present study, the following topics should be investigated.

RMS errors as large as 0.32 were found between Erbs' hourly diffuse fraction correlation and data values. Garrison [7] found the diffuse fraction to be related to five independent parameters: global solar irradiance; solar elevation; surface albedo; atmospheric precipitable water; and atmospheric turbidity. However, most of these parameters are not generally available. A "clear sky" parameter, which is dependent on air mass, surface altitude, and climate, is an alternative approach. Existing clear sky correlations are described by Erbs [5]. An evaluation should be made concerning the significance of the Garrison parameters, versus the significance of the clear sky parameter, versus improving existing correlations based only on the clearness index.

The average variance between Erbs' [5] monthly-average daily diffuse fraction correlation and data monthly-average daily diffuse fractions values is 6%. For the 24 months studied, the largest vari-

ance is 14%. However, the accuracy of monthly-average hourly diffuse fractions, I_d/I , calculated from H_d/H were not investigated. Diffuse fractions are important parameters in radiation ratio models. The evaluation of utilizability values calculated by Clark's correlation show the monthly-average hourly radiation ratio, \tilde{R} , to be the largest source of error. It is not known if the major cause of this error in \tilde{R} is from poor estimates of I_d/I , error from the isotropic diffuse radiation assumption, or both.

Hay's [8] hourly anisotropic correction factor for the isotropic radiation ratio model typically improved estimation of radiation levels on tilted surfaces. The correction factor can be defined by the hourly diffuse fraction and the hourly clearness index. Because of this simple relation, Hay's correction factor is probably valid on a monthly-average bases when used with monthly-average hourly diffuse fractions and clearness indexes. However, the accuracy of Hay's anisotropic correction factor on a monthly-average hourly basis needs to be investigated. A simple monthly-average anisotropic correction factor could be useful for calculating monthly-average hourly tilted surface radiation, as required for Clark's correlation.

Minute data clearness frequency distributions for an hourly period within a month show considerably more variability in insolation levels than the presently used long-term hourly distributions. These minute clearness frequency distributions sometimes coincide and sometimes differ from hour data clearness frequency distributions calculated from the same data base. This observation, indicates a

possible dependence of tilted solar radiation on more parameters than just the monthly-average hourly clearness index. An investigation needs to be made on the significance of long-term minute clearness frequency distributions, along with the possibility of more than one independent parameter defining both the minute and hourly distributions.

Utilizability RMS errors equal to 0.02 or less, represent a pair of approximately identical utilizability values. For surfaces receiving large amounts of beam radiation, the utilizability RMS error between minute and hour data exceeded this 0.02 value for half of the 24 months studied. Depending on the results from future investigations of the previously discussed minute clearness frequency distributions, the possibility of basing utilizability correlations on minute data should be studied. Judging from this present investigation, long-term utilizable energy estimations for south-facing surfaces could be improved up to 30%, through a correlation based on minute data and using an improved model to calculate tilted surface radiation.

APPENDIX: COMPUTER PROGRAM LISTINGS

- Appendix A: Generating Hour Tape from San Antonio, TX Minute Data
- Appendix B: Generating Hour Tape from Albany, NY Minute Data
- Appendix C: Calculating Monthly-Average Daily Radiation Ratios from Hour Data
- Appendix D: Calculating Hourly and Daily Clearness Frequency Distributions from Hour Data
- Appendix E: Calculating Minute Clearness Frequency Distributions for Hourly Periods, from Minute Data
- Appendix F: Calculating Hourly and Daily Utilizability from Hour Data
- Appendix G: Calculating Hourly and Daily Utilizability from Minute Data
- Appendix H: Calculating Hourly and Daily Utilizability from Clark's [3] Hourly Correlation

APPENDIX A

```

C  PROGRAM TO MAKE AN HOURLY DATA TAPE FROM A MINUTE-BY-MINUTE SOLAR DATA
C  TAPE, BY SUMMATION OF THE MINUTE VALUES.  OUTPUT IS IN TRUE SOLAR TIME.
C  INPUT (MINUTE TAPE) IS IN LOCAL STANDARD TIME.  DATA WITH '99' AND '13'
C  FLAGS ARE REJECTED.  AVERAGE VALUES ARE USED IN THEIR PLACE.
C      THIS VERSION IS WRITTEN SPECIFICALLY FOR THE TRINITY TAPES.
C      (*** SOLAR TIME LAGS LOCAL STANDARD TIME ***)
C      MAXIMUM NUMBER OF INSTRUMENTS = 20.
C      MAXIMUM NUMBER OF RADIATION READING INSTRUMENTS = 15.
C  NOMENCLATURE:  I = # OF WANTED INSTRUMENTS;
C                  M = # OF INSTRUMENTS TO SKIP;
C                  N = # OF DAYS IN MONTH.
C  TRACK1 IS A RUNNING TOTAL OF THE HOURS WITH 15 OR LESS GOOD DATA POINTS.
C  TRACK2 IS A RUNNING TOTAL OF THE HOURS WITH ALL OF THE DATA POINTS.
C  TRACK3 IS A RUNNING TOTAL OF THE HOURS WITH ALL BAD DATA POINTS.
C
C      DEFINE FILE 11(ANSI, FB, 567, 6237, 0)
C      DEFINE FILE 12(ANSI, FB, 243, 6075, 0)
C
C      CHARACTER*2 FLAG
C      CHARACTER*4 AINST, AIN(15)
C      CHARACTER*6 HRMN, HRM(15)
C      CHARACTER*10 RTCODE
C      INTEGER YR, DAY, HOUR, TRACK1(15), TRACK2(15), TRACK3(15)
C      INTEGER EXP(15), EX, SUM1, SUM2(15), SUM(24,15)
C      INTEGER COUNT, COUNT1, COUNT2(15), SOLART
C      DIMENSION NFLAG(24,15)
C      COMMON /COM1/MDATA(60),FLAG(60)
C      DATA SUM,TRACK1,TRACK2,TRACK3/360*0,15*0,15*0,15*0/
C      PI = 3.1415927
C      I HOUR = 0
C
C      WRITE(*,10)
C      WRITE(*,15)
C      WRITE(*,16)
10  FORMAT('0','**** SEMRTS:  TRINITY UNIVERSITY ****')
15  FORMAT(' ','PROGRAM CHECK FOR HOURLY SUMMATION OF MINUTE DATA,',
& ' WITH REVISED FLAGS AND UPDATED EXPONENTS')
16  FORMAT(' ','OUTPUT TO TAPE IS IN TRUE SOLAR TIME')
C      READ(*,20) I,M,N
20  FORMAT(I2,I2,I2)
C      WRITE(*,25) I,M,N
25  FORMAT('0','DESIRED INSTRUMENTS = ',I2,'  INSTRUMENTS TO SKIP = ',
& I2,'  DAYS IN MONTH = ',I2)
50  FORMAT(1X)
100 FORMAT(A10,A4,I2,I2,A6,I3,60(I7,A2))
110 FORMAT(A10,A4,I2,I2,A6,I3.2,60(I7,I2))
C
C  *****

```

```

C   *** START OF TAPE PROCESSING ***
C   ****
      DO 1000 DAY = 1,N
        DO 500 HOUR = 1,24
          I HOUR = I HOUR + 1
          DO 200 INST = 1,I
            READ(11,100) RTCODE,AINST,YR,MONTH,HRMN,EX,(M DATA(MIN),
            &      FLAG(MIN), MIN = 1,60)
            IF(HOUR .EQ. 1) THEN
              IF(DAY .EQ. 1) THEN
                AIN(INST) = AINST
                IF(INST .EQ. 1) CALL DAYCAL(MONTH,YDAY)
              END IF
              EXP(INST) = EX
              HRM(INST) = HRMN
C   CALCULATE THE CONVERSION FROM STANDARD TIME TO TRUE SOLAR TIME
C   4 * (STAND. MER. - LONGTITUDE) = -34 MINUTES (TRINITY UNIVERSITY)
              IF (INST .EQ. 1) THEN
                YDAY = YDAY + 1.0
                B = 2.*PI*(YDAY-81.0)/364.0
C   MINUTES SOLAR TIME LAGS STANDARD TIME (EMIN WILL BE NEGATIVE)
                EMIN = 9.87*SIN(2.*B)-7.53*ACOS(B)-1.5*SIN(B)-34.
                INDEX2 = -IFIX(EMIN)
                INDEX1 = INDEX2 - 1
                WRITE(*,111) YDAY, INDEX2, INDEX1
111      &      FORMAT(' ',YDAY = ',F5.1,' INDEX2 = ',I3,
                &      'INDEX1 = ',I3)
              END IF
              CALL SUMSUB(SUM2(INST),COUNT2(INST),AINST,HRMN,
              &      INDEX2,60)
              GO TO 200
            ELSE
              IF(AINST .NE. AIN(INST)) THEN
                WRITE(*,1005) AIN(INST),AINST,HRMN
                GO TO 2000
              END IF
              IF(EX .NE. EXP(INST)) THEN
                WRITE(*,1010) AINST,EX,EXP(INST),HRMN
                GO TO 2000
              END IF
              CALL SUMSUB(SUM1,COUNT1,AINST,HRMN,1,INDEX1)
            END IF
C   *** DO FOR ALL HOURS ***
            SOLART = HOUR - 1
            COUNT = COUNT1 + COUNT2(INST)
            SUM(SOLART,INST) = SUM1 + SUM2(INST)
            CALL CHECK(AINST,HRMN,COUNT,SUM(SOLART,INST),
            &      TRACK1(INST),TRACK2(INST),TRACK3(INST))
            NFLAG(SOLART,INST) = COUNT
            CALL SUMSUB(SUM2(INST),COUNT2(INST),AINST,HRMN,
            &      INDEX2,60)

```

```

                IF(HOUR .EQ. 24) THEN
                    SUM(HOUR,INST) = SUM2(INST)
                    COUNT = COUNT2(INST)
                    CALL CHECK(AINST,HRMN,COUNT,SUM(HOUR,INST),
&                        TRACK1(INST),TRACK2(INST),TRACK3(INST))
                    NFLAG(HOUR,INST) = COUNT
                END IF
C   *** REPEAT FOR NEXT INSTRUMENT ***
200      CONTINUE
C
C   *** SKIP OVER UNWANTED INSTRUMENTS ***
        DO 300 ISKIP = 1,M
300      READ(11,50)
C
C   *** REPEAT FOR NEXT HOUR ***
500      CONTINUE
C
C   *** OUTPUT ***
C   FORMAT: 1 RECORD = 1 DAY'S (24 HOURS) WORTH OF DATA FOR 1 INSTRUMENT.
        DO 600 INST = 1,I
            EXP(INST) = EXP(INST) + 2
            WRITE(*,1020)  RTCODE,AINST,YR,MONTH,HRM(INST),
&                        EXP(INST)
            WRITE(*,1040) (SUM(HOUR,INST),NFLAG(HOUR,INST),HOUR=1,12)
            WRITE(*,1040) (SUM(HOUR,INST),NFLAG(HOUR,INST),HOUR=13,24)
C            WRITE(12,110) RTCODE,AINST,YR,MONTH,HRM(INST),
&                        EXP(INST),(SUM(HOUR,INST),NFLAG(HOUR,INST), HOUR=1,24)
600      CONTINUE
C
C   *** REPEAT FOR FOLLOWING DAY ***
1000 CONTINUE
C
1005 FORMAT('0','MISMATCH IN INSTRUMENTS:  OLD = ',A4,'  NEW = ',A4,
&      ' DAY,HR,MN = ',A6)
1010 FORMAT('0','MISMATCH IN EXPONENTS:  INST = ',A4,
&      ' NEW EXP = ',I3.2,'  OLD EXP = ',I3.2,' DAY,HR,MN = ',A6)
1020      FORMAT(' ',A10,A4,J2,J2,A6,I3.2)
1040      FORMAT(' ',12(I7,I2))
C
C   *****
C   *** CHECK IF AT END OF TAPE ***
C   *****
        DO 1060 INST = 1,10
            READ(11,100,END=1070) RTCODE,AINST,YR,MONTH,HRMN,EX,
&            (MDATA(MIN),FLAG(MIN), MIN = 1,60)
            WRITE(*,*) 'NEXT RECORD IN FILE:'
            WRITE(*,1020) RTCODE,AINST,YR,MONTH,HRMN,EX
1060 CONTINUE
1070 CONTINUE
C
C   *****

```

```

C *** FINAL MONTHLY OUTPUT ***
C *****
  WRITE(*,1100)
1100 FORMAT('0','NUMBER OF HOURS WITH ALL BAD DATA POINTS',
  & ' (60 BAD MINUTE VALUES)')
  WRITE(*,1125)
1125 FORMAT(' ','INST  HORI  20S  30S  40S  90N  90E  90S  90W',
  & ' NIP DIFF  UV   PIR 0530 R630 R690')
  WRITE(*,1150) (TRACK3(INST),INST=1,I)
1150 FORMAT(' ','HOURS',15(I5))
  WRITE(*,1200)
1200 FORMAT('0','NUMBER OF HOURS WITH 15 OR LESS GOOD DATA POINTS')
  WRITE(*,1125)
  WRITE(*,1150) (TRACK1(INST),INST=1,I)
  WRITE(*,1400)
1400 FORMAT('0','NUMBER OF HOURS WITH ALL GOOD DATA POINTS')
  WRITE(*,1125)
  WRITE(*,1150) (TRACK2(INST),INST=1,I)
  WRITE(*,1500) I HOUR
1500 FORMAT('0','TOTAL NUMBER OF HOURS IN MONTH = ',I4)
  IDAY = I HOUR/24
  WRITE(*,1510) IDAY
1510 FORMAT(' ','TOTAL NUMBER OF DAYS IN MONTH = ',I3)
C   END OF MONTH (END OF FILE)
C   ENDFILE 12
C
2000 WRITE(*,*)
      STOP
      END

      SUBROUTINE CHECK(AINST,HRMN,COUNT,SUM,TRACK1,TRACK2,TRACK3)
C   SUBROUTINE TO MODIFY THE SUMMATION OF MINUTE DATA, ACCORDING TO THE NUMBER
C   OF BAD DATA POINTS.
C
      CHARACTER*4 AINST
      CHARACTER*6 HRMN
      INTEGER COUNT, SUM, TRACK1, TRACK2, TRACK3
C
      IF (COUNT.EQ. 0) THEN
        SUM = 999999
        TRACK3 = TRACK3 + 1
        TRACK1 = TRACK1 + 1
      ELSE IF (COUNT.LT. 15) THEN
        SUM = (SUM*60)/(COUNT*100)
        TRACK1 = TRACK1 + 1
      ELSE IF (COUNT.LT. 60) THEN
        SUM = (SUM*60)/(COUNT*100)
      ELSE IF (COUNT.EQ. 60) THEN
        SUM = SUM/100

```

```

        TRACK2 = TRACK2 + 1
    ELSE
        WRITE(*,200) COUNT, AINST, HRMN
200    FORMAT('0','ERROR IN COUNT: COUNT = ',I3,' INST = ',A4,
& ' DAY,HR,MN = ',A6)
    END IF
C
    RETURN
    END

```

```

SUBROUTINE SUMSUB(SUM,COUNT,AINST,HRMN,I1,I2)
    INTEGER COUNT,SUM
    CHARACTER*2 FLAG
    CHARACTER*4 AINST
    CHARACTER*6 HRMN
    COMMON /COM1/MDATA(60),FLAG(60)
    COUNT = 0
    SUM = 0
C
    DO 400 MIN = I1,I2
        IF(FLAG(MIN).EQ.'11' .OR. FLAG(MIN).EQ.'12') THEN
            COUNT = COUNT + 1
            SUM = SUM + MDATA(MIN)
        ELSE IF(FLAG(MIN).EQ.'99' .OR. FLAG(MIN).EQ.'13') THEN
            GO TO 400
        ELSE
            WRITE(*,600) FLAG(MIN),AINST,HRMN
            COUNT = COUNT + 1
            SUM = SUM + MDATA(MIN)
        END IF
400    CONTINUE
600    FORMAT('0','UNRECOGNIZED FLAG (',A2,'): INST = ',A4,
& ' DAY,HR,MN = ',A6)
C
    RETURN
    END

```

```

SUBROUTINE DAYCAL(MONTH,DAY)
    IF (MONTH .EQ. 1) THEN
        WRITE(*,*) 'JANUARY'
        DAY = 0.0
    ELSE IF (MONTH .EQ. 2) THEN
        WRITE(*,*) 'FEBRUARY'
        DAY = 31.0
    ELSE IF (MONTH .EQ. 3) THEN
        WRITE(*,*) 'MARCH'
        WRITE(*,*) '*** NOTE: NO DIFFUSE DATA ***'
        DAY = 59.0
    ELSE IF (MONTH .EQ. 4) THEN

```

```
        WRITE(*,*) 'APRIL'
        DAY = 90.0
    ELSE IF (MONTH .EQ. 5) THEN
        WRITE(*,*) 'MAY'
        DAY = 120.0
    ELSE IF (MONTH .EQ. 6) THEN
        WRITE(*,*) 'JUNE'
        DAY = 151.0
    ELSE IF (MONTH .EQ. 7) THEN
        WRITE(*,*) 'JULY'
        DAY = 181.0
    ELSE IF (MONTH .EQ. 8) THEN
        WRITE(*,*) 'AUGUST'
        DAY = 212.0
    ELSE IF (MONTH .EQ. 9) THEN
        WRITE(*,*) 'SEPTEMBER'
        DAY = 243.0
    ELSE IF (MONTH .EQ. 10) THEN
        WRITE(*,*) 'OCTOBER'
        DAY = 273.0
    ELSE IF (MONTH .EQ. 11) THEN
        WRITE(*,*) 'NOVEMBER'
        DAY = 304.0
    ELSE IF (MONTH .EQ. 12) THEN
        WRITE(*,*) 'DECEMBER'
        DAY = 334.0
    ELSE
        WRITE(*,50) MONTH
50      FORMAT('0','PROGRAM ERROR: MONTH = ',I3)
    END IF
C
    RETURN
END
```

APPENDIX B

```

C  PROGRAM TO MAKE AN HOURLY DATA TAPE FROM A MINUTE-BY-MINUTE SOLAR DATA
C  TAPE, BY SUMMATION OF THE MINUTE VALUES.  OUTPUT IS IN TRUE SOLAR TIME.
C  INPUT (MINUTE TAPE) IS IN LOCAL STANDARD TIME.  DATA WITH '99' AND '13'
C  FLAGS ARE REJECTED.  AVERAGE VALUES ARE USED IN THEIR PLACE.
C  TEMPERATURES (AMBIENT & DEWPOINT) ARE AVERAGED OVER THE HOUR.
C      THIS VERSION IS WRITTEN SPECIFICALLY FOR THE ALBANY SEMRTS TAPES.
C      MAXIMUM NUMBER OF INSTRUMENTS = 28.
C      NUMBER OF DESIRED INSTRUMENTS = 15.
C      COUNT OF DESIRED INSTRUMENTS = 1.
C  TRACK1 IS A RUNNING TOTAL OF THE HOURS WITH 15 OR LESS GOOD DATA POINTS.
C  TRACK2 IS A RUNNING TOTAL OF THE HOURS WITH ALL OF THE DATA POINTS.
C  TRACK3 IS A RUNNING TOTAL OF THE HOURS WITH ALL BAD DATA POINTS.
C
C      DEFINE FILE 11(ANSI, FB, 567, 6237, 0)
C      DEFINE FILE 12(ANSI, FB, 243, 6075, 0)
C
C      CHARACTER*2 FLAG
C      CHARACTER*4 AINST, AIN(28), SOURCE(15)
C      CHARACTER*6 HRMN, HRM(28,31)
C      CHARACTER*10 RTCODE
C      INTEGER YR, DAY, HOUR, TRACK1, TRACK2, TRACK3
C      INTEGER EXP(15,31), EX, SUM
C      DIMENSION EMIN(31)
C      COMMON /COM1/MDATA(24,60),FLAG(24,60)
C      COMMON /COM2/SUM(15,31,24),NFLAG(15,31,24)
C      COMMON /COM3/TRACK1(15),TRACK2(15),TRACK3(15)
C      DATA TRACK1,TRACK2,TRACK3/15*0,15*0,15*0/
C      DATA AIN/'1000','1001','1460','1560','1660','1920','1940','1960',
C      & '1980','2010','2011','2012','2013','3000','3001','3002','5000',
C      & '6000','6001','7000','7001','7002','9150','9200','9210','9300',
C      & '9320','9400'/
C
C      I = 0
C      PI = 3.141593
C 10  DIGIT STATION NUMBER, RESOLUTION & TIME CODE (ALBANY, N.Y.)
C      TRUE SOLAR TIME (TST) AVERAGED VALUE.
C      RTCODE = '3054727660'
C
C      WRITE(*,10)
C      WRITE(*,15)
C      WRITE(*,16)
C 10  FORMAT('0','**** SEMRTS:  ALBANY, NEW YORK ****')
C 15  FORMAT(' ','PROGRAM CHECK FOR HOURLY SUMMATION OF MINUTE DATA,',
C      & ' WITH REVISED FLAGS AND UPDATED EXPONENTS')
C 16  FORMAT(' ','OUTPUT TO TAPE IS IN TRUE SOLAR TIME')
C
C  READ IN DAYS IN MONTH
C      READ(*,20,ERR=35) N

```

```

20  FORMAT(I2)
   WRITE(*,22) N
22  FORMAT('0','DAYS IN MONTH = ',I2)
   GO TO 45
35  WRITE(*,40)
40  FORMAT('0','INPUT ERROR FOR DAYS IN MONTH')
   STOP
45  CONTINUE
50  FORMAT(1X)
100 FORMAT(10X,A4,I2,I2,A6,I3,60(I7,A2))
110 FORMAT(A10,A4,J2,J2,A6,I3.2,60(I7,J2))
C
C *****
C *** START OF TAPE PROCESSING ***
C *****
C NOTE: HOUR COUNTER IS ENDING HOUR OF HOUR INTERVAL (STANDARD TIME)
C       (I.E. HOUR 1-2: HOUR COUNTER = 2)
C       HOUR IN TAPE RECORD HEADER IS STARTING HOUR (STANDARD TIME)
C       HOUR IN OUTPUT TAPE RECORD HEADER WILL BE STARTING HOUR (SOLAR TIME)
DO 1000 INST = 1,28
C  SKIP UNWANTED INSTRUMENTS
      IF (INST .EQ. 2 .OR. INST .EQ. 11) GO TO 140
      IF (INST .EQ. 12 .OR. INST .EQ. 13) GO TO 140
      IF (INST .EQ. 15 .OR. INST .EQ. 18) GO TO 140
      IF (INST .EQ. 20 .OR. INST .EQ. 21) GO TO 140
      IF (INST .EQ. 22 .OR. INST .EQ. 23) GO TO 140
      IF (INST .EQ. 24 .OR. INST .EQ. 25) GO TO 140
      IF (INST .EQ. 28) GO TO 140
      GO TO 170
C
140      DO 160 DAY = 1,N
           DO 150 HOUR = 1,24
150          READ(11,50,END=1200)
160          CONTINUE
           GO TO 1000
C
C  DESIRED INSTRUMENTS
170      I = I + 1
           DO 900 DAY = 1,N
C  READ IN A DAY'S WORTH OF DATA FOR GIVEN INSTRUMENT
           DO 300 HOUR = 1,24
               READ(11,100,END=1200) AINST,YR,MONTH,HRMN,EX,
               &      (MDATA(HOUR,MIN),FLAG(HOUR,MIN), MIN = 1,60)
               IF(AINST .NE. AIN(INST)) THEN
                   WRITE(*,1005) AIN(INST),AINST,HRMN
                   STOP
               END IF
               IF(HOUR .EQ. 1) THEN
                   HRM(I,DAY) = HRMN
                   EXP(I,DAY) = EX
                   IF (DAY .EQ. 1) THEN

```



```

SOURCE(I) = AINST
IF (INST .EQ. 1) CALL DAYCAL(MONTH,YDAY)
END IF
ELSE
IF (EXP(I,DAY) .NE. EX) THEN
WRITE(*,1010) AINST,EX,EXP(I,DAY),HRMN
STOP
END IF
END IF
300 CONTINUE
C
C CONVERSION FROM STANDARD TIME TO TRUE SOLAR TIME
C 4 * (STAND. MER. - LONGITUDE) = 4.7 MINUTES (ALBANY, N.Y.)
IF (INST .EQ. 1) THEN
YDAY = YDAY + 1.0
B = 2.*PI*(YDAY - 81.0)/364.0
EMIN(DAY) = 9.87*SIN(2.*B) - 7.53*COS(B) -
& 1.5*SIN(B) + 4.7
END IF
C
IF (EMIN(DAY) .GT. -2.0 .AND. EMIN(DAY) .LT. 2.0) THEN
C SOLAR TIME EQUALS STANDARD TIME
IF (INST .EQ. 1 .AND. DAY .EQ. 1)
& WRITE(*,*) 'SOLAR TIME EQUALS STANDARD TIME'
CALL EQUAL(I,DAY,AINST)
ELSE IF (EMIN(DAY) .LE. -2.0) THEN
C SOLAR TIME LAGS STANDARD TIME
IF (INST .EQ. 1 .AND. DAY .EQ. 1)
& WRITE(*,*) 'SOLAR TIME LAGS STANDARD TIME'
CALL LAG(EMIN(DAY),I,DAY,AINST)
ELSE
C SOLAR TIME LEADS STANDARD TIME
IF (INST .EQ. 1 .AND. DAY .EQ. 1)
& WRITE(*,*) 'SOLAR TIME LEADS STANDARD TIME'
CALL LEAD(EMIN(DAY),I,DAY,AINST)
END IF
C
900 CONTINUE
1000 CONTINUE
1005 FORMAT('0','MISMATCH IN INSTRUMENTS: OLD = ',A4,' NEW = ',A4,
& ' DAY,HR,MN = ',A6)
1010 FORMAT('0','MISMATCH IN EXPONENTS: INST = ',A4,
& ' NEW EXP = ',I3.2,' OLD EXP = ',I3.2,' DAY,HR,MN = ',A6)
C
C *****
C *** CHECK IF AT END OF TAPE ***
C *****
1025 FORMAT(10X,A4,4X,A6)
1030 FORMAT(' ','NEXT RECORD IN FILE: INST = ',A4,' DAY/HR/MN = ',
& A6)
1050 FORMAT('0','PREDICTED END OF MONTH')

```

```

        WRITE(*,1050)
        DO 1060 INST = 1,10
            READ(11,1025,END=1070) AINST,HRMN
1060     WRITE(*,1030) AINST,HRMN
        STOP
1070     WRITE(*,*) 'END OF FILE DETECTED'
        GO TO 1250
C
C   PREMATURE END OF FILE
1200     WRITE(*,1205)
1205     FORMAT('0','*** END OF FILE PREMATURELY FOUND ***')
        WRITE(*,1210) DAY,INST,HOUR
1210     FORMAT(' ','DAY = ',I2,' INST = ',I2,' HOUR = ',I2)
        STOP
1250     CONTINUE
C
C   *****
C   *** OUTPUT ***
C   *****
C   FORMAT: 1 RECORD = 1 DAY'S (24 HOURS) WORTH OF DATA FOR 1 INSTRUMENT.
C   OUTPUT ONLY DESIRED INSTRUMENTS
1300     FORMAT('0',A10,A4,J2,J2,A6,I3.2)
1310     FORMAT(' ',12(I7,I2))
        DO 1600 DAY = 1,N
            DO 1500 INST = 1,I
C   UPDATE EXPONENT ON RADIATION INSTRUMENTS.
                IF (SOURCE(INST) .NE. '9300' .AND.
                    & SOURCE(INST) .NE. '9320') THEN
                    EXP(INST,DAY) = EXP(INST,DAY) + 2
                END IF
C   WRITE(*,1300) RTCODE,SOURCE(INST),YR,MONTH,HRM(INST,DAY),
C   & EXP(INST,DAY)
C   WRITE(*,1310) (SUM(INST,DAY,HOUR),NFLAG(INST,DAY,HOUR),
C   & HOUR=1,12)
C   WRITE(*,1310) (SUM(INST,DAY,HOUR),NFLAG(INST,DAY,HOUR),
C   & HOUR=13,24)
                WRITE(12,110) RTCODE,SOURCE(INST),YR,MONTH,HRM(INST,DAY),
                    & EXP(INST,DAY),(SUM(INST,DAY,HOUR),NFLAG(INST,DAY,HOUR),
                    & HOUR=1,24)
1500     CONTINUE
1600     CONTINUE
C
C   *****
C   *** FINAL MONTHLY OUTPUT ***
C   *****
        WRITE(*,1650)
1650     FORMAT('0','NUMBER OF HOURS WITH ALL BAD DATA POINTS',
        & ' (60 BAD MINUTE VALUES)')
        WRITE(*,1655)
1655     FORMAT(' ','INST HORI 33S 43S 53S 90N 90E 90S 90W',
        & ' NIP DIFF DCAL UV IR TAMB IDEW')

```

```

        WRITE(*,1660) (TRACK3(INST),INST=1,I)
1660  FORMAT(' ', 'HOURS',15(I5))
        WRITE(*,1670)
1670  FORMAT('0', 'NUMBER OF HOURS WITH 15 OR LESS GOOD DATA POINTS')
        WRITE(*,1655)
        WRITE(*,1660) (TRACK1(INST),INST=1,I)
        WRITE(*,1680)
1680  FORMAT('0', 'NUMBER OF HOURS WITH ALL GOOD DATA POINTS')
        WRITE(*,1655)
        WRITE(*,1660) (TRACK2(INST),INST=1,I)
        I HOUR = N * 24
        WRITE(*,1690) I HOUR
1690  FORMAT('0', 'TOTAL NUMBER OF HOURS IN MONTH = ',I4)
C    END OF MONTH (END OF FILE)
        ENDFILE 12
C
2000 WRITE(*,*)
        WRITE(*,*)
        STOP
        END

        SUBROUTINE CHECK(AINST,DAY,HOUR,COUNT,SUM,I)
C    SUBROUTINE TO MODIFY THE SUMMATION OF MINUTE DATA, ACCORDING TO THE NUMBER
C    OF BAD DATA POINTS.
C
        CHARACTER*4 AINST
        INTEGER COUNT,SUM,TRACK1,TRACK2,TRACK3,DAY,HOUR
        COMMON /COM3/TRACK1(15),TRACK2(15),TRACK3(15)
C
        IF (COUNT .EQ. 0) THEN
            SUM = 999999
            TRACK3(I) = TRACK3(I) + 1
            TRACK1(I) = TRACK1(I) + 1
        ELSE IF (COUNT .LT. 15) THEN
            TRACK1(I) = TRACK1(I) + 1
            IF(AINST .EQ. '9300' .OR. AINST .EQ. '9320') GO TO 300
            SUM = (SUM*60)/(COUNT*100)
        ELSE IF (COUNT .LT. 60) THEN
            IF(AINST .EQ. '9300' .OR. AINST .EQ. '9320') GO TO 300
            SUM = (SUM*60)/(COUNT*100)
        ELSE IF (COUNT .EQ. 60) THEN
            TRACK2(I) = TRACK2(I) + 1
            IF(AINST .EQ. '9300' .OR. AINST .EQ. '9320') GO TO 300
            SUM = SUM/100
        ELSE
            WRITE(*,200) COUNT,AINST,DAY,HOUR
200    FORMAT('0', 'ERROR IN COUNT: COUNT = ',I3,' INST = ',A4,
& ' DAY/HR = ',I2,'/',I2)
        END IF

```

```

      RETURN
C
C  AMBIENT OR DEWPOINT TEMPERATURE.  TAKE AVERAGE VALUE.
300  SUM = SUM/COUNT
      RETURN
      END

      SUBROUTINE SUMSUB(SUM,COUNT,AINST,DAY,I1,I2,HOUR)
      INTEGER COUNT,SUM,DAY,HOUR
      CHARACTER*2 FLAG
      CHARACTER*4 AINST
      COMMON /COM1/MDATA(24,60),FLAG(24,60)
      COUNT = 0
      SUM = 0
C
      DO 400 MIN = I1,I2
      IF(FLAG(HOUR,MIN).EQ.'11' .OR. FLAG(HOUR,MIN).EQ.'12') THEN
          COUNT = COUNT + 1
          SUM = SUM + MDATA(HOUR,MIN)
      ELSE IF(FLAG(HOUR,MIN).EQ.'99' .OR. FLAG(HOUR,MIN).EQ.'13') THEN
          GO TO 400
      ELSE
          WRITE(*,600) FLAG(HOUR,MIN),AINST,DAY,HOUR,MIN
          COUNT = COUNT + 1
          SUM = SUM + MDATA(HOUR,MIN)
      END IF
400  CONTINUE
600  FORMAT('0','UNRECOGNIZED FLAG (',A2,'):  INST = ',A4,
&      ' DAY/HR/MIN = 'I2,'/',I2,'/',I2)
C
      RETURN
      END

      SUBROUTINE DAYCAL(MONTH,DAY)
      IF (MONTH .EQ. 1) THEN
          WRITE(*,*) 'JANUARY'
          DAY = 0.0
      ELSE IF (MONTH .EQ. 2) THEN
          WRITE(*,*) 'FEBRUARY'
          DAY = 31.0
      ELSE IF (MONTH .EQ. 3) THEN
          WRITE(*,*) 'MARCH'
          DAY = 59.0
      ELSE IF (MONTH .EQ. 4) THEN
          WRITE(*,*) 'APRIL'
          DAY = 90.0
      ELSE IF (MONTH .EQ. 5) THEN
          WRITE(*,*) 'MAY'
          DAY = 120.0

```

```

ELSE IF (MONTH .EQ. 6) THEN
    WRITE(*,*) 'JUNE'
    DAY = 151.0
ELSE IF (MONTH .EQ. 7) THEN
    WRITE(*,*) 'JULY'
    DAY = 181.0
ELSE IF (MONTH .EQ. 8) THEN
    WRITE(*,*) 'AUGUST'
    DAY = 212.0
ELSE IF (MONTH .EQ. 9) THEN
    WRITE(*,*) 'SEPTEMBER'
    DAY = 243.0
ELSE IF (MONTH .EQ. 10) THEN
    WRITE(*,*) 'OCTOBER'
    DAY = 273.0
ELSE IF (MONTH .EQ. 11) THEN
    WRITE(*,*) 'NOVEMBER'
    DAY = 304.0
ELSE IF (MONTH .EQ. 12) THEN
    WRITE(*,*) 'DECEMBER'
    DAY = 334.0
ELSE
    WRITE(*,50) MONTH
50    FORMAT('0','PROGRAM ERROR: MONTH = ',I3)
END IF
C
RETURN
END

SUBROUTINE LAG(EMIN,I,DAY,AINST)
C SOLAR TIME LAGS STANDARD TIME
    INTEGER DAY,HOUR,COUNT,COUNT1,COUNT2,SUM1,SUM2,SUM,SOLART
    CHARACTER*4 AINST
    COMMON /COM2/SUM(15,31,24),NFLAG(15,31,24)
C
    INDEX2 = -IFIX(EMIN)
    INDEX1 = INDEX2 - 1
    HOUR = 1
    CALL SUMSUB(SUM2,COUNT2,AINST,DAY,INDEX2,60,HOUR)
    DO 100 HOUR = 2,24
        SOLART = HOUR - 1
        CALL SUMSUB(SUM1,COUNT1,AINST,DAY,1,INDEX1,HOUR)
        COUNT = COUNT1 + COUNT2
        SUM(I,DAY,SOLART) = SUM1 + SUM2
        CALL CHECK(AINST,DAY,HOUR,COUNT,SUM(I,DAY,SOLART),I)
        NFLAG(I,DAY,SOLART) = COUNT
        CALL SUMSUB(SUM2,COUNT2,AINST,DAY,INDEX2,60,HOUR)
100 CONTINUE
C

```

```

      SOLART = 24
      SUM(I, DAY, SOLART) = SUM2
      COUNT = COUNT2
      CALL CHECK(AINST, DAY, HOUR, COUNT, SUM(I, DAY, SOLART), I)
      NFLAG(I, DAY, SOLART) = COUNT
C
      RETURN
      END

```

```

      SUBROUTINE LEAD(EMIN, I, DAY, AINST)
C  SOLAR TIME LEADS STANDARD TIME
      INTEGER DAY, HOUR, COUNT, COUNT1, COUNT2, SUM1, SUM2, SUM
      CHARACTER*4 AINST
      COMMON /COM2/SUM(15, 31, 24), NFLAG(15, 31, 24)
C
      INDEX2 = IFIX(EMIN)
      INDEX1 = INDEX2 - 1
      SUM2 = 0.0
      COUNT2 = 0
C
      DO 100 HOUR = 1, 24
        CALL SUMSUB(SUM1, COUNT1, AINST, DAY, 1, INDEX1, HOUR)
        SUM(I, DAY, HOUR) = SUM1 + SUM2
        COUNT = COUNT1 + COUNT2
        CALL CHECK(AINST, DAY, HOUR, COUNT, SUM(I, DAY, HOUR), I)
        NFLAG(I, DAY, HOUR) = COUNT
        CALL SUMSUB(SUM2, COUNT2, AINST, DAY, INDEX2, 60, HOUR)
100  CONTINUE
C
      RETURN
      END

```

```

      SUBROUTINE EQUAL(I, DAY, AINST)
C  SOLAR TIME EQUALS STANDARD TIME
      INTEGER DAY, HOUR, COUNT, SUM1, SUM
      CHARACTER*4 AINST
      COMMON /COM2/SUM(15, 31, 24), NFLAG(15, 31, 24)
C
      DO 100 HOUR = 1, 24
        CALL SUMSUB(SUM1, COUNT, AINST, DAY, 1, 60, HOUR)
        CALL CHECK(AINST, DAY, HOUR, COUNT, SUM1, I)
        SUM(I, DAY, HOUR) = SUM1
        NFLAG(I, DAY, HOUR) = COUNT
100  CONTINUE
C
      RETURN
      END

```

APPENDIX C

C THIS PROGRAM CALCULATES THE MONTHLY AVERAGED RADIATION RATIO
 C FOR EACH GLOBAL RADIATION INSTRUMENT FROM REAL DATA. HOURLY HORIZONTAL
 C AND NIP VALUES ARE THEN USED TO NUMERICALLY INTEGRATE THE MONTHLY AVERAGED
 C RADIATION RATIOS, USING THE: 1) ISOTROPIC MODEL; 2) HAY MODEL.
 C ERBS MONTHLY-AVERAGED DIFFUSE RATIO IS ALSO USED TO CALCULATE THE RADIATION
 C RATIO, USING THE MONTHLY-AVERAGED CLEARNESS INDEX AS CALCULATED FROM THE
 C HORIZONTAL DATA.

DEFINE FILE 11(ANSI, FB, 243, 6075, 0)

C DHOOR = TOTAL NUMBER OF DAYLIGHT HOURS IN MONTH
 C TIME = TOTAL NUMBER OF HOURS IN MONTH WITH GOOD DATA (EACH INST)
 C NDAY = TOTAL NUMBER OF DAYS FOR GIVEN TIME PERIOD AND INSTRUMENT
 C WITH GOOD DATA (NDAY(HOUR,INST))
 C DKTB = MONTHLY AVERAGED DAILY CLEARNESS INDEX
 C IBAR(HOUR) = MONTHLY AVERAGED HOURLY RADIATION ON HOR. SURFACE
 C RC=PI/180=0.01745, RLAT=LATITUDE, GSC=SOLAR CONSTANT (KW/M2)
 C N = # OF DAYS IN THE MONTH, DAY= DAY OF YEAR
 C AVRAD(INST) = MONTHLY AVERAGED RADIATION FOR ALL HOURS FOR GIVEN
 C INSTRUMENT

INTEGER EXP, HOUR, INST(9), HDATA, FLAG
 REAL IBAR, AVRAD(9), NDAY, NDAY2, NDAY3, AZ(8), B(8)
 CHARACTER*4 CFLAG
 CHARACTER*5 AINST(9)
 DIMENSION HKT(21),RBAR(8),ERB(21),RBR2(8),RBR3(8)
 COMMON /COM1/HDATA(24,9),FLAG(24,9),EXP(9)
 COMMON /COM2/SETR(21),SUMI(21,9),SUMH(9),NDAY(21,9),TIME(9),
 & W2W1(21),HRBAR2(21,8),SUMH2(8),NDAY2(21,8),TIME2(8),
 & HRBAR3(21,8),SUMH3(8),NDAY3(21,8),TIME3(8)
 COMMON /COM3/PI,GSC,RC,TANLAT,SINLAT,COSLAT,COSB(8),SINB(8),
 & COSAZ(8),SINAZ(8),COS1(8),COS2(8)
 COMMON /COM4/HRBAR(21,8),RBERB(21,8),IBAR(21)

C DATA PI, RC, GSC / 3.141593, 0.01745, 1.353/
 DATA SUMH,SETR,SUMI,HKT(9*0.0,21*0.0,189*0.0,21*0.0/
 DATA NDAY,TIME,W2W1/189*0.0,9*0.0,21*0.0/
 DATA NDAY2,TIME2,NDAY3,TIME3/168*0.0,8*0.0,168*0.0,8*0.0/
 DATA AZ/4*0.0,180.0,-90.0,0.0,90.0/

C TRINITY DATA
 DATA AINST,RLAT,RHO/'HORIZ','20S','30S','40S','90N','90E',
 & '90S','90W','NIP',29.53,0.05/
 DATA B/0.0,20.0,30.0,40.0,4*90.0/

C
 20 WRITE(*,20) RLAT
 FORMAT('0','TRINITY SEMRT: HOURLY DATA',20X,'LATITUDE = ',F5.2)
 RLAT = RLAT*RC
 TANLAT = TAN(RLAT)
 SINLAT = SIN(RLAT)
 COSLAT = COS(RLAT)
 IEQUIP = 9

```

DO 50 I = 1,8
  B(I) = B(I)*RC
  AZ(I) = AZ(I)*RC
  COSB(I) = COS(B(I))
  SINB(I) = SIN(B(I))
  COSAZ(I) = COS(AZ(I))
  SINAZ(I) = SIN(AZ(I))
  COS1(I) = (1. + COSB(I))/2.
50  COS2(I) = RHO*(1. - COSB(I))/2.
  SUMHO = 0.0
  DHOURL = 0.0

C
C *****
C ***** REAL DATA PART *****
C *****
C PROCESS DATA
90  FORMAT(1X)
100 FORMAT(10X,I4,2X,I2,I2,4X,I3,24(I7,I2))
DO 1500 JDAY = 1,32
  DO 1000 I = 1,IEQUIP
    READ(11,100,END=1800) IN,MONTH,IDAY,EXP(I), (HDATA(HOUR,I),
    & FLAG(HOUR,I), HOUR=1,24)
C
    IF (JDAY .EQ. 1) THEN
      INST(I) = IN
      IF (I .EQ. 1) THEN
        CALL DAYCAL(MONTH,IDAY,DAY,N,ISKIP)
        IF (N .EQ. 0) STOP
      END IF
    ELSE
      IF (IN .NE. INST(I)) THEN
        WRITE(*,1510) INST(I), IN
        WRITE(*,*) 'ERROR OCCURED ON DAY: ',JDAY
        STOP
      END IF
    END IF
1000  CONTINUE
C
DO 1200 I = 10,ISKIP
1200  READ(11,90)
  DAY = DAY + 1.0
  CALL EXTR(DAY,CFLAG)
  IF (CFLAG .EQ. 'STOP') STOP
1500 CONTINUE
1510 FORMAT('0','MISMATCH IN INSTRUMENTS: OLD = ',I4,' NEW = ',I4)
  WRITE(*,*) '***** END OF FILE NOT FOUND *****'
  GO TO 2000
C
C END OF TAPE FOUND
1800 LDAY = JDAY - 1
  IF (N .NE. LDAY) WRITE(*,1815)

```



```

1815 FORMAT('0','*** IMPROPER MATCH IN NUMBER OF DAYS IN MONTH ***')
2000 CONTINUE
C
C *****
C *** KTBAR, RBAR CALCULATIONS ***
C *****
      DKTB = SUMH(1)*DHOURL/(SUMHO*TIME(1))
      DO 2030 HOUR = 5,20
        IBAR(HOUR) = SUMI(HOUR,1)/NDAY(HOUR,1)
        HKTB(HOUR) = IBAR(HOUR)*W2W1(HOUR)/SETR(HOUR)
2030 CONTINUE
      AVRAD(1) = SUMH(1)/TIME(1)
      DO 2080 I = 2,8
        AVRAD(I) = SUMH(I)/TIME(I)
        RBAR(I) = AVRAD(I)/AVRAD(1)
        RBAR2(I) = SUMH2(I)/(AVRAD(1)*TIME2(I))
        RBAR3(I) = SUMH3(I)/(AVRAD(1)*TIME3(I))
      DO 2060 HOUR = 5,20
        HRBAR(HOUR,I) = SUMI(HOUR,I)/(IBAR(HOUR)*NDAY(HOUR,I))
        HRBAR2(HOUR,I) = HRBAR2(HOUR,I)/(IBAR(HOUR)*NDAY2(HOUR,I))
2060      HRBAR3(HOUR,I) = HRBAR3(HOUR,I)/(IBAR(HOUR)*NDAY3(HOUR,I))
2080 CONTINUE
      GO TO 4000
C
C *****
C *** DATA OUTPUT ***
C *****
2085 WRITE(*,2090)
2090 FORMAT('0','THE FOLLOWING NUMBERS WERE GENERATED FROM REAL DATA')
      WRITE(*,2100) DKTB
2100 FORMAT(' ','MONTHLY AVERAGED DAILY CLEARNESS INDEX = ',F5.3)
      WRITE(*,*) 'DHOURL = ',DHOURL, ' TIME(1) = ',TIME(1)
      WRITE(*,2275)
2275 FORMAT('0','KTBAR & RBAR FOR LISTED INSTRUMENTS AND TIMES')
      WRITE(*,2300)
2300 FORMAT(' ','TIME 05-06 06-07 07-08 08-09 09-10 10-11 11-12 ',
& '12-13 13-14 14-15 15-16 16-17 17-18 18-19 DAILY')
      WRITE(*,2400) (HKTB(HOUR),HOUR=6,19), DKTB
2400 FORMAT(' ','KTBAR',14(2X,F4.2),3X,F4.2)
      DO 2600 I = 2,8
        WRITE(*,2500) AINST(I),(HRBAR(HOUR,I),HOUR=6,19), RBAR(I)
2500      FORMAT(' ',A5,14(2X,F4.2),3X,F4.2)
2600 CONTINUE
C
C *****
C ***** CORRELATION PART *****
C *****
2800 CALL RBCORR(DKTB,AINST,ERBHK,MONTH)
C      GO TO 4000
C
C *****

```

```

C   *** CORRELATION OUTPUT ***
C   ****
      WRITE(*,3300)
3300 FORMAT('0','THE FOLLOWING NUMBERS WERE GENERATED FROM',
      &      ' CORRELATIONS.')
      WRITE(*,*) 'THE INPUT WAS MONTHLY AVERAGED DAILY CLEARNESS INDEX',
      &      ' AS FOUND FROM THE REAL DATA'
      WRITE(*,2275)
      WRITE(*,3320)
3320 FORMAT(' ', 'TIME 05-06 06-07 07-08 08-09 09-10 10-11 11-12 ',
      &      '12-13 13-14 14-15 15-16 16-17 17-18 18-19')
      WRITE(*,3340) (ERBHKI(HOUR), HOUR=6,19)
3340 FORMAT(' ', 'KTIBAR',14(2X,F4.2))
      DO 3350 I = 2,8
3350      WRITE(*,3360) AINST(I), (RBERB(HOUR,I), HOUR=6,19)
3360 FORMAT(' ',A5,14(1X,F5.2))
C
C   DAILY RBAR OUTPUT
4000 WRITE(*,4100)
4100 FORMAT('0','MONTHLY-AVERAGED DAILY RBARS')
      WRITE(*,4120)
4120 FORMAT(' ', 'INST',3X,'DATA',2X,'ISO',3X,'HAY')
      DO 4150 I = 2,8
4150      WRITE(*,4160) AINST(I), RBAR(I), RBAR2(I), RBAR3(I)
4160 FORMAT(' ',A5,3(F6.2))
C
6000 STOP
      END

```

```

      SUBROUTINE DAYCAL(MONTH, IDAY, DAY, N, ISKIP)
      ISKIP = 15
      IF (IDAY .NE. 1) THEN
        WRITE(*,10) MONTH, IDAY
10      FORMAT('0','INITIAL DAY OF MONTH ',I2,' IS NOT DAY 1.',
      &      ' DAY = ',I2)
        N = 0
        RETURN
      END IF
      IF (MONTH .EQ. 1) THEN
        DAY = 0.0
        N = 31
        WRITE(*,*) 'JAN'
      ELSE IF (MONTH .EQ. 2) THEN
        DAY = 31.0
        N = 28
        WRITE(*,*) 'FEB'
      ELSE IF (MONTH .EQ. 3) THEN
        DAY = 59.0
        N = 31
        ISKIP = 14

```

```

        WRITE(*,*) 'MARCH'
    ELSE IF (MONTH .EQ. 4) THEN
        DAY = 90.0
        N = 30
        WRITE(*,*) 'APRIL'
    ELSE IF (MONTH .EQ. 5) THEN
        DAY = 120.0
        N = 31
        WRITE(*,*) 'MAY'
    ELSE IF (MONTH .EQ. 6) THEN
        DAY = 151.0
        N = 30
        WRITE(*,*) 'JUNE'
    ELSE IF (MONTH .EQ. 7) THEN
        DAY = 181.0
        N = 31
        WRITE(*,*) 'JULY'
    ELSE IF (MONTH .EQ. 8) THEN
        DAY = 212.0
        N = 31
        WRITE(*,*) 'AUG'
    ELSE IF (MONTH .EQ. 9) THEN
        DAY = 243.0
        N = 30
        WRITE(*,*) 'SEPT'
    ELSE IF (MONTH .EQ. 10) THEN
        DAY = 273.0
        N = 31
        WRITE(*,*) 'OCT'
    ELSE IF (MONTH .EQ. 11) THEN
        DAY = 304.0
        N = 30
        WRITE(*,*) 'NOV'
    ELSE IF (MONTH .EQ. 12) THEN
        DAY = 334.0
        N = 31
        WRITE(*,*) 'DEC'
    ELSE
        WRITE(*,50) MONTH
50      FORMAT('0','PROGRAM ERROR: (NONEXISTENT MONTH)',
&        ' MONTH = ',I3)
        N = 0
    END IF
C
100    RETURN
    END

```

```

        SUBROUTINE EXTR(DAY,CFLAG)
C    SUBROUTINE TO CALCULATE EXTRATERRESTRIAL RADIATION, AND TO ADD UP

```

```

C   THE RADIATION IN A GIVEN HOUR.
      CHARACTER*4 CFLAG
      INTEGER HOUR,EXP,HDATA,FLAG
      REAL RDATA(9),THETA(9),NDAY,NDAY2,NDAY3
      COMMON /COM1/HDATA(24,9),FLAG(24,9),EXP(9)
      COMMON /COM2/SETR(21),SUMI(21,9),SUMH(9),NDAY(21,9),TIME(9),
&   W2W1(21),HRBAR2(21,8),SUMH2(8),NDAY2(21,8),TIME2(8),
&   HRBAR3(21,8),SUMH3(8),NDAY3(21,8),TIME3(8)
      COMMON /COM3/PI,GSC,RC,TANLAT,SINLAT,COSLAT,COSB(8),SINB(8),
&   COSAZ(8),SINAZ(8),COS1(8),COS2(8)
      CFLAG = 'GO'

C
C   DECLINATION IN RADIANS
      DEC = 23.45*RC*SIN(2*PI*(284. + DAY)/365.0)
      COSDEC = COS(DEC)
      SINDEC = SIN(DEC)

C   SUNSET HOUR ANGLE IN RADIANS
      WS = ACOS(-TANLAT * TAN(DEC))
      DHOUR = DHOUR + 2.*WS/0.2618

C   DAILY EXTRATERRESTRIAL RADIATION ON HORIZ. SURFACE (KJ/M2)
      HO = 27500.0*GSC*(1.0+0.033*COS(2.*PI*DAY/365.)) *
&   (COSLAT*COSDEC*SIN(WS) + WS*SINLAT*SINDEC)
      SUMHO = SUMHO + HO

C
C   DO FOR POSSIBLE DAYLIGHT HOURS 4 TO 20
      DO 200 HOUR = 5,20
        W2 = FLOAT(HOUR)
        W1 = W2 - 1.0

C   CONVERSION TO HOUR ANGLES IN +/- RADIANS
        W2 = (W2-12.0) * 0.2618
        W1 = (W1-12.0) * 0.2618

C   CHECK WITH SUNSET HOUR ANGLE
        IF (W2 .LT. -WS) GO TO 200
        IF (W1 .GT. WS) GO TO 200

C   IF GETTING DARK
        IF (W2 .GE. WS) W2 = WS

C   IF GETTING LIGHT
        IF (W1 .LE. -WS) W1 = -WS
        W = (W1 + W2)/2.

C
C   HOURLY EXTRATERRESTRIAL RADIATION (KJ/M2)
      ETRR = 13750.*GSC*(1.0+0.033*COS(2.*PI*DAY/365.))
      ETRL = COSLAT*COS(DEC)*(SIN(W2)-SIN(W1)) +
&   (W2-W1)*SINLAT*SIN(DEC)
      ETR = ETRR * ETRL
      SETR(HOUR) = SETR(HOUR) + ETR
      W2W1(HOUR) = W2W1(HOUR) + (W2 - W1)/0.2618
      THEZ = COSDEC*COSLAT*COS(W) + SINDEC*SINLAT
      IF (THEZ .LT. 1.0E-06) THEZ = 0.0
      DO 100 I = 1,9
        RDATA(I) = 0.0

```

```

      IF (FLAG(HOUR,I) .EQ. 0) GO TO 200
      IF (HDATA(HOUR,I) .LE. 0) GO TO 200
      RDATA(I) = (FLOAT(HDATA(HOUR,I))) * 10.**EXP(I)
      TIME(I) = TIME(I) + 1.
      NDAY(HOUR,I) = NDAY(HOUR,I) + 1.
      SUMI(HOUR,I) = SUMI(HOUR,I) + RDATA(I)
      SUMH(I) = SUMH(I) + RDATA(I)
      P = SINDEC*(SINLAT*COSEB(I) - COSLAT*SINB(I)*COSAZ(I))
      Q = COSDEC*COS(W)*(COSLAT*COSEB(I) + SINLAT*SINB(I)*COSAZ(I))
      S = COSDEC*SINB(I)*SINAZ(I)*SIN(W)
      THETA(I) = P + Q + S
      IF (THETA(I) .LT. 1.0E-04) THETA(I) = 0.0
100    CONTINUE
C
C    CALCULATE NUMERATORS FOR RBARS
      IF( RDATA(1) .EQ. 0.0 .OR. RDATA(9) .EQ. 0.0) GO TO 200
      RTHEZ = RDATA(9)*THEZ
      DO 150 I = 2,8
C    ISOTROPIC MODEL (HRBAR2)
      RISO = (RDATA(1)-RTHEZ)*COS1(I) + RDATA(9)*THETA(I) +
&          RDATA(1)*COS2(I)
      IF (RISO .LT. 0.0) THEN
        WRITE(*,*) 'ERROR: RISO = ',RISO
        WRITE(*,*) 'I = ',I,' HOUR = ',HOUR
        CFLAG = 'STOP'
      END IF
      HRBAR2(HOUR,I) = HRBAR2(HOUR,I) + RISO
      SUMH2(I) = SUMH2(I) + RISO
      NDAY2(HOUR,I) = NDAY2(HOUR,I) + 1.
      TIME2(I) = TIME2(I) + 1.
C    HAY MODEL (HRBAR3)
      HAY = ((RDATA(1)-RTHEZ)*COS1(I) + RDATA(9)*THETA(I))*
&          (1.-RTHEZ/ETR) + RDATA(1)*COS2(I)
      IF (HAY .LT. 0.0) THEN
        WRITE(*,*) 'ERROR: HAY = ',HAY
        WRITE(*,*) 'I = ',I,' HOUR = ',HOUR
        CFLAG = 'STOP'
      END IF
      HRBAR3(HOUR,I) = HRBAR3(HOUR,I) + HAY
      SUMH3(I) = SUMH3(I) + HAY
      NDAY3(HOUR,I) = NDAY3(HOUR,I) + 1.
      TIME3(I) = TIME3(I) + 1.
150    CONTINUE
200    CONTINUE
C
      RETURN
      END

```

SUBROUTINE RBCORR(DKTB,AINST,HKTB,MONTH)

C THIS SUBROUTINE CALCULATES RBARS FROM CORRELATIONS.

```

C  RBERB = DIFFUSE + BEAM + GROUND REFLECTANCE (RBAR WITH ERBS CORR. INPUT)
C  NOTE: RANGE OF ERBS NONSEASONAL HD/H CORRELATION IS FOR  $0.3 < KT < 0.8$ 
C    B(INST) = SLOPE,  AZ(INST) = AZIMUTH ANGLE
C  AVDAY(MONTH) = AVE. DAY FOR MONTH IN YEAR
    CHARACTER*5 AINST(9)
    INTEGER HOUR
    REAL IDI, IBAR
    DIMENSION AVDEC(12), HKTB(21), AVDAY(12)
    COMMON /COM3/PI,GSC,RC,TANLAT,SINLAT,COSLAT,COSB(8),SINB(8),
&  COSAZ(8),SINAZ(8),COS1(8),COS2(8)
    COMMON /COM4/HRBAR(21,8),RBERB(21,8),IBAR(21)
    DATA AVDEC/-20.9,-13.0,-2.4,9.4,18.8,23.1,21.2,13.5,2.2,-9.6,
&  -18.9,-23.0/
    DATA AVDAY/17.,47.,75.,105.,135.,162.,198.,228.,258.,288.,
&  318.,344./
    DATA RBERB/168*0.0/
    RHO = 0.05

C
    WRITE(*,100)
100  FORMAT('0','TRINITY SERMRT:  ERBS RBAR CORRELATION')
    WRITE(*,110) RHO
110  FORMAT(' ','GROUND REFLECTANCE = ',F4.2)
C
C  *** CALCULATE CONSTANTS ***
    DECL = AVDEC(MONTH) * RC
C  (SUNSET HOUR ANGLE IN DEGREES)
    WS = ACOS(-TANLAT*TAN(DECL))/RC
    INST = 8
    COSDEC = COS(DECL)
    SINDEC = SIN(DECL)
    GON = GSC*(1.+0.033*COS(2.*PI*AVDAY(MONTH)/365.))
C  CONSTANTS FOR RT (EQ. 2.13.1)
    RTA = 0.409 + 0.5016*SIN((WS-60)*RC)
    RTB = 0.6609 - 0.4767*SIN((WS-60)*RC)
C  CONVERT SUNSET HOUR ANGLE BACK TO RADIANS
    WS = WS * RC
C  HD/H:  FROM ERBS NONSEASONAL CORRELATION (EQ. 4.23)
    HDH = 1.317 + (-3.023 + (3.373 - 1.760*DKTB)*DKTB) * DKTB
    IF (HDH .GT. 1.0) THEN
        HDH = 1.0
        WRITE(*,*) 'HDH > 1.0'
    END IF
C  FROM ERBS RBAR PROGRAM:
    IF (DKTB .GT. 0.8) HDH = 0.156
C
    DO 2000 HOUR=6,19
C  CHECK IF ALL OF HOUR IS DARK
    WBEG = (FLOAT(HOUR) - 1.0 - 12.0) * 0.2618
    WEND = (FLOAT(HOUR) - 12.0) * 0.2618
    IF (WBEG .GE. WS) GO TO 2000
    IF (WEND .LE. -WS) GO TO 2000

```

```

C   USE MIDDLE OF HOUR FOR ACTUAL CALCULATION (IN RADIANS)
      W = (FLOAT(HOUR) - 0.5 - 12.0) * 0.2618
      IF (W .LT. -WS) THEN
        IF ((WEND+WS) .LT. 0.01) GO TO 2000
        IF ((WEND+WS) .LT. 0.05) THEN
          W = WEND
        ELSE
          W = (-WS + WEND)/2.
        END IF
      END IF
      IF (W .GT. WS) THEN
        IF ((WS-WBEG) .LT. 0.01) GO TO 2000
        IF ((WS-WBEG) .LT. 0.05) THEN
          W = WBEG
        ELSE
          W = (WS + WBEG)/2.
        END IF
      END IF
      RDRT = 1/(RTA + RTBACOS(W))
      HKTB(HOUR) = DKTB/RDRT
C   ID/I = (RD/RT)(HD/H)
      IDI = HDH*RDRT
      IF (IDI .LE. 0.0) THEN
        WRITE(*,*) 'HOUR = ', HOUR, '    IDI = ', IDI
        IDI = 0.0
      END IF
      IF (IDI .GE. 1.0) THEN
        WRITE(*,*) 'HOUR = ', HOUR, '    IDI = ', IDI
        IDI = 1.0
      END IF
      THEZ = COSDEC*COSLAT*COS(W) + SINDEC*SINLAT
      IF (THEZ .LT. 1.0E-06) THEN
C   BEAM COMPONENT, RB(HOUR,I) = 0.0
        THEZ = 0.0
        DO 300 I = 2, INST
          300   RBERB(HOUR,I) = IDI*COS1(I) + COS2(I)
          GO TO 2000
        END IF
      END IF
C
      DO 1000 I = 2, INST
        P = SINDEC*(SINLAT*COSB(I) - COSLAT*SINB(I)*COSAZ(I))
        Q = COSDEC*COS(W)*(COSLAT*COSB(I) + SINLAT*SINB(I)*COSAZ(I))
        S = COSDEC*SINB(I)*SINAZ(I)*SIN(W)
        THETA = P + Q + S
        IF (THETA .LT. 1.0E-04) THETA = 0.0
        RB = THETA/THEZ
        RBERB(HOUR,I) = IDI*COS1(I) + (1-IDI)*RB + COS2(I)
        IF (RBERB(HOUR,I) .LT. 0.0) THEN
          RBERB(HOUR,I) = 0.0
          WRITE(*,2100) AINST(I), HOUR
          WRITE(*,*) 'IDI = ', IDI, '    COS2(I) = ', COS2(I)
        END IF
      END DO

```

```
        END IF
1000 CONTINUE
C
2000 CONTINUE
2100 FORMAT('0','RBAR WAS < 0 FOR INST ',A5,', HOUR ',I2)
C
      WS = WS/0.2618
      WRITE(*,*) 'WS (HOURS AFTER NOON) = ',WS
      RETURN
      END
```


APPENDIX D

```

C THIS PROGRAM CALCULATES THE FREQUENCY DISTRIBUTION OF HOURLY & DAILY
C CLEARNESS INDEXES FOR A GIVEN MONTH.
C COMPLETE HOURS ONLY FOR DAILY CLEARNESS INDEX.
C N = NUMBER OF GOOD DATA POINTS
C
C   DEFINE FILE 11(ANSI, FB, 243, 6075, 0)
C
C   INTEGER DESHR(6), HOUR, TDAY, EXP, HDATA(24), FLAG(24), N(6), I HOUR(6)
C   REAL KT(6,31), KTPLOT(6,31), FRAC(6,31), DKT(31), DKPLOT(31),
C   &   DFRAC(31), SUMRAD(6), SUMEXT(6), HKTB(6), DUMKT(31)
C   COMMON /COM1/EX1, EX2(6), EX3(6), PI2, DECL, TANLAT, COSLAT, SINLAT, HEX
C DESIRED ENDING HOURS
C   DATA DESHR/10,11,12,13,14,15/
C   DATA KTPLOT, SUMRAD, SUMEXT, N/186*0.0, 6*0.0, 6*0.0, 6*0.0/
C   DATA SUMH, SUMHO, SUMDH, SUMDL/0.0, 0.0, 0.0, 0.0/
C LATITUDE FOR TRINITY UNIVERSITY
C   RLAT = 29.53
C LATITUDE FOR ALBANY N.Y.
C   RLAT = 42.70
C   CALL CONST(DESHR, RLAT)
C
C *****
C *** READ IN DATA & CALCULATE KT'S. DO FOR EACH DAY. ***
C *****
C DAY = DAY IN YEAR, TDAY = DAY ON TAPE, MDAY = DAY OF MONTH
C NDAY = DAYS IN MONTH
C   WRITE(*,50)
C 50  FORMAT('0','ALBANY, NY')
C   50  FORMAT('0','TRINITY UNIVERSITY')
C   DO 200 MDAY = 1,32
C READ IN GLOBAL HORIZONTAL RADIATION
C   READ(11,250,END=290) INST, MO, TDAY, EXP, (HDATA(HOUR),
C   &   FLAG(HOUR), HOUR = 1,24)
C   IF (MDAY .EQ. 1) THEN
C     INCHK = INST
C     CALL DAYCAL(MO, TDAY, DAY, ISKIP, NDAY)
C   ELSE
C     DAY = DAY + 1.0
C     IF (INST .NE. INCHK) THEN
C       WRITE(*,260) MDAY, INST
C       STOP
C     END IF
C   END IF
C
C   H = 0.0
C   DHOURS = 0.0
C DECLINATION (IN RADIAN), SUNSET HOUR ANGLE (IN RADIAN)
C   DEC = DECLASIN(PI2*(284.0 + DAY))

```

```

        WS = ACOS(-TANLAT * TAN(DEC))
C   DAY LENGTH IN HOURS
        DAYLGT = 2.*WS/0.2618
        SUMDL = SUMDL + DAYLGT
C   CHECK FLAG TO SEE IF DESIRED DATA IS GOOD
        DO 100 HOUR = 5,20
            W2 = (FLOAT(HOUR) - 12.0) * 0.2618
            W1 = (FLOAT(HOUR) - 1.0 - 12.0) * 0.2618
C   SKIP EARLY MORNING & LATE EVENING PART HOURS
            IF (W1 .LT. -WS) GO TO 100
            IF (W2 .GT. WS) GO TO 100
            IF (FLAG(HOUR) .NE. 0 .AND. HDATA(HOUR) .GT. 0) THEN
                DHOURS = DHOURS + 1.0
                SUMDH = SUMDH + 1.0
                RAD = (FLOAT(HDATA(HOUR))) * 10.0**EXP
                H = H + RAD
                SUMH = SUMH + RAD
C   CHECK IF HOUR IS DESIRED HOUR
                DO 75 I = 1,6
                    IF (HOUR .EQ. DESHR(I)) THEN
                        N(I) = N(I) + 1
                        SUMRAD(I) = SUMRAD(I) + RAD
                        EXTR = EX1*(1.0 + 0.033*ACOS(PI2*DAY)) *
&                            (EX2(I)*COS(DEC) + EX3(I)*SIN(DEC))
                        SUMEXT(I) = SUMEXT(I) + EXTR
                        N1 = N(I)
                        KT(I,N1) = RAD/EXTR
                        GO TO 100
                    END IF
75                CONTINUE
                END IF
100            CONTINUE
C
            HEXTR = HEX*(1.+0.033*ACOS(PI2*DAY))*(COSLAT*COS(DEC)*SIN(WS) +
&                WS*SINLAT*SIN(DEC))
            SUMHO = SUMHO + HEXTR
            DKT(MDAY) = H*DAYLGT/(DHOURS*HEXTR)
C
C   SKIP OVER UNWANTED INSTRUMENTS
        DO 190 JUMP = 2,ISKIP
190            READ(11,255)
C
C   REPEAT FOR FOLLOWING DAY
200        CONTINUE
C
250        FORMAT(10X,I4,2X,I2,I2,4X,I3,24(I7,I2))
255        FORMAT(1X)
260        FORMAT('0','READING TAPE IN WRONG SPOT: DAY = ',I2,
&                ' INST = ',I4)
        WRITE(*,*) 'END OF FILE NOT FOUND'
        STOP

```

```

C   CHECK IF LAST DAY
290   LDAY = MDAY - 1
      IF (LDAY .NE. NDAY) WRITE(*,295) LDAY,NDAY
295   FORMAT(' ', 'ERROR: LAST DAY = ', I2, ' DAYS IN MONTH = ', I2)
C
C   *****
C   *** CALCULATE KT & CUMULATIVE FREQUENCIES ***
C   *****
C   DO FOR HOUR KT
      DO 400 I = 1,6
        J = N(I)
        DO 350 M = 1,J
350      DUMKT(M) = KT(I,M)
        CALL FREQ(DUMKT,J,KTPLT,FRAC)
        DO 375 M = 1,J
375      KT(I,M) = DUMKT(M)
        N(I) = J
C   MONTHLY AVERAGED HOURLY CLEARNESS INDEX
      HKTB(I) = SUMRAD(I)/SUMEXT(I)
      IHOURL(I) = DESHR(I) - 1
400   CONTINUE
C
C   DO FOR DAILY KT
      CALL FREQ(DKT,LDAY,DKPLOT,DFRAC)
C   MONTHLY AVERAGED DAILY CLEARNESS INDEX
      DKTB = SUMH*SUMDL/(SUMHO*SUMDH)
C
C   *****
C   *** FINAL OUTPUT ***
C   *****
      WRITE(*,1020) (IHOURL(I),DESHR(I), I = 1,6)
1020  FORMAT('0', 'HOURL: ', 6(6X, I2, '- ', I2))
      WRITE(*,1025) (HKTB(I), I = 1,6)
1025  FORMAT(' ', 'KTBAR: ', 4X, 6(F5.3, 11X))
      WRITE(*,1030)
1030  FORMAT(' ', 6(7X, 'KT', 6X, 'FRAC'))
      DO 1050 M = 1,31
1050  WRITE(*,1100) (KTPLT(I,M),FRAC(I,M), I = 1,6)
1100  FORMAT(' ', 6X, 6(6X, F5.3, 4X, F5.2))
C   DAILY OUTPUT
      WRITE(*,2000) DKTB
2000  FORMAT('0', 'MONTHLY AVERAGED DAILY CLEARNESS INDEX = ', F5.3)
      WRITE(*,1030)
      DO 2100 M = 1,LDAY
2100  WRITE(*,1100) DKPLOT(M), DFRAC(M)
C
      WRITE(*,*)
      STOP
      END

```

```

      SUBROUTINE CONST(DESHR, RLAT)
C   SUBROUTINE TO CALCULATE CONSTANTS FOR THE DECLINATION FUNCTION AND THE
C   EXTRATERRESTRIAL RADIATION FUNCTION.
      INTEGER DESHR(6)
      COMMON /COM1/EX1,EX2(6),EX3(6),PI2,DECL,TANLAT,COSLAT,SINLAT,HEX
C   RC=PI/180=0.01745, RLAT=LATITUDE, GSC = SOLAR CONSTANT (KW/M2)
      DATA PI,RC,GSC/3.141593,0.01745,1.353/
      RLAT = RLAT * RC
      TANLAT = TAN(RLAT)
      COSLAT = COS(RLAT)
      SINLAT = SIN(RLAT)
C   DECLINATION CONSTANTS
      DECL = 23.45*RC
C   EXTRATERRESTRIAL RADIATION CONSTANTS
      PI2 = 2. * PI/365.
      EX1 = 13750. * GSC
      HEX = 27500.0 * GSC
C
      DO 200 I = 1,6
C   HOUR ANGLES IN +/- RADIANS
      W2 = (FLOAT(DESHR(I)) - 12.0)*0.2618
      W1 = (FLOAT(DESHR(I)) - 13.0)*0.2618
      EX2(I) = COS(RLAT)*(SIN(W2) - SIN(W1))
      EX3(I) = (W2 - W1)*SIN(RLAT)
200  CONTINUE
C
      RETURN
      END

      SUBROUTINE DAYCAL(MONTH, IDAY, DAY,ISKIP,N)
C   SUBROUTINE TO DETERMINE MONTH OF YEAR, AND INITIAL DAY IN YEAR
      ISKIP = 15
      IF (IDAY .NE. 1) THEN
        WRITE(*,10) MONTH, IDAY
10      FORMAT('0','INITIAL DAY OF MONTH ',I2,' IS NOT DAY 1.',
        & ' DAY = ',I2)
        GO TO 60
      END IF
      IF (MONTH .EQ. 1) THEN
        DAY = FLOAT(IDAY)
        N = 31
        WRITE(*,*) 'JAN'
      ELSE IF (MONTH .EQ. 2) THEN
        DAY = FLOAT(31 + IDAY)
C      N = 29
        N = 28
        WRITE(*,*) 'FEB'
      ELSE IF (MONTH .EQ. 3) THEN
        ISKIP = 14
        DAY = FLOAT(59 + IDAY)

```

```

      N = 31
      WRITE(*,*) 'MARCH'
    ELSE IF (MONTH .EQ. 4) THEN
      DAY = FLOAT(90 + IDAY)
      N = 30
      WRITE(*,*) 'APRIL'
    ELSE IF (MONTH .EQ. 5) THEN
      DAY = FLOAT(120 + IDAY)
      N = 31
      WRITE(*,*) 'MAY'
    ELSE IF (MONTH .EQ. 6) THEN
      DAY = FLOAT(151 + IDAY)
      N = 30
      WRITE(*,*) 'JUNE'
    ELSE IF (MONTH .EQ. 7) THEN
      DAY = FLOAT(181 + IDAY)
      N = 31
      WRITE(*,*) 'JULY'
    ELSE IF (MONTH .EQ. 8) THEN
      DAY = FLOAT(212 + IDAY)
      N = 31
      WRITE(*,*) 'AUG'
    ELSE IF (MONTH .EQ. 9) THEN
      DAY = FLOAT(243 + IDAY)
      N = 30
      WRITE(*,*) 'SEPT'
    ELSE IF (MONTH .EQ. 10) THEN
      DAY = FLOAT(273 + IDAY)
      N = 31
      WRITE(*,*) 'OCT'
    ELSE IF (MONTH .EQ. 11) THEN
      DAY = FLOAT(304 + IDAY)
      N = 30
      WRITE(*,*) 'NOV'
    ELSE IF (MONTH .EQ. 12) THEN
      DAY = FLOAT(334 + IDAY)
      N = 31
      WRITE(*,*) 'DEC'
    ELSE
      WRITE(*,50) MONTH
50      FORMAT('0','PROGRAM ERROR: (NONEXISTENT MONTH)',
&        ' MONTH = ',I3)
      N = 0
    END IF
C
60    RETURN
    END

```

SUBROUTINE FREQ(KT,J,KIPLT,FRAC)

```

C  SUBROUTINE TO FIND THE FREQUENCY DISTRIBUTION OF A SET OF DATA
      REAL KT(31),KTPLOT(31),FRAC(31)
C
C  ROUND OFF KT VALUES TO 3 DECIMAL PLACES
      DO 400 M = 1,J
          ITEM = IFIX((KT(M) + 0.0005)*1000)
400    KT(M) = FLOAT(ITEM)/1000.0
C  SORT KT IN INCREASING ORDER
      CALL SELECT (KT,J)
C  ACTUAL FREQUENCY CALCULATION
      J1 = 0
      DEN = FLOAT(J-1)
      DO 500 I = 1,J
          IF (I .LT. J) THEN
              IF (KT(I) .LT. KT(I+1)) THEN
                  J1 = J1 + 1
                  FRAC(J1) = FLOAT(I-1)/DEN
                  KTPLOT(J1) = KT(I)
              END IF
          ELSE
              J1 = J1 + 1
              FRAC(J1) = 1.0
              KTPLOT(J1) = KT(J)
          END IF
500    CONTINUE
      J = J1
      RETURN
      END

      SUBROUTINE SELECT(DATA,N)
C  THIS SUBROUTINE SORTS REAL NUMBERS BY THE SELECTION SORTING METHOD.
C  NUMBERS ARE ORDERED IN INCREASING VALUE.
C
      INTEGER PRESNT, SMALL, SEARCH
      DIMENSION DATA(N)
C
      J = N - 1
      DO 1000 PRESNT = 1,J
          SMALL = PRESNT
          K = PRESNT + 1
          DO 500 SEARCH = K,N
              IF (DATA(SEARCH) .LT. DATA(SMALL)) SMALL = SEARCH
500    CONTINUE
          IF (SMALL .NE. PRESNT) THEN
              TEMP = DATA(PRESNT)
              DATA(PRESNT) = DATA(SMALL)
              DATA(SMALL) = TEMP
          END IF
1000  CONTINUE
C

```

RETURN
END

APPENDIX E

```

C  PROGRAM TO CALCULATE THE MINUTE CLEARNESS FREQUENCY DISTRIBUTION.
C  OUTPUT IS IN TRUE SOLAR TIME.
C  DATA WITH '99' AND '13' FLAGS ARE REJECTED.
C  THIS VERSION IS WRITTEN SPECIFICALLY FOR THE ALBANY SEMRTS TAPES.
C
C      DEFINE FILE 11(ANSI, FB, 567, 6237, 0)
C
C      CHARACTER*2 FLAG
C      CHARACTER*6 HRMN
C      INTEGER DAY, HOUR, EX
C      REAL KT,KTBIN(51),EMIN(31)
C      COMMON /COM1/MDATA(14,60),FLAG(14,60),KT(1860),FRAC(51)
C      COMMON /COM2/PI2,EX1,EX2,EX3,COSDEC,SINDEC,SUMRAD,SUMEXT
C  RC = PI/180 =0.01745, RLAT = LATITUDE
C      DATA PI,RC,GSC/3.141593,0.01745,1.353/
C  ALBANY DATA: LATITUDE & 4*(STAND. MER. - LONG)
C      DATA RLAT,ECON/42.70,4.7/
C  TRINITY DATA: LATITUDE & 4*(STAND. MER. - LONG)
C      DATA RLAT,ECON/29.53,-34.0/
C      RLAT = RLAT*RC
C      SINLAT = SIN(RLAT)
C      COSLAT = COS(RLAT)
C  NUMBER OF CLEARNESS INDEXES FROM MINUTE DATA
C      K = 0
C      SUMRAD = 0.0
C      SUMEXT = 0.0
C  HOUR ANGLES IN RADIANS (W2 = HOUR 13, W1 = HOUR 12)
C      W2 = 0.2618
C      W1 = 0.0
C  EXTRATERRESTRIAL CONSTANTS
C      DECL = 23.45*RC
C      PI2 = 2.*PI/365.
C      EX1 = 229.2*GSC
C      EX2 = COSLAT*(SIN(W2) - SIN(W1))
C      EX3 = (W2 - W1)*SINLAT
C
C      WRITE(*,10)
C 10  FORMAT('0','***** SEMRTS:  ALBANY NEW YORK *****')
C 10  FORMAT('0','***** SEMTRS:  TRINITY UNIVERSITY *****')
C
C  READ IN DAYS IN MONTH
C      READ(*,20,ERR=35) N
C 20  FORMAT(I2)
C      WRITE(*,22) N
C 22  FORMAT(' ', 'DAYS IN MONTH = ', I2)
C      GO TO 45
C 35  WRITE(*,40)
C 40  FORMAT('0','INPUT ERROR FOR DAYS IN MONTH')

```



```

        STOP
45  CONTINUE
50  FORMAT(1X)
100 FORMAT(10X,A4,2X,I2,A6,I3,60(17,A2))
C
C *****
C *** START OF TAPE PROCESSING ***
C *****
C NOTE: HOUR COUNTER IS ENDING HOUR OF HOUR INTERVAL (STANDARD TIME)
C       (I.E. HOUR 1-2: HOUR COUNTER = 2)
C       HOUR IN TAPE RECORD HEADER IS STARTING HOUR (STANDARD TIME)
C       DO 1000 DAY = 1,N
C           DO 200 HOUR = 1,11
200      READ(11,50)
C  READ IN A DAY'S WORTH OF DATA FOR GIVEN INSTRUMENT
C       DO 300 HOUR = 1,14
C           READ(11,100) INST,MONTH,HRMN,EX,
C           &      (MDATA(HOUR,MIN),FLAG(HOUR,MIN), MIN = 1,60)
C           IF(HOUR.EQ. 4) THEN
C               IN = INST
C               IF (DAY.EQ. 1) CALL DAYCAL(MONTH,YDAY,ISKIP)
C           ELSE
C               IF (IN.NE. INST) THEN
C                   WRITE(*,1005) IN,INST,HRMN
C                   STOP
C               END IF
C           END IF
300      CONTINUE
C
C  CONVERSION FROM STANDARD TIME TO TRUE SOLAR TIME
C       YDAY = YDAY + 1.0
C       DEC = DECL*SIN(PI2*(284. + YDAY))
C       COSDEC = COS(DEC)
C       SINDEC = SIN(DEC)
C       B = 2.*PI*(YDAY - 81.0)/364.0
C       EMIN(DAY) = 9.87*SIN(2.*B) - 7.53*COS(B) - 1.5*SIN(B) + ECON
C
C       IF (EMIN(DAY) .GT. -2.0 .AND. EMIN(DAY) .LT. 2.0) THEN
C  SOLAR TIME EQUALS STANDARD TIME
C       CALL PHISUB(13,1,60,EX,YDAY,K)
C       ELSE IF (EMIN(DAY) .LE. -2.0) THEN
C  SOLAR TIME LAGS STANDARD TIME
C       INDEX2 = -IFIX(EMIN(DAY))
C       INDEX1 = INDEX2 - 1
C       CALL PHISUB(13,INDEX2,60,EX,YDAY,K)
C       CALL PHISUB(14,1,INDEX1,EX,YDAY,K)
C       ELSE
C  SOLAR TIME LEADS STANDARD TIME
C       INDEX2 = IFIX(EMIN(DAY))
C       INDEX1 = INDEX2 - 1
C       CALL PHISUB(12,INDEX2,60,EX,YDAY,K)

```

```

                CALL PHISUB(13,1,INDEX1,EX,YDAY,K)
            END IF
C
            DO 950 HOUR = 15,24
950             READ(11,50)
C
C     FOR TRINITY MINUTE TAPES, SKIP OTHER INSTRUMENTS
C         DO 970 I = 2,ISKIP
C             DO 960 HOUR = 1,24
C960             READ(11,50)
970             CONTINUE
C
C     REPEAT FOR NEXT DAY
1000    CONTINUE
1005    FORMAT('0','MISMATCH IN INSTRUMENTS: OLD = ',I4,' NEW = ',I4,
            & ' DAY,HR,MN = ',A6)
C
C     PUT CLEARNESS INDEXES INTO BINS FOR PLOTTING
            CALL BIN(K)
C
C     *****
C     *** OUTPUT ***
C     *****
            HKT = SUMRAD/SUMEXT
            WRITE(*,2010) HKT
2010    FORMAT(' ', 'M.A. HOURLY INDEX (HOUR: 12-13) = ',F5.3)
            WRITE(*,2020)
2020    FORMAT(' ', ' KT',5X,'FRACTION')
            DO 2100 J = 1,50
                KTBIN(J) = FLOAT(J)*0.02 - 0.01
2100    WRITE(*,2120) KTBIN(J),FRAC(J)
2120    FORMAT(' ',F5.3,4X,F5.2)
C
            WRITE(*,*)
            STOP
            END

        SUBROUTINE PHISUB(HOUR,I1,I2,EX,DAY,K)
C     SUBROUTINE TO CALCULATE CLEARNESS INDEX
        REAL KT
        INTEGER HOUR,EX
        CHARACTER*2 FLAG
        COMMON /COM1/MDATA(14,60),FLAG(14,60),KT(1860),FRAC(51)
        COMMON /COM2/PI2,EX1,EX2,EX3,COSDEC,SINDEC,SUMRAD,SUMEXT
C
        DO 400 MIN = I1,I2
            IF(MDATA(HOUR,MIN) .LE. 0) GO TO 400
            IF(FLAG(HOUR,MIN).EQ.'99' .OR. FLAG(HOUR,MIN).EQ.'13') GO TO 400
            IF(FLAG(HOUR,MIN).EQ.'11' .OR. FLAG(HOUR,MIN).EQ.'12') THEN

```

```

        RDATA = (FLOAT(MDATA(HOUR,MIN))) * 10.0**EX
        K = K + 1
        EXTR = EX1*(1.0 + 0.033*COS(PI2*DAY)) *
&          (EX2*COSDEC + EX3*SINDEC)
        KT(K) = RDATA/EXTR
        SUMRAD = SUMRAD + RDATA
        SUMEXT = SUMEXT + EXTR
    ELSE
        WRITE(*,600) FLAG(HOUR,MIN),HOUR,MIN
    END IF
400 CONTINUE
600 FORMAT('0','UNRECOGNIZED FLAG (',A2,'):  HR/MIN = ',I2,'/',I2)
C
    RETURN
    END

    SUBROUTINE DAYCAL(MONTH,DAY,ISKIP)
C  SUBROUTINE TO CALCULATE THE MONTH & CRITICAL LEVELS FOR INSTRUMENTS
    CHARACTER*2 FLAG
    ISKIP = 15
C
    IF (MONTH .EQ. 1) THEN
        WRITE(*,*) 'JANUARY'
        DAY = 0.0
    ELSE IF (MONTH .EQ. 2) THEN
        WRITE(*,*) 'FEBRUARY'
        DAY = 31.0
    ELSE IF (MONTH .EQ. 3) THEN
        WRITE(*,*) 'MARCH'
        DAY = 59.0
C
        ISKIP = 14
    ELSE IF (MONTH .EQ. 4) THEN
        WRITE(*,*) 'APRIL'
        DAY = 90.0
    ELSE IF (MONTH .EQ. 5) THEN
        WRITE(*,*) 'MAY'
        DAY = 120.0
    ELSE IF (MONTH .EQ. 6) THEN
        WRITE(*,*) 'JUNE'
        DAY = 151.0
    ELSE IF (MONTH .EQ. 7) THEN
        WRITE(*,*) 'JULY'
        DAY = 181.0
    ELSE IF (MONTH .EQ. 8) THEN
        WRITE(*,*) 'AUGUST'
        DAY = 212.0
    ELSE IF (MONTH .EQ. 9) THEN
        WRITE(*,*) 'SEPTEMBER'
        DAY = 243.0
    ELSE IF (MONTH .EQ. 10) THEN

```

```

        WRITE(*,*) 'OCTOBER'
        DAY = 273.0
    ELSE IF (MONTH .EQ. 11) THEN
        WRITE(*,*) 'NOVEMBER'
        DAY = 304.0
    ELSE IF (MONTH .EQ. 12) THEN
        WRITE(*,*) 'DECEMBER'
        DAY = 334.0
    ELSE
        WRITE(*,50) MONTH
50      FORMAT('0','PROGRAM ERROR: MONTH = ',I3)
    END IF
C
    RETURN
    END

    SUBROUTINE BIN(K)
C   SUBROUTINE TO PUT THE CLEARNESS INDEXES INTO BINS, AND TO CALCULATE THE
C   APPROPRIATE CUMULATIVE FREQUENCY.
    REAL KT, CHECK(51)
    COMMON /COM1/MDATA(14,60),FLAG(14,60),KT(1860),FRAC(51)
    TFRAC = 0.0
C
C   SET BIN BOUNDARIES (0.0 TO 1.0 IN 0.02 INCREMENTS)
    DO 100 J = 1,51
100      CHECK(J) = FLOAT(J - 1)*0.02
C
C   FIND BIN FOR EACH CLEARNESS INDEX
    DO 500 I = 1,K
        DO 400 J = 1,50
            J1 = J + 1
            IF (KT(I) .GE. CHECK(J) .AND. KT(I) .LT. CHECK(J1)) THEN
                DO 300 J2 = J,50
                    FRAC(J2) = FRAC(J2) + 1.0
300              TFRAC = TFRAC + 1.0
            END IF
400          CONTINUE
500        CONTINUE
C
C   CALCULATE THE ACTUAL CUMULATIVE FRACTION FOR EACH BIN
    DO 600 J = 1,50
600      FRAC(J) = FRAC(J)/TFRAC
C
    RETURN
    END

```

APPENDIX F

```

C PROGRAM TO CALCULATE HOURLY AND DAILY UTILIZABILITY FROM EITHER SAN
C ANTONIO OR ALBANY HOUR DATA.
C   DEFINE FILE 11(ANSI, FB, 243, 6075, 0)
C
C TIME = TOTAL NUMBER OF HOURS IN MONTH WITH GOOD DATA (EACH INST)
C NDAY = TOTAL NUMBER OF DAYS FOR GIVEN TIME PERIOD AND INSTRUMENT
C   WITH GOOD DATA (NDAY(TIME,INST))
C N = # OF DAYS IN THE MONTH, DAY= DAY OF YEAR
C IC = I-CRITICAL (KJ/M2-HR)
C HPHI(HOUR,INST,IC) = HOURLY UTILIZABILITY
C DPHI(INST,IC) = DAILY UTILIZABILITY
C ARAD(HOUR,INST) = MONTHLY AVERAGED HOURLY RADIATION (KN/M2)
C SLOPE(HOUR,INST) = INITIAL SLOPE OF UTILIZABILITY CURVE (DPHI/DXC)
C RC=PI/180=0.01745, RLAT=LATITUDE, GSC=SOLAR CONSTANT (KW/M2)
C
C   REAL IC, NDAY
C   INTEGER HDATA(24,15), EXP(15), HOUR, FLAG(24,15)
C   CHARACTER*5 AINST(15)
C   DIMENSION INST(15),HKT(21),HRBAR(21,15),RBAR(15),NDAY(21,15),
C &   ARAD(20,15),SLOPE(20,15),SETR(21),SUMI(21,15),SUMH(15)
C   COMMON /COM1/ HPHI(21,8,11), DPHI(8,11), IC(8,11)
C   COMMON /COM2/PI,RLAT,GSC,RC,TIME(15),TANLAT,SINLAT,COSLAT
C
C   DATA PI,RC,GSC,HRBAR / 3.141593,0.01745,1.353,315*0.0/
C   DATA SUMH,SETR,SUMI,HKT / 15*0.0,21*0.0,315*0.0,21*0.0/
C   DATA HPHI,DPHI,NDAY,TIME/1848*0.0,88*0.0,315*0.0,15*0.0/
C TRINITY DATA
C   DATA AINST,RLAT/'HORIZ','20S','30S','40S','90N','90E','90S',
C & '90W','NIP','DIFF','UV-EP','FIR','06530','RG630','RG690',29.53/
C ALBANY DATA
C   DATA AINST,RLAT/'HORIZ','33S','43S','53S','90N','90E','90S',
C & '90W','NIP','DIF-D','DIF-C','UV','IR','AMB','DEW',42.70/
C
C   WRITE(*,5) RLAT
C 5   FORMAT('0','TRINITY SEMRT:  HOURLY DATA',20X,'LATITUDE = ',F5.2)
C 5   FORMAT('0','ALBANY NY:  HOURLY SEMRT DATA',15X,'LATITUDE = ',F5.2)
C   RLAT = RLAT*RC
C   TANLAT = TAN(RLAT)
C   SINLAT = SIN(RLAT)
C   COSLAT = COS(RLAT)
C   IEQUIP = 8
C   I2 = IEQUIP + 1
C   SUMHO = 0.0
C 10  FORMAT(1X)
C 100 FORMAT(10X,I4,2X,I2,I2,4X,I3,24(I7,I2))
C 110 FORMAT('0','MISMATCH IN INST:  OLD = ',I4,'   NEW = ',I4)
C
C *****

```

```

C   *** READ IN THE DATA FOR THE DAY ***
C   ****
DO 2000 JDAY = 1,32
DO 1000 I = 1,IEQUIP
    READ(11,100,END=2002) IN,MO,IDAY,EXP(I),(HDATA(HOUR,I),
&    FLAG(HOUR,I),HOUR=1,24)
    IF (JDAY .EQ. 1) THEN
        INST(I) = IN
        IF (I .EQ. 1) THEN
            CALL DAYCAL(MONTH,IDAY,DAY,N,ISKIP)
            IF (N .EQ. 0) STOP
        END IF
    END IF
    IF (IN .NE. INST(I)) THEN
        WRITE(*,*) 'JDAY = ',JDAY
        WRITE(*,110) INST(I),IN
        STOP
    END IF
    IF (I .EQ. 1) THEN
        DAY = DAY + 1.0
        DEC = 23.45*ARC*SIN(2*PI*(284. + DAY)/365.0)
        WS = ACOS(-TANLAT*TAN(DEC))
    END IF
1000    CONTINUE
C
C   SKIP UNWANTED INSTRUMENTS
DO 1050 I = I2,ISKIP
1050    READ(11,10)
C
C   *** CALCULATIONS ***
DO 1900 HOUR = 5,20
C   CALCULATE HOUR ANGLES (IN RADIANS)
    W2 = (FLOAT(HOUR)-12.0)*0.2618
    W1 = (FLOAT(HOUR)-13.0)*0.2618
C   CHECK IF BEFORE SUNRISE OR AFTER SUNSET
    IF (W2 .LT. -WS) GO TO 1900
    IF (W1 .GT. WS) GO TO 1900
C   CHECK FOR PARTIAL HOUR
    IF (W1 .LT. -WS) W1 = -WS
    IF (W2 .GT. WS) W2 = WS
C   CHECK FOR VALID DATA
DO 1500 I = 1,IEQUIP
    IF (FLAG(HOUR,I) .EQ. 0) GO TO 1900
    IF (HDATA(HOUR,I) .LE. 0) GO TO 1900
    RDATA = (FLOAT(HDATA(HOUR,I))) * 10.**EXP(I)
    IF (I .EQ. 1) THEN
C   HOURLY EXTRATERRESTRIAL RADIATION (KJ/M2)
        ETRR = 13750.*GSC*(1.0+0.033*ACOS(2.*PI*DAY/365.))
        ETRL = COSLAT*COS(DEC)*(SIN(W2)-SIN(W1)) +
&        (W2-W1)*SINLAT*SIN(DEC)
        ETR = ETRR * ETRL

```

```

        SETR(HOUR) = SETR(HOUR) + ETR
        SUMHO = SUMHO + ETR
    END IF
    SUMI(HOUR,I) = SUMI(HOUR,I) + RDATA
    NDAY(HOUR,I) = NDAY(HOUR,I) + 1.
    SUMH(I) = SUMH(I) + RDATA
    TIME(I) = TIME(I) + 1.
    DO 1400 J = 1,11
        IF (RDATA .GT. IC(I,J)) THEN
            HPHI(HOUR,I,J) = HPHI(HOUR,I,J) + RDATA - IC(I,J)
            DPHI(I,J) = DPHI(I,J) + RDATA - IC(I,J)
        END IF
1400    CONTINUE
C   REPEAT FOR NEXT INSTRUMENT
1500    CONTINUE
C   REPEAT FOR NEXT HOUR
1900    CONTINUE
C   REPEAT FOR NEXT DAY
2000 CONTINUE
        WRITE(*,*) 'END OF FILE NOT FOUND'
        STOP
C
C   *** END OF TAPE ***
2002 LAST = JDAY - 1
        IF (LAST .NE. N) THEN
            WRITE(*,*) 'ERROR IN NUMBER OF DAYS'
            WRITE(*,2005) N,LAST
            STOP
        END IF
2005 FORMAT(' ', 'DAYS IN MONTH = ',I2,'   LAST DAY READ = ',I2)
C
C   *****
C   *** KTBAR, RBAR & PHIBAR CALCULATIONS ***
C   *****
2010 DKTB = SUMH(1)/SUMHO
        DO 2015 J = 1,11
2015    DPHI(1,J) = DPHI(1,J)/SUMH(1)
            DO 2030 HOUR = 5,20
                HKTB(HOUR) = SUMI(HOUR,1)/SETR(HOUR)
                IF (HKTB(HOUR) .GT. 1.0) HKTB(HOUR) = 1.0
                ARAD(HOUR,1) = SUMI(HOUR,1)/NDAY(HOUR,1)
                DO 2020 J = 1,11
2020    HPHI(HOUR,1,J) = HPHI(HOUR,1,J)/SUMI(HOUR,1)
                    SLOPE(HOUR,1) = -(HPHI(HOUR,1,1)-HPHI(HOUR,1,2))*
                    & ARAD(HOUR,1)/IC(1,2)
2030 CONTINUE
                DO 2080 I = 2,IEQUIP
                    RBAR(I) = SUMH(I)*TIME(1)/(SUMH(1)*TIME(I))
                    DO 2040 J = 1,11
2040    DPHI(I,J) = DPHI(I,J)/SUMH(I)
                        DO 2060 HOUR = 5,20

```

```

      HRBAR(HOUR,I) = SUMI(HOUR,I)*NDAY(HOUR,I)/
&      (SUMI(HOUR,I)*NDAY(HOUR,I))
      ARAD(HOUR,I) = SUMI(HOUR,I)/NDAY(HOUR,I)
      DO 2050 J = 1,11
2050      HPHI(HOUR,I,J) = HPHI(HOUR,I,J)/SUMI(HOUR,I)
      SLOPE(HOUR,I) = -(HPHI(HOUR,I,1)-HPHI(HOUR,I,2))*
&      ARAD(HOUR,I)/IC(I,2)
2060      CONTINUE
2080 CONTINUE
C   CONVERT IC(I,J) FROM KJ/M2-HR TO W/M2 FOR OUTPUT
      DO 2095 I = 1,IEQUIP
        DO 2090 J = 1,11
2090      IC(I,J) = IC(I,J)/3.6
2095 CONTINUE
      GO TO 4000

C
C   *****
C   *** OUTPUT TYPE A:  RBAR, DAILY & HOURLY PHI ***
C   *****
2100 WRITE(*,2150) SUMH(1), SUMHO, DKTB
2150 FORMAT('0','SUMH(1) = ',F10.1,' SUMHO = ',F10.1,' DKTB = ',F5.3)
      WRITE(*,2275)
2275 FORMAT('0','KTBAR & RBARS FOR LISTED INSTRUMENTS AND TIMES')
2280 WRITE(*,2300)
C 2300 FORMAT(' ', 'TIME  04-05 05-06 06-07 07-08 08-09 09-10 10-11 ',
C      & '11-12 12-13 13-14 14-15 15-16 16-17 17-18 18-19 19-20')
2300 FORMAT(' ', 'TIME  05-06 06-07 07-08 08-09 09-10 10-11 11-12 ',
      & '12-13 13-14 14-15 15-16 16-17 17-18 18-19  DAILY')
      WRITE(*,2400) (HKT(BAR),HOUR=6,19), DKT(B)
2400 FORMAT(' ', 'KTBAR',14(2X,F4.2),3X,F4.2)
      DO 2500 I = 2,IEQUIP
C2500      WRITE(*,2600) AINST(I), (HRBAR(HOUR,I),HOUR=6,19), RBAR(I)
2500      WRITE(*,2600) AINST(I), (HRBAR(HOUR,I),HOUR=5,20)
C2600 FORMAT(' ',A5,14(2X,F4.2),3X,F4.2)
2600 FORMAT(' ',A5,16(1X,F5.2))
2610 DO 2700 I = 1,IEQUIP
      WRITE(*,2800) AINST(I)
      WRITE(*,2300)
      DO 2650 J = 1,11
2650      WRITE(*,2900) IC(I,J), (HPHI(HOUR,I,J),HOUR=6,19), DPHI(I,J)
      WRITE(*,2910) (SLOPE(HOUR,I), HOUR=6,19)
2700 CONTINUE
2800 FORMAT('0','UTILIZABILITY FOR LISTED CRITICAL LEVEL (W/M2)',
      & ' AND TIME',15X,'INSTRUMENT ',A5)
2900      FORMAT(' ',F5.1,14(2X,F4.2),3X,F4.2)
2910 FORMAT(' ', 'SLOPE',14(F6.2))
      WRITE(*,*)
      STOP

C
C   *****
C   ***** OUTPUT TYPE B:  DAILY PHI ONLY *****

```



```

C *****
4000 WRITE(*,*) 'DAILY UTILIZABILITY'
      WRITE(*,4010) AINST(1),AINST(3),AINST(7),AINST(5),AINST(8)
4010 FORMAT(' ', 'IC1(W/M2)',5(3X,A5))
      DO 4050 J = 1,11
4050   WRITE(*,4060) IC(1,J),DPHI(1,J),DPHI(3,J),DPHI(7,J),DPHI(5,J),
      &      DPHI(8,J)
4060 FORMAT(' ',F7.1,2X,5(2X,F6.3))
      WRITE(*,*)
      STOP

C
C *****
C ***** OUTPUT TYPE C:  HOURLY PHI ONLY *****
C *****
5000 HOUR = 13
      LHOURL = HOUR - 1
      WRITE(*,5010) LHOURL,HOUR
5010 FORMAT(' ', 'HOURLY UTILIZABILITY:  HOUR ',I2,'-',I2)
      WRITE(*,4010) AINST(1),AINST(3),AINST(7),AINST(5),AINST(8)
      DO 5050 J = 1,11
5050   WRITE(*,4060) IC(1,J),HPHI(HOUR,1,J),HPHI(HOUR,3,J),
      &      HPHI(HOUR,7,J),HPHI(HOUR,5,J),HPHI(HOUR,8,J)
      WRITE(*,*)
      STOP

C
      END

      SUBROUTINE DAYCAL(MONTH, IDAY, DAY, N, ISKIP)
C SUBROUTINE TO CALCULATE MONTH & CRITICAL LEVELS FOR INSTRUMENTS.
      REAL IC,KMAX,DECL(12),B(8),AZ(8),DKT(12)
      COMMON /COM1/ HPHI(21,8,11), DPHI(8,11), IC(8,11)
      COMMON /COM2/PI,RLAT,GSC,RC,TIME(15),TANLAT,SINLAT,COSLAT
      DATA DECL/-20.9,-13.0,-2.4,9.4,18.8,23.1,21.2,13.5,2.2,-9.6,
      &      -18.9,-23.0/
      DATA AZ/4*0.0,180.0,-90.0,0.0,90.0/
C TRINITY DATA
      DATA B/0.0,20.0,30.0,40.0,4*90.0/
      DATA DKT,CONST/0.463,0.406,0.390,0.376,0.488,0.475,0.557,0.540,
      &      0.577,0.452,0.533,0.443,0.8/
C ALBANY DATA
C DATA B/0.0,33.0,43.0,53.0,4*90.0/
C DATA DKT,CONST/0.461,0.353,0.423,0.428,0.546,0.487,0.459,0.453,
C &      0.517,0.408,0.372,0.406,0.7/
C
      ISKIP = 15
      IF (IDAY .NE. 1) THEN
        WRITE(*,10) MONTH, IDAY
10      FORMAT('0','INITIAL DAY OF MONTH ',I2,' IS NOT DAY 1.',
      &      ' DAY = ',I2)
      N = 0

```

```

        RETURN
    END IF
    IF (MONTH .EQ. 1) THEN
        DAY = 0.0
        N = 31
        WRITE(*,*) 'JAN'
    ELSE IF (MONTH .EQ. 2) THEN
        DAY = 31.0
        N = 28
C   ALBANY DATA INCLUDES LEAP YEAR
C       N = 29
        WRITE(*,*) 'FEB'
    ELSE IF (MONTH .EQ. 3) THEN
        DAY = 59.0
        N = 31
C   TRINITY DATA LACKED DIFFUSE DATA FOR MARCH
        ISKIP = 14
        WRITE(*,*) 'MARCH'
    ELSE IF (MONTH .EQ. 4) THEN
        DAY = 90.0
        N = 30
        WRITE(*,*) 'APRIL'
    ELSE IF (MONTH .EQ. 5) THEN
        DAY = 120.0
        N = 31
        WRITE(*,*) 'MAY'
    ELSE IF (MONTH .EQ. 6) THEN
        DAY = 151.0
        N = 30
        WRITE(*,*) 'JUNE'
    ELSE IF (MONTH .EQ. 7) THEN
        DAY = 181.0
        N = 31
        WRITE(*,*) 'JULY'
    ELSE IF (MONTH .EQ. 8) THEN
        DAY = 212.0
        N = 31
        WRITE(*,*) 'AUG'
    ELSE IF (MONTH .EQ. 9) THEN
        DAY = 243.0
        N = 30
        WRITE(*,*) 'SEPT'
    ELSE IF (MONTH .EQ. 10) THEN
        DAY = 273.0
        N = 31
        WRITE(*,*) 'OCT'
    ELSE IF (MONTH .EQ. 11) THEN
        DAY = 304.0
        N = 30
        WRITE(*,*) 'NOV'
    ELSE IF (MONTH .EQ. 12) THEN

```

```

        DAY = 334.0
        N = 31
        WRITE(*,*) 'DEC'
    ELSE
        WRITE(*,50) MONTH
50      FORMAT('0','PROGRAM ERROR:  MONTH = ',I3)
        N = 0
        RETURN
    END IF

C
C  CRITICAL LEVELS (CALCULATE NOON IRRADIATION TO FIND)
    SINDEC = SIN(RC*DECL(MONTH))
    COSDEC = COS(RC*DECL(MONTH))
    KMAX = 0.208 + DKT(MONTH)*(2.77 + DKT(MONTH)*(-4.75 + 2.92*
&    DKT(MONTH)))
    DO 200 I = 1,8
        COSB = COS(B(I)*RC)
        SINB = SIN(B(I)*RC)
        COSAZ = COS(AZ(I)*RC)
        THETA = SINDEC*(SINLAT*COSB - COSLAT*SINB*COSAZ) +
&        COSDEC*(COSLAT*COSB + SINLAT*SINB*COSAZ)
C  CHECK IF SUN IS BEHIND SURFACE AT NOON
        IF (THETA .LT. 0.3) THEN
            IF (I .EQ. 6 .OR. I .EQ. 8) THEN
C  EAST & WEST SURFACES
                THETA = CONST*DKT(MONTH)
            ELSE IF (I .EQ. 5) THEN
C  NORTH SURFACE
                THETA = 0.3*DKT(MONTH)
            ELSE
C  SOUTH SURFACE, SUN HIGH ABOVE TILT
                THETA = 0.3
            END IF
        END IF
        RMAX = 495.0*THETA*KMAX
        DO 100 J = 1,11
100      IC(I,J) = FLOAT(J - 1)*RMAX
200    CONTINUE
C
    RETURN
END

```

APPENDIX G

```

C  PROGRAM TO CALCULATE DAILY AND HOURLY UTILIZABILITY FROM MINUTE DATA.
C  OUTPUT IS IN TRUE SOLAR TIME.
C  LATITUDE IS FOR TRINITY UNIVERSITY.
C      IC = I-CRITICAL (KJ/M2-MIN)
C      HPHI(HOUR,INST,IC) = HOURLY UTILIZABILITY
C      DPHI(INST,IC) = DAILY UTILIZABILITY
C      SUMI(HOUR,INST) = HOURLY RADIATION TOTAL
C      SUMH(INST) = DAILY RADIATION TOTAL
C      IEQUIP = # OF WANTED INSTRUMENTS
C      ISKIP = # OF INSTRUMENTS TO SKIP
C      N = DAYS IN MONTH
C
C      DEFINE FILE 11(ANSI, FB, 567, 6237, 0)
C      REAL IC
C      INTEGER EX, HOUR, FLAG, SOLART, HRMN
C      CHARACTER*5 AINST(15)
C      DIMENSION IN(15)
C      COMMON /COM1/ HPHI(21,8,11), DPHI(8,11)
C      COMMON /COM2/ SUMI(21,15),SUMH(15),IC(8,11),RC,RLAT,PI
C      COMMON /COM3/ MDATA(60), FLAG(60)
C  RC=PI/180=0.01745, RLAT=LATITUDE
C      DATA RC, RLAT, PI / 0.01745, 29.53, 3.1415927/
C      DATA SUMH, SUMI / 15*0.0, 315*0.0 /
C      DATA HPHI,DPHI / 1848*0.0, 88*0.0 /
C      DATA AINST/'HORIZ',' 20S ',' 30S ',' 40S ',' 90N ',
C      & ' 90E ',' 90S ',' 90W ',' NIP ',' DIFF','UV-EP',
C      & ' PIR ','OG530','RG630','RG690'/
C
C      READ(*,25) IEQUIP,ISKIP,N
C 25  FORMAT(I2,I2,I2)
C      IBEGIN = 6
C      ISTART = IBEGIN - 1
C      ISTOP = 21
C      ITOTAL = IEQUIP + ISKIP
C      IJUMP1 = ITOTAL * 4
C      IJUMP2 = ITOTAL * 3
C
C      WRITE(*,50) RLAT
C 50  FORMAT('0','TRINITY SEMRT: MINUTE DATA',20X,'LATITUDE = ',F5.2)
C      WRITE(*,*) 'OUTPUT IS IN TRUE SOLAR TIME'
C      WRITE(*,60) IEQUIP, ISKIP, N
C 60  FORMAT(' ','DESIRED INSTRUMENTS = ',I2,' INSTRUMENTS TO SKIP = ',
C      & I2,' DAYS IN MONTH = ',I2)
C      RLAT = RLAT*RC
C 75  FORMAT(1X)
C 100 FORMAT(10X,I4,2X,I2,I6,I3,60(I7,I2))
C 120 FORMAT('0','MISMATCH IN INSTRUMENTS: OLD = ',I4,
C      & ' NEW = ',I4)

```

```

150  FORMAT('0','DAY = ',I2)
C
C  *****
C  *** START OF TAPE PROCESSING ***
C  *****
      DO 1700 JDAY = 1,N
C  *** SKIP PRE-DAWN HOURS, ALL INSTRUMENTS ***
      DO 200 J = 1,IJUMP1
200    READ(11,75)
C  *** HOURS 5 THROUGH 21, ALL DESIRED INSTRUMENTS ***
      DO 1500 HOUR = ISTART,ISTOP
      DO 1300 I = 1,IEQUIP
      READ(11,100) INST,MO,HRMN,EX,(MDATA(MIN),
&      FLAG(MIN),MIN=1,60)
      IF(HOUR .EQ. ISTART) THEN
      IF(JDAY .EQ. 1) THEN
      IN(I) = INST
      IF(I .EQ. 1) THEN
      CALL DAYCAL(MO,INDEX1,INDEX2)
      IF (MO .EQ. 0) STOP
      END IF
      END IF
      ELSE
      IF(INST .NE. IN(I)) THEN
      WRITE(*,120) IN(I), INST
      STOP
      END IF
      SOLART = HOUR - 1
C  SUM SECTION1 FOR SOLAR HOUR SOLART
      CALL PHI(I,SOLART,AINST(I),1,INDEX1,HRMN,EX)
      END IF
C  SUM SECTION2 FOR FOLLOWING SOLAR HOUR
      CALL PHI(I,HOUR,AINST(I),INDEX2,60,HRMN,EX)
C
C  *** REPEAT FOR NEXT INSTRUMENT ***
1300    CONTINUE
C
C  SKIP UNWANTED INSTRUMENTS
      DO 1400 J = 1,ISKIP
1400    READ(11,75)
C  *** REPEAT FOR NEXT HOUR ***
1500    CONTINUE
C
C  *** SKIP NIGHT HOURS, ALL INSTRUMENTS ***
      DO 1600 J = 1,IJUMP2
1600    READ(11,75)
C  *** REPEAT FOR NEXT DAY ***
1700    CONTINUE
C
C  *****
C  *** CHECK IF AT END OF TAPE ***

```

```

C *****
  DO 1740 I = 1,5
    READ(11,100,END=1780) INST,MO,HRMN,EX,(MDATA(MIN),FLAG(MIN),
    &      MIN = 1,60)
    WRITE(*,*) 'NEXT RECORD IN FILE:'
    WRITE(*,*) 'INST = ',INST,' DAY/HR/MN = ',HRMN
1740 CONTINUE
    GO TO 1790
1780 WRITE(*,*) ' END OF FILE DETECTED'
1790 CONTINUE
C
C *****
C *** PHIBAR CALCULATIONS ***
C *****
  DO 2000 I = 1,IEQUIP
    DO 1900 J = 1,11
      DPHI(I,J) = DPHI(I,J)/SUMH(I)
      DO 1800 HOUR = IBEGIN,ISTOP
1800        HPHI(HOUR,I,J) = HPHI(HOUR,I,J)/SUMI(HOUR,I)
1900      CONTINUE
2000 CONTINUE
C  CONVERT IC(I,J) BACK TO W/M2 FOR OUTPUT
  DO 2055 I = 1,IEQUIP
    DO 2050 J = 1,11
2050      IC(I,J) = IC(I,J) * 16.66667
2055 CONTINUE
    GO TO 4000
C
C *****
C *** OUTPUT TYPE A: DAILY & HOURLY PHI ***
C *****
2100 DO 2300 I = 1,IEQUIP
  WRITE(*,2400) AINST(I)
  WRITE(*,2500)
  DO 2200 J = 1,11
2200    WRITE(*,2800) IC(I,J),(HPHI(HOUR,I,J),HOUR=6,19),
    &      DPHI(I,J)
2300 CONTINUE
2400 FORMAT('0','UTILIZABILITY FOR LISTED CRITICAL LEVEL (W/M2)',
    & ' AND TIME',15X,'INSTRUMENT ',A5)
2500 FORMAT(' ','ICRT 05-06 06-07 07-08 08-09 09-10 10-11 11-12',
    & '12-13 13-14 14-15 15-16 16-17 17-18 18-19 DAILY')
2800 FORMAT(' ',F5.1,14(2X,F4.2),3X,F4.2)
  WRITE(*,*)
  STOP
C
C *****
C *** OUTPUT TYPE B: DAILY PHI ONLY ***
C *****
4000 WRITE(*,*) 'DAILY UTILIZABILITY'
  WRITE(*,4010) AINST(1),AINST(3),AINST(7),AINST(5),AINST(8)

```

```

4010 FORMAT(' ', 'IC1(W/M2)', 5(3X, A5))
      DO 4050 J = 1, 11
4050   WRITE(*, 4060) IC(1, J), DPHI(1, J), DPHI(3, J), DPHI(7, J), DPHI(5, J),
      &      DPHI(8, J)
4060   FORMAT(' ', F7.1, 2X, 5(2X, F6.3))
      WRITE(*, *)
C      STOP
C
C *****
C *** OUTPUT TYPE C: HOURLY PHI ONLY ***
C *****
5000   HOUR = 13
      LHOURL = HOUR - 1
      WRITE(*, 5010) LHOURL, HOUR
5010   FORMAT(' ', 'HOURLY UTILIZABILITY: HOUR ', I2, '-', I2)
      WRITE(*, 4010) AINST(1), AINST(3), AINST(7), AINST(5), AINST(8)
      DO 5050 J = 1, 11
5050   WRITE(*, 4060) IC(1, J), HPHI(HOUR, 1, J), HPHI(HOUR, 3, J),
      &      HPHI(HOUR, 7, J), HPHI(HOUR, 5, J), HPHI(HOUR, 8, J)
      WRITE(*, *)
      STOP
C
      END

      SUBROUTINE DAYCAL(MONTH, INDEX1, INDEX2)
C      SUBROUTINE TO CALCULATE THE MONTH, EQUATION OF TIME INDEXES, &
C      CRITICAL LEVELS FOR EACH INSTRUMENT.
      REAL IC, KMAX, DECL(12), BE(8), AZ(8), DKT(12)
      COMMON /COM2/SUMI(21, 15), SUMH(15), IC(8, 11), RC, RLAT, PI
      DATA DECL/-20.9, -13.0, -2.4, 9.4, 18.8, 23.1, 21.2, 13.5, 2.2, -9.6,
      &      -18.9, -23.0/
      DATA BE/0.0, 20.0, 30.0, 40.0, 4A90.0/
      DATA AZ/4A0.0, 180.0, -90.0, 0.0, 90.0/
      DATA DKT/0.463, 0.406, 0.390, 0.376, 0.488, 0.475, 0.557, 0.540,
      &      0.577, 0.452, 0.533, 0.443/
C
      IF (MONTH .EQ. 1) THEN
        WRITE(*, *) 'JAN'
        DAY = 1.0
      ELSE IF (MONTH .EQ. 2) THEN
        WRITE(*, *) 'FEB'
        DAY = 32.0
      ELSE IF (MONTH .EQ. 3) THEN
        WRITE(*, *) 'MARCH'
        DAY = 60.0
      ELSE IF (MONTH .EQ. 4) THEN
        WRITE(*, *) 'APRIL'
        DAY = 91.0
      ELSE IF (MONTH .EQ. 5) THEN
        WRITE(*, *) 'MAY'

```

```

        DAY = 121.0
    ELSE IF (MONTH .EQ. 6) THEN
        WRITE(*,*) 'JUNE'
        DAY = 152.0
    ELSE IF (MONTH .EQ. 7) THEN
        WRITE(*,*) 'JULY'
        DAY = 182.0
    ELSE IF (MONTH .EQ. 8) THEN
        WRITE(*,*) 'AUG'
        DAY = 213.0
    ELSE IF (MONTH .EQ. 9) THEN
        WRITE(*,*) 'SEPT'
        DAY = 244.0
    ELSE IF (MONTH .EQ. 10) THEN
        WRITE(*,*) 'OCT'
        DAY = 274.0
    ELSE IF (MONTH .EQ. 11) THEN
        WRITE(*,*) 'NOV'
        DAY = 305.0
    ELSE IF (MONTH .EQ. 12) THEN
        WRITE(*,*) 'DEC'
        DAY = 335.0
    ELSE
        WRITE(*,50) MONTH
50      FORMAT('0','PROGRAM ERROR: (NONEXISTENT MONTH)',
      &      ' MONTH = ',I3)
        MONTH = 0
        RETURN
    END IF

C
C  CALCULATE THE CONVERSION FROM STANDARD TIME TO TRUE SOLAR TIME
C  4 * (STAND. MER. - LONGITUDE) = -34 MINUTES (TRINITY UNIVERSITY)
    B = 2.*PI*(DAY-81.0)/364.0
C  MINUTES SOLAR TIME LAGS STANDARD TIME (EMIN WILL BE NEGATIVE)
    EMIN = 9.87*SIN(2*B) - 7.53*COS(B) - 1.5*SIN(B) - 34.0
C  INDEXES TO CONTROL THE PHASE SHIFT FROM LOCAL TO SOLAR TIME
    INDEX2 = -IFIX(EMIN)
    INDEX1 = INDEX2 - 1
    WRITE(*,55) INDEX1, INDEX2
55  FORMAT('0','INDEXES TO SHIFT FROM LOCAL TO SOLAR TIME:  I1 = ',
      &  I2,' I2 = ',I2)
C
C  CALCULATE CRITICAL LEVELS (FIND NOON IRRADIATION)
    SINDEC = SIN(RC*DECL(MONTH))
    COSDEC = COS(RC*DECL(MONTH))
    SINLAT = SIN(RLAT)
    COSLAT = COS(RLAT)
    KMAX = 0.208 + DKT(MONTH)*(2.77 + DKT(MONTH)*(-4.75 + 2.92*
      &  DKT(MONTH)))
    DO 200 I = 1,8
        COSB = COS(RC*BE(I))

```



```

        SINB = SIN(RC*ABE(I))
        COSAZ = COS(RC*AZ(I))
        THETA = SINDEC*(SINLAT*COSB - COSLAT*SINB*COSAZ) +
        &          COSDEC*(COSLAT*COSB + SINLAT*SINB*COSAZ)
C   CHECK IF SUN IS BEHIND SURFACE AT NOON
        IF (THETA .LT. 0.3) THEN
            IF (I .EQ. 6 .OR. I .EQ. 8) THEN
C   EAST & WEST SURFACES
                THETA = 0.8*DKT(MONTH)
            ELSE IF (I .EQ. 5) THEN
C   NORTH SURFACE
                THETA = 0.3*DKT(MONTH)
            ELSE
C   SOUTH SURFACE, SUN HIGH ABOVE TILT
                THETA = 0.3
            END IF
        END IF
        RMAX = 8.25*THETA*KMAX
        DO 100 J = 1,11
100      IC(I,J) = FLOAT(J - 1)*RMAX
200    CONTINUE
C
        RETURN
        END

SUBROUTINE PHI(IN, HOUR, AINST, I1, I2, HRMN, EX)
C   SUBROUTINE TO CALCULATE THE UTILIZABILITY NUMERATOR
C   IN = INSTRUMENT INDEX NUMBER, AINST = INSTRUMENT LABEL
        REAL IC
        INTEGER FLAG, HOUR, EX, HRMN
        CHARACTER*5 AINST
        COMMON /COM1/ HPHI(21,8,11), DPHI(8,11)
        COMMON /COM2/ SUMI(21,15), SUMH(15), IC(8,11), RC, RLAT, PI
        COMMON /COM3/ MDATA(60), FLAG(60)
        DO 500 MIN = I1, I2
            IF (MDATA(MIN) .LE. 0) GO TO 500
            IF (FLAG(MIN) .EQ. 99 .OR. FLAG(MIN) .EQ. 13) GO TO 500
            IF (FLAG(MIN) .EQ. 11 .OR. FLAG(MIN) .EQ. 12) THEN
                RDATA = (FLOAT(MDATA(MIN))) * 10.**EX
                SUMI(HOUR, IN) = SUMI(HOUR, IN) + RDATA
                SUMH(IN) = SUMH(IN) + RDATA
                DO 100 J = 1,11
                    IF (RDATA .GT. IC(IN,J)) THEN
                        HPHI(HOUR, IN, J) = HPHI(HOUR, IN, J) + RDATA - IC(IN, J)
                        DPHI(IN, J) = DPHI(IN, J) + RDATA - IC(IN, J)
                    END IF
                100 CONTINUE
            ELSE
                WRITE(*,600) AINST, HRMN, FLAG(MIN)
            END IF
        END DO

```

```
      END IF  
500  CONTINUE  
600  FORMAT('0','UNRECOGNIZED FLAG:  INST ',A5,' DAY/HR/MN ',I6,  
      &      ' FLAG = ',I2)  
      RETURN  
      END
```

APPENDIX H

```

C THIS PROGRAM CALCULATES THE DAILY UTILIZABILITY USING CLARK'S HOURLY
C CORRELATION. OUTPUT ALSO INCLUDES HOURLY UTILIZABILITY FOR HOUR 12-13.
C THIS VERSION USES EITHER MONTHLY-AVERAGE DAILY KT'S OR READS IN
C MONTHLY-AVERAGE HOURLY KT'S FROM LFN 16.
C WRITTEN BY ALAN SCHULER, SEPT. 1985, FOR THE HARRIS COMPUTER.
C
C DKTB = MONTHLY-AVERAGE DAILY CLEARNESS INDEX FROM REAL DATA.
C HKTB(HOUR) = MONTHLY-AVERAGE HOURLY CLEARNESS INDEXES.
C RC=PI/180=0.01745, RLAT=LATITUDE, GSC=SOLAR CONSTANT (KW/M2)
C RBERB = DIFFUSE + BEAM + GROUND REFLECTANCE (RBER WITH ERBS CORR. INPUT)
C NOTE: RANGE OF ERBS NONSEASONAL HD/H CORRELATION IS FOR 0.3 < KT < 0.8
C B(INST) = SLOPE, AZ(INST) = AZIMUTH ANGLE
C AVDAY(MONTH) = AVE. DAY FOR MONTH IN YEAR
C
C   INTEGER HOUR
C   REAL IC, IMAX, IDI, DKTB(12)
C   CHARACTER*5 AINST(8),AMONTH(12),AMO
C   CHARACTER*7 LOCTN
C   DIMENSION B(8),AVDEC(12),AZ(8),COS1(8),COS2(8),AVDAY(12)
C   COMMON /COM3/PI,GSC,RC,TANLAT,SINLAT,COSLAT,COSDEC,SINDEC,
C   &      COSAZ(8),SINAZ(8),COSB(8),SINB(8)
C   COMMON /COM4/HKTB(21),RBERB(21,8),IC(8,11),DPHI(8,11),DEN(8),
C   &      HPHI(8,11),HDEN(8)
C
C   DATA AZ/4*0.0,180.,-90.,0.0,90./
C   DATA AVDEC/-20.9,-13.0,-2.4,9.4,18.8,23.1,21.2,13.5,2.2,-9.6,
C   &      -18.9,-23.0/
C   DATA AVDAY/17.,47.,75.,105.,135.,162.,198.,228.,258.,288.,
C   &      318.,344./
C   DATA AMONTH/'JAN','FEB','MARCH','APRIL','MAY','JUNE',
C   &      'JULY','AUG','SEPT','OCT','NOV','DEC'/
C   DATA PI, RC, GSC / 3.141593, 0.01745, 1.353/
C   DATA HKTB/21*0.0/
C
C *** TRINITY UNIVERSITY DATA SECTION ***
C   DATA AINST,RLAT/'HORIZ',' 20S ',' 30S ',' 40S ',' 90N ',' 90E ',
C   &      ' 90S ',' 90W ',29.53/
C   DATA DKTB,RHO,CONST/0.498,0.445,0.402,0.405,0.507,0.479,0.570,
C   &      0.579,0.603,0.482,0.593,0.472,0.05,0.8/
C   DATA B/0.0,20.,30.,40.,4*90./
C
C *** ALBANY, N.Y. DATA SECTION ***
C   DATA AINST,RLAT/'HORIZ',' 33S ',' 43S ',' 53S ',' 90N ',' 90E ',
C   &      ' 90S ',' 90W ',42.7/
C   DATA DKTB,RHO,CONST/0.499,0.382,0.443,0.432,0.561,0.489,0.489,
C   &      0.450,0.533,0.435,0.387,0.418,0.0,0.7/
C   DATA B/0.0,33.,43.,53.,4*90./

```

```

    RLAT = RLAT*RC
    TANLAT = TAN(RLAT)
    SINLAT = SIN(RLAT)
    COSLAT = COS(RLAT)
    INST = 8
C   *** CALCULATE CONSTANTS FOR GIVEN INSTRUMENT ***
    DO 50 I = 1,INST
        AZ(I) = AZ(I) * RC
        COSAZ(I) = COS(AZ(I))
        SINAZ(I) = SIN(AZ(I))
        B(I) = B(I) * RC
        COSB(I) = COS(B(I))
        SINB(I) = SIN(B(I))
        COS1(I) = (1. + COSB(I))/2.
50    COS2(I) = RHO*(1. - COSB(I))/2.
C100  FORMAT('TRINITY SEMRT:  CLARKS METHOD')
100   FORMAT('ALBANY SEMRT:  CLARKS METHOD')
110   FORMAT(' ',A5)
120   FORMAT(A5)
125   FORMAT('DAILY UTILIZABILITY')
126   FORMAT('HOURLY UTILIZABILITY')
C130  FORMAT('TRINITY SEMRT:  CLARKS HOURLY (12-13) UTILIZABILITY')
130   FORMAT('ALBANY SEMRT:  CLARKS HOURLY (12-13) UTILIZABILITY')
131   FORMAT(A7)
133   FORMAT(' ', 'MISMATCH IN MONTHS:  FILE = ',A5)
135   FORMAT(16(F4.2))
C
C   READ IN HOURLY KT'S
    READ(16,131) LOCTN
C   IF (LOCTN .NE. 'TRINITY') THEN
    IF (LOCTN .NE. 'ALBANY') THEN
        WRITE(3,*) 'MISMATCH IN KT LOCATIONS'
        STOP
    END IF
C
    DO 5000 MONTH = 1,12
        WRITE(12,100)
        WRITE(3,110) AMONTH(MONTH)
        WRITE(12,120) AMONTH(MONTH)
        WRITE(12,125)
C   READ IN HOURLY KT'S
        READ(16,120) AMO
        IF (AMO .NE. AMONTH(MONTH)) THEN
            WRITE(3,133) AMO
            STOP
        END IF
        READ(16,135) (HKTB(HOUR), HOUR = 5,20)
C
        DECL = AVDEC(MONTH) * RC
        COSDEC = COS(DECL)
        SINDEC = SIN(DECL)

```

```

C (SUNSET HOUR ANGLE IN DEGREES)
  WS = ACOS(-TANLAT*TAN(DECL))/RC
C EXTRATERRESTRIAL (KJ/M2-HR)
  GON = 13750.*GSC*(1.+0.033*COS(2.*PI*AVDAY(MONTH)/365.))
C CONSTANTS FOR RT (EQ. 2.13.1)
  RTA = 0.409 + 0.5016*SIN((WS-60)*RC)
  RTB = 0.6609 - 0.4767*SIN((WS-60)*RC)
C CONVERT SUNSET HOUR ANGLE BACK TO RADIANS
  WS = WS * RC
C HD/H: FROM ERBS NONSEASONAL CORRELATION (EQ. 4.23)
  HDH = (-3.023 + (3.373 - 1.760*DKTB(MONTH))*DKTB(MONTH))*
    & DKTB(MONTH) + 1.317
  IF (HDH .GT. 1.0) THEN
    HDH = 1.0
    WRITE(3,*) 'HDH > 1.0'
  END IF
C FROM ERBS RBAR PROGRAM:
  IF (DKTB(MONTH) .GT. 0.8) HDH = 0.156
C
C RESET VALUES AT THE START OF EACH MONTH
  DO 200 I = 1, INST
    DO 150 J = 1, 11
      HPHI(I,J) = 0.0
150    DPHI(I,J) = 0.0
      HDEN(I) = 0.0
      DEN(I) = 0.0
200    CALL ICRIT(I, MONTH, AINST, CONST)
C
  DO 2000 HOUR = 5, 20
    DO 300 I = 1, INST
300    RBERB(HOUR, I) = 0.0
C HOUR ANGLES IN RADIANS
  W1 = (FLOAT(HOUR) - 1.0 - 12.0) * 0.2618
  W2 = (FLOAT(HOUR) - 12.0) * 0.2618
C CHECK IF ALL OF HOUR IS DARK
  IF (W1 .GE. WS) GO TO 2000
  IF (W2 .LE. -WS) GO TO 2000
C CHECK IF PART OF HOUR IS DARK
  IF (W1 .LT. -WS) W1 = -WS
  IF (W2 .GT. WS) W2 = WS
C USE MIDDLE OF HOUR FOR ZENITH ANGLE, AND RDRT CALCULATIONS (IN RADIANS)
  W = (W1 + W2)/2.
  RDRT = 1./(RTA + RTB*COS(W))
  HKTB(HOUR) = DKTB(MONTH)/RDRT
C ID/I = (RD/RT)(HD/H)
  IDI = HDH*RDRT
  IF (IDI .LE. 0.0) THEN
    WRITE(3,*) 'HOUR = ', HOUR, ' IDI = ', IDI
    IDI = 0.0
  END IF
  IF (IDI .GE. 1.0) THEN

```

```

        WRITE(3,*) 'HOUR = ',HOUR,'   IDI = ',IDI
        IDI = 1.0
    END IF
    THEZ = COSDEC*cosLAT*cos(W) + SINDEC*sinLAT
    IF (THEZ .LT. 1.0E-06) THEN
C   BEAM COMPONENT, RB(HOUR,I) = 0.0
        THEZ = 0.0
        DO 500 I = 2,INST
500      RBERB(HOUR,I) = IDI*cos1(I) + cos2(I)
        GO TO 1500
    END IF
C
    DO 1000 I = 1,INST
        P = SINDEC*(sinLAT*cosB(I) - cosLAT*sinB(I)*cosAZ(I))
        Q = COSDEC*cos(W)*(cosLAT*cosB(I) + sinLAT*sinB(I)*cosAZ(I))
        S = COSDEC*sinB(I)*sinAZ(I)*sin(W)
        THETA = P + Q + S
        IF (THETA .LT. 1.0E-04) THETA = 0.0
        RB = THETA/THEZ
        RBERB(HOUR,I) = IDI*cos1(I) + (1-IDI)*RB + cos2(I)
        IF (RBERB(HOUR,I) .LT. 0.0) THEN
            RBERB(HOUR,I) = 0.0
            WRITE(3,2100) AINST(I),HOUR
            WRITE(3,*) 'IDI = ',IDI,'   cos2(I) = ',cos2(I)
        END IF
1000 CONTINUE
C
1500 CALL PHICAL(GON,W2,W1,HOUR,INST)
C
2000 CONTINUE
2100 FORMAT('0','RBER WAS < 0 FOR INST ',A5,', HOUR ',I2)
C
C   *** UTILIZABILITY ***
    DO 2500 I = 1,INST
        DO 2400 J = 1,11
            HPHI(I,J) = HPHI(I,J)/HDEN(I)
2400      DPHI(I,J) = DPHI(I,J)/DEN(I)
2500 CONTINUE
        GO TO 4000
C
C   *** RBER OUTPUT ***
    WRITE(3,3320)
3320 FORMAT(' ', 'TIME 05-06 06-07 07-08 08-09 09-10 10-11 11-12 ',
        & '12-13 13-14 14-15 15-16 16-17 17-18 18-19')
    WRITE(3,3340) (HKT(B(HOUR),HOUR=6,19)
3340 FORMAT(' ', 'KIBAR',14(2X,F4.2))
    DO 3350 I = 2,8
3350      WRITE(3,3360) AINST(I),(RBERB(HOUR,I),HOUR=6,19)
3360 FORMAT(' ',A5,14(1X,F5.2))
C
C   *** CRITICAL LEVEL OUTPUT ***

```

```

3500 WRITE(3,3540)
3540 FORMAT(' ','CRITICAL LEVELS (W/M2)')
      WRITE(3,3550) AINST(1),AINST(3),AINST(7),AINST(5),AINST(8)
3550 FORMAT(' ',5(2X,A5))
      DO 3600 J = 1,11
          IC(1,J) = IC(1,J)/3.6
          IC(3,J) = IC(3,J)/3.6
          IC(7,J) = IC(7,J)/3.6
          IC(5,J) = IC(5,J)/3.6
          IC(8,J) = IC(8,J)/3.6
3600     WRITE(3,3700) IC(1,J),IC(3,J),IC(7,J),IC(5,J),IC(8,J)
3700 FORMAT(' ',5(F7.1))
C
C   *** DAILY PHI OUTPUT ***
4000 WRITE(12,4010) AINST(1),AINST(2),AINST(7),AINST(4),AINST(6)
4010 FORMAT('IC1(W/M2)',5(3X,A5))
C   DO FOR ALL CRITICAL LEVELS, SURFACES 1,2,7,4,6
      DO 4050 J = 1,11
          IC(1,J) = IC(1,J)/3.6
4050     WRITE(12,4060) IC(1,J),DPHI(1,J),DPHI(2,J),DPHI(7,J),
          &             DPHI(4,J),DPHI(6,J)
4060 FORMAT(F7.1,2X,5(2X,F6.3))
C
C   *** HOURLY PHI OUTPUT, HOUR 12-13 ***
      WRITE(14,130)
      WRITE(14,120) AMONTH(MONTH)
      WRITE(14,126)
      WRITE(14,4010) AINST(1),AINST(2),AINST(7),AINST(4),AINST(6)
      DO 4080 J = 1,11
          WRITE(14,4060) IC(1,J),HPHI(1,J),HPHI(2,J),HPHI(7,J),
          &             HPHI(4,J),HPHI(6,J)
4080     IC(1,J) = IC(1,J)*3.6
C
C   REPEAT FOR NEXT MONTH
5000 CONTINUE
C
6000 STOP
      END

      SUBROUTINE PHICAL(GON,W2,W1,HOUR,INST)
C   SUBROUTINE TO CALCULATE THE DAILY UTILIZABILITY
C   IHOR = IRRADIATION ON HORIZONTAL SURFACE (KJ/M2-HR)
C   IT = TILTED IRRADIATION (KJ/M2-HR)
      INTEGER HOUR
      REAL IC,IT,IHOR
      COMMON /COM3/PI,GSC,RC,TANLAT,SINLAT,COSLAT,COSDEC,SINDEC,
          &     COSAZ(8),SINAZ(8),COSB(8),SINB(8)
      COMMON /COM4/HKTB(21),RBERB(21,8),IC(8,11),DPHI(8,11),DEN(8),
          &     HPHI(8,11),HDEN(8)
C

```

```

      IF (HKT(B(HOUR)) .LE. 0.0001) RETURN
      IHOR = GON*(COSLAT*COSEDEC*(SIN(W2)-SIN(W1)) +
&      (W2-W1)*SINLAT*SINDEC)*HKT(B(HOUR))
      IF (IHOR .LT. 0.0) THEN
        WRITE(3,*) 'ERROR: IHOR = ',IHOR
        IHOR = 0.0
      END IF
C
      DO 1000 I = 1,INST
        IT = IHOR*RB(B(HOUR),I)
        IF (IT .LT. 0.0) THEN
          WRITE(3,*) 'ERROR: IT = ',IT
          IT = 0.0
        END IF
        DEN(I) = DEN(I) + IT
        XM = 1.85 + 0.169*RB(B(HOUR),I)/(HKT(B(HOUR))*HKT(B(HOUR))) -
&        0.0696*COSE(I)/(HKT(B(HOUR))*HKT(B(HOUR))) -
&        0.981*HKT(B(HOUR))/(COSEDEC*COSEDEC)
        XM = AMAX1(XM,1.)
        DO 500 J = 1,11
          IF (IT .EQ. 0.0) THEN
            PHID = 0.0
            GO TO 500
          ELSE
            XC = IC(I,J)/IT
            END IF
            IF (XC .GE. XM) THEN
              PHID = 0.0
            ELSE IF (XM .EQ. 2.0) THEN
              SPHI = 1. - XC/XM
              PHID = SPHI*SPHI
            ELSE
              A = (XM - 1.0)/(2.0 - XM)
              DISCR = AAA + (1.+2.*A)*(XM-XC)*(XM-XC)/(XM*XM)
              DISCR = AMAX1(DISCR,0.0)
              PHID = ABS(ABS(A) - SQRT(DISCR))
            END IF
            DPHI(I,J) = DPHI(I,J) + PHID*IT
            IF (HOUR .EQ. 13) THEN
              HPHI(I,J) = HPHI(I,J) + PHID*IT
              IF (J .EQ. 1) HDEN(I) = HDEN(I) + IT
            END IF
          500 CONTINUE
        1000 CONTINUE
C
      RETURN
      END

```

```

      SUBROUTINE ICRIT(I,MONTH,AINST,CONST)
C  SUBROUTINE TO CALCULATE CRITICAL LEVELS FOR EACH INSTRUMENT.

```



```

C  USE FRACTION OF MAXIMUM NOON TIME VALUES (W=0.0) FOR LARGEST CRITICAL
C  LEVEL.
      REAL IC,KMAX,KTB(12)
      CHARACTER*5 AINST(8)
      COMMON /COM3/PI,GSC,RC,TANLAT,SINLAT,COSLAT,COSDEC,SINDEC,
&  COSAZ(8),SINAZ(8),COSB(8),SINB(8)
      COMMON /COM4/HKTB(21),RBERB(21,8),IC(8,11),DPHI(8,11),DEN(8),
&  HPHI(8,11),HDEN(8)
C
C  TRINITY DKTB'S FOR CRITICAL LEVEL CALCULATIONS (OLD VALUES)
C  DATA KTB/0.463,0.406,0.390,0.376,0.488,0.475,0.557,0.540,0.577,
C  & 0.452,0.533,0.443/
C  ALBANY DKTB'S FOR CRITICAL LEVEL CALCULATIONS (OLD VALUES)
C  DATA KTB/0.461,0.353,0.423,0.428,0.546,0.487,0.459,0.453,0.517,
C  & 0.408,0.372,0.406/
C
      DKTB = KTB(MONTH)
      THETA = SINDEC*(SINLAT*COSB(I) - COSLAT*SINB(I)*COSAZ(I))
&  + COSDEC*(COSLAT*COSB(I) + SINLAT*SINB(I)*COSAZ(I))
      KMAX = 0.208 + DKTB*(2.77 + DKTB*(-4.75 + 2.92*DKTB))
C  CHECK IF SUN IS BEHIND SURFACE AT NOON
      IF (THETA .LT. 0.3) THEN
        IF (I .EQ. 6 .OR. I .EQ. 8) THEN
C  EAST & WEST SURFACES
          THETA = CONST*DKTB
        ELSE IF (I .EQ. 5) THEN
C  NORTH SURFACE
          THETA = 0.3*DKTB
        ELSE
C  SOUTH SURFACE, SUN HIGH ABOVE TILT
          THETA = 0.3
        END IF
      END IF
      RMAX = 495.0*THETA*KMAX
      DO 100 J = 1,11
100    IC(I,J) = FLOAT(J - 1)*RMAX
C
      RETURN
      END

```

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CLOSING THOUGHTS

And so ends my thesis,
There's no where else to look.
You may read it again,
If you're really hooked.

I do hope you learned
Something interesting today.
For God's world is exciting,
In a most wonderful way.

-- Alan Schuler
January, 1986